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COMPARISON OF LIGHTNING AND NEMP: EXTRAPOLATION OF AIRCRAFT EMP SIMULATOR DATA

Volume III—Data - Preliminary Study

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ABSTRACT (Continue on reverse if necessary and identify by block number) TRESTLE Simulator Data acquired during the 1982 B-52 OAS/CMC EMP Test is extrapolated to lightning and EMP criteria. The extrapolated data is compared via study of waveform attributes.					
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CONVERSION TABLE

Conversion factors for U.S. customary to metric (SI) units of measurement.

To Convert From	То	Multiply By
angstrom	meters (m)	1.000 000 X E -10
atmosphere (normal)	kilo pascal (kPa)	1.013 25 XE+2
bar	kilo pascal (kPa)	1.000 000 X E +2
barn	meter ² (m ²)	1.000 000 X E -28
British thermal unit (thermochemical)	joule (J)	1.054 350 X E +3
calorie (thermochemical)	joule (J)	4. 181 000
cal (thermochemical)/cm ²	mega joule/m ² (MJ/m ²)	4. 184 000 X E -2
curie	*giga becquerel (GBq)	3.700 000 X E +1
degree (angle)	radian (rad)	1. 745 329 X E -2
degree Fahrenheit	degree kelvin (K)	$t_{\nu} = (t^{2}f + 459.67)/1.8$
electron volt	joule (J)	1.602 19 X E -19
erg	joule (J)	1.000 000 X E -7
erg/second	watt (W)	1.000 000 X E -7
foot	meter (m)	3, 048 000 X E -1
foot-pound-force	joule (J)	1, 355 818
gallon (U.S. Hquid)	meter ³ (m ³)	3. 785 412 X E -3
inch	meter (m)	2. 540 000 X E -2
jerk	joule (J)	1.000 000 X E +9
joule/kilogram (J/kg) (radiation dose absorbed)	Gray (Gy)	1,000 000
kilotons	terajoules	4. 183
kip (1000 lbf)	newton (N)	4. 448 222 X E +3
kip/inch ² (l:3i)	kilo pascal (kPa)	6, 894 757 X E +3
ktap	newton-second/m ² (N-s/m ²)	1.000 000 X E +2
micron	meter (m)	1 000 000 X E -6
mil	meter (m)	2, 540 000 X E -5
mile (international)	meter (m)	1, 609 344 X E +3
ounce	kilog ram (kg)	2. 834 952 X E -2
pound-force (lbs ave trdupois)	newton (N)	4, 448 222
pound-force unch	newton-moter (K·m)	1. 129 848 X E -1
pound-force/inch	newton/meter (N/m)	1, 751 268 X E +2
pound-force/foot ²	kilo pascal (kPa)	4. 788 026 X E -2
pound-force/inch ² (psi)	kilo pascal (kPa)	6, 894 757
pound-mass (lbm avoirdupois)	kilogram (kg)	4. 535 924 X E -1
pound-mass-foot ² (moment of inertia)	kilogram-meter ² (kg·m ²)	4. 214 011 X E -2
pound-mass/foot ³	kılogram/meter ³ (kg/m ³)	1. 601 846 X E +1
rad (radiation dose absorbed)	**Gray (Cy)	1,000 000 X E -2
roentgen	coulomb/kilc-f;ram (C/kg)	2, 579 760 X E -4
shake	second (s)	1 000 000 X E -8
slug	kilogram (Vg)	1. 459 390 X E +1
torr (mm Hg, 0° C)	kilo pasc Pa)	1. 333 22 X E -1

The becquerel (Bq) is the SI unit of radioactivity; 1 Bq = 1 ev., ni/s.
**The Gray (Gy) is the SI unit of absorbed radiation.



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SECTION 1 INTRODUCTION

This volume presents the preliminary study which was performed using a double exponential EMP criterion and lightning criteria¹. The methods used for this preliminary study were identical to those used for the final study. These methods are described in Volume I of this report. This volume will describe the criteria used in the preliminary study and discuss the results of this preliminary comparison. Appendix A contains a table of the scalar attributes of the extrapolated waveforms. Appendix B contains plots of the corrected B-52 data as well as that data extrapolated to the EMP and lightning criteria.

B.G. Melander, et. al., "Atmospheric Electricity Hazards Threat Environment Definition," Boeing Document D180-27423-1, April 1983.

SECTION 2 EMP AND LIGHTNING CRITERIA

2.1 EMP CRITERION.

The EMP criterion used in the preliminary study is a double exponential waveform. The electric field is defined as:

$$E(t) = E_0(e^{-\alpha t} - e^{-\beta t})$$
 (1)

where

$$E_0 = 5.23 \times 10^4 \text{ V/m},$$

$$\alpha = 4.0 \times 10^6 \text{ s}^{-1}$$

and

$$\beta = 4.76 \times 10^8 \text{ s}^{-1}$$

The EMP waveform propagates as a plane wave, therefore the magnetic field is defined as:

$$H(t) = E(t)/Z_0, (2)$$

where, Z_0 = impedance of free space = 377Ω .

2.2 LIGHTNING CRITERION.

The lightning criterion used in the preliminary study was defined in the Atmospheric Electricity Hazards Protection (AEHP) program. This program defined two separate lightning criteria (both moderate and severe) by study of existing lightning data. These criteria are described in terms of the lightning current, and are also double exponential waveforms. The magnetic field produced by this current can be approximated by assuming that the field is produced by uniform current on an infinite cylinder, and is given by Equation 3.

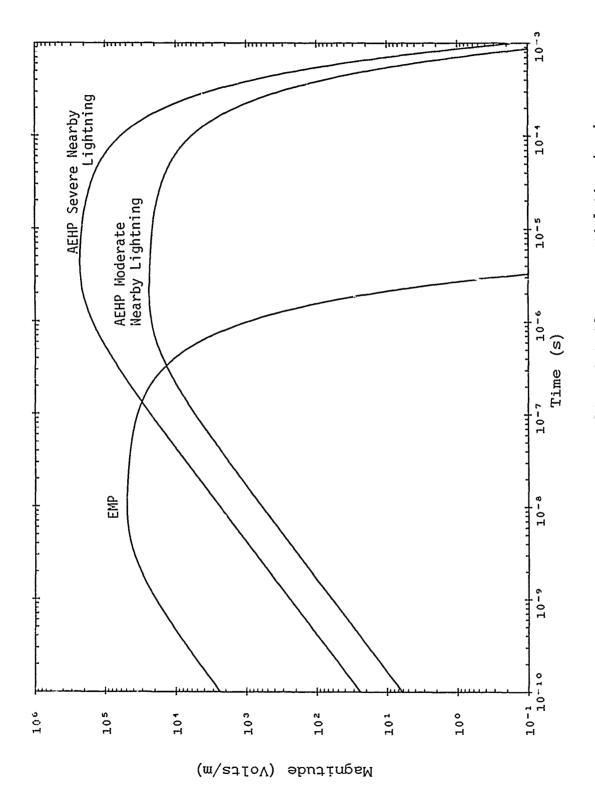
$$H(t) = I(t)/2\pi R \tag{3}$$

where R is the distance from the lightning strike.

I(t) is the lightning current given by the double exponential waveform. The AEHP lightning criteria have the peak current and rise and fall rates shown in Table 1. The resulting electric fields at 50 m from the lightning stroke along with the EMP waveform are shown in Figures 1 and 2. Only the severe criterion was used in this study.

Table 1. AEHP lightning parameters.

Io	α	β
20.6kA	14.3x10 ³ s ⁻¹	2.5x10 ⁶ s ⁻¹
206kA	14.3x10 ³ s ⁻¹	1.0 x10 ⁶ s ⁻¹



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AEHP lightning fields and double exponential-time domain. Figure 1.

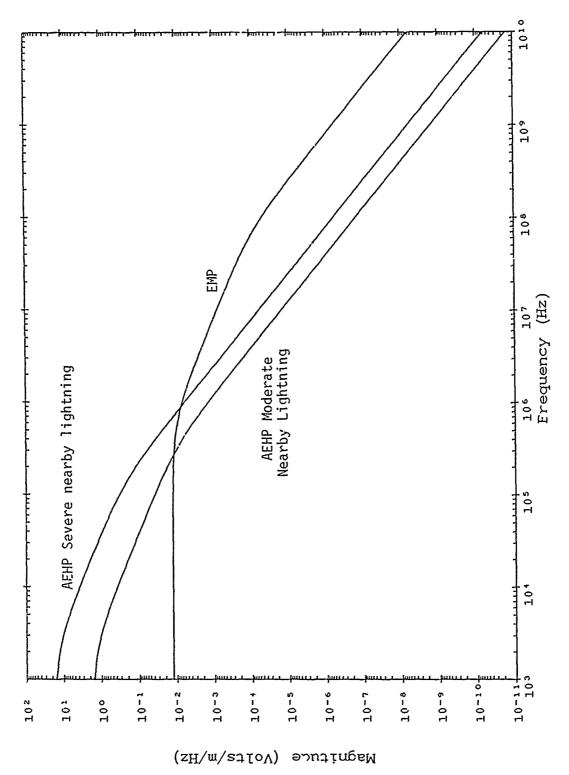


Figure 2. AEHP lightning fields and double exponential-frequency domain.

SECTION 3 COMPARISON OF EXTRAPOLATED DATA

The comparison of the responses after extrapolation to the EMP and lightning threats is accomplished via use of the waveform attributes described in Volume I of this report.

3.1 PEAK ABSOLUTE AMPLITUDE.

We can see from Figure A-2 that the peak absolute amplitude of the waveform for the EMP threat was higher than the lightning response for all cases. At frequencies above 2 MHz, the EMP magnetic field is stronger than the lightning fields. The majority of the corrected data responses resonate well above 2 MHz, thus the extrapolated responses at the resonant frequencies are stronger for EMP than lightning.

3.2 PEAK ABSOLUTE DERIVATIVE.

Figure A-4 shows that the peak absolute derivative of the EMP response is significantly greater than that of the lightning response. This is due to the difference in risetime between the two threats.

3.3 PEAK ABSOLUTE IMPULSE.

The peak absolute impulse of a waveform is related to the low frequency content. The lightning field has a larger low frequency content than the EMP field, thus the peak absolute impulse of the lightning response is generally larger than that of the EMP response.

3.4 RECTIFIED IMPULSE.

The rectified impulse comparison is shown in Figures A-7 and A-8. This parameter is not clearly worse for either EMP or lightning fields.

3.5 ROOT ACTION INTEGRAL.

The root action integral is a measure of the energy carried by the waveform. Figure A-10 shows that the EMP response almost always had a higher root action integral than the lightning response.

APPENDIX A WAVEFORM NORM ATTRIBUTES

Table A-1. Comparison of peak absolute amplitudes.

TEST POINT	SHOT Number	PEAK ABSOLUTE AMPLITUDE EMP	PEAK ABSOLUTE AMPLITUDE LIGHTNING
0059	2276	0.600E+00	0.256E+00
0141	2662	0.253E-02	0.333E-03
0434	2502	0.954E+01	0.891E+00
0504	1680	0.439E+00	0.716E-01
0516	2615	0.927E+00	0.319E+00
0594	2584	0.277E-02	0.521E-03
0643	2261	0.666E+00	0.898E-01
0705	2535	0.197E+01	0.832E+00
0715	1798	0.325E+00	0.275E-01
0723	2256	0.405E+01	0.972E+00
0903	1428	0.203E-01	0.173E-01
0918	2550	0.825E+00	0.228E+00
1182	1159	0.113E+01	0.204E+00
1473	1779	0.493E+00	0.717E-01
1660	2545	0.508E+00	0.777E-01
2238	2154	0.718E+00	0.682E-01
2391	1734	0.589E+00	0.169E+00 0.959E-01
2426 2717	1306 2560	0.760E+00 0.188E+01	0.459E+00
2866	2274	0.421E+01	0.459E+00 0.107E+01
3313	2521	0.421E+01 0.104E+01	0.178E+00
3313	2689	0.104E+01 0.103E+01	0.178E+00 0.133E+00
3385	1718	0.772E+00	0.133E+00 0.487E-01
3473	2607	0.772E+00 0.198E+01	0.560E+00
3539	2727	0.139E+01	0.365E+00
3543	2265	0.674E+00	0.927E-01
3615	1675	0.848E+00	0.223E+00
3626	2531	0.136E+01	0.218E+00
3795	2281	0.174E+01	0.847E-01
3884	2255	0.402E+01	0.102E+01
3919	1156	0.990E+01	0.381E+01
4050	1680	0.353E+00	0.499E-01
4225	2671	0.109E-01	0.249E-02
4309	2653	0.105E=01 0.381E+00	0.615E-01
4597	2436	0.101E+01	0.193E+00
4859	2144	0.624E+00	0.461E-01
4914	2217	0.531E+00	0.138E+00
4924	2645	0.122E+01	0.266E+00
5169	2588	0.928E+00	0.166E+00
5283	1717	0.457E+00	0.215E+00
5352	1234	0.454E+00	0.271E-01

Table A-1. Comparison of peak absolute amplitudes (Concluded)

TEST POINT	SHOT NUMBER	PEAK ABSOLUTE AMPLITUDE EMP	PEAK ABSOLUTE AMPLITUDE LIGHTNING
5393	2623	0.272E+01	0.203E+01
5415	2700	0.660E+00	0.332E+00
5511	2274	0.243E+01	0.211E+00
5524	2584	0.107E-02	0.368E-03
5584	2687	0.152E+01	0.299E+00
5611	2308	0.243E+00	0.222E-01
5611	2501	0.652E-01	0.174E-01
5727	1180	0.405E+00	0.365E-01
5737	2165	0.120E+01	0.472E-01
5813	2606	0.966E+00	0.224E+00
5869	2271	0.416E+01	0.846E+00
6369	2584	0.510E-01	0.113E+00
6381	1151	0.601E+00	0.166E+00
6482	2501	0.434E+00	0.561E-01
6562	2501	0.256E+01	0.392E+00
6708	2712	0.148E+01	0.224E+00
6732	2712	0.199E+01	0.297E+00
7045	2260	0.380E+01	0.999E+00
7059 7171	2226	0.135E+01	0.100E+00
7171	2504 2266	0.720E+00 0.731E+00	0.244E+00
7407	2166	0.731E+00 0.864E+00	0.985E-01 0.276E+00
7513	2638	0.770E+00	0.276E+00 0.134E+00
7516	2528	0.415E+01	0.134E+00 0.930E+00
7681	1720	0.415E+01	0.930E+00 0.628E-01
7873	2626	0.408E-02	0.429E-03
8027	2594	0.530E-03	0.464E-03
8075	2460	0.721E+00	0.404E-03 0.988E-01
8524	2151	0.711E+00	0.489E-01
8681	1797	0.476E+00	0.403E-01 0.801E-01
8695	2478	0.120E+02	0.107E+01
8806	2197	0.184E+01	0.207E+00
8877	2276	0.768E+00	0.154E+00
9063	2265	0.981E+00	0.103E∻00
9082	2609	0.960E+00	0.324E+00
9323	2605	0.128E-01	0.336E-02
9406	2421	0.811E+00	0.160E+00
9461	2628	0.110E+01	0.101E+01
9470	1684	0.252E+00	0.168E+00
9513	2618	0.107E+01	0.413E+00
9786	2697	0.389E+00	0.709E-01
9893	2551	0.424E+00	0.248E-01

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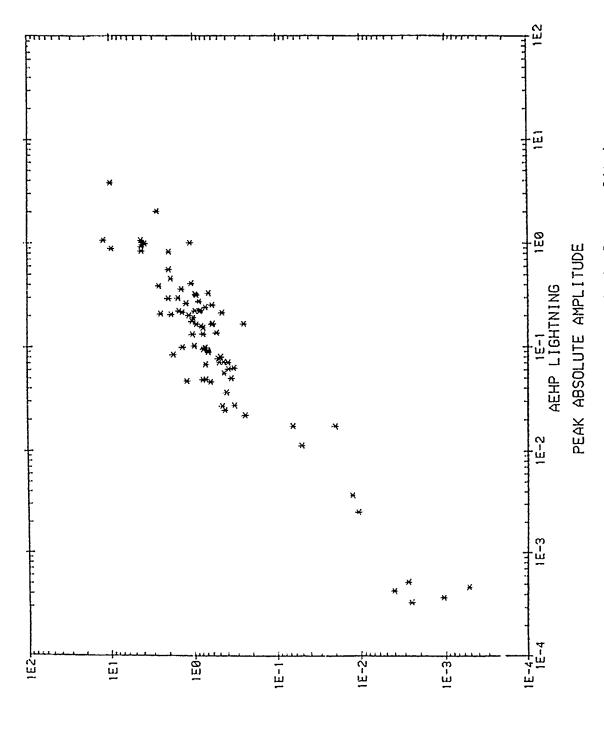


Figure A-1. Scatter plot of peak absolute amplitude.

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PEAK ABSOLUTE AMPLITUDE

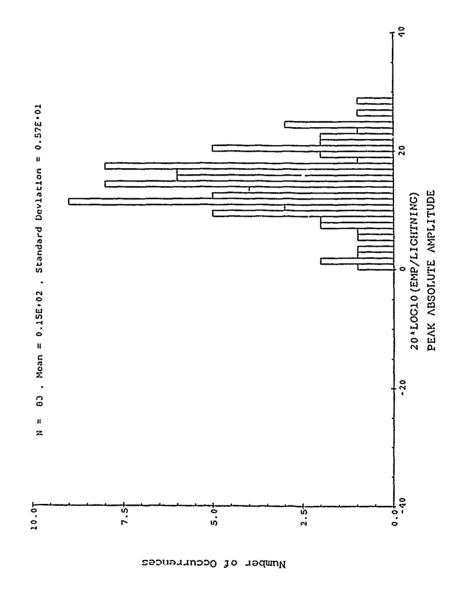


Figure A-2. Histogram of peak absolute amplitude.

Table A-2. Comparison of peak absolute derivatives.

TEST POINT	SHOT Number	PEAK ABSOLUTE DERIVATIVE EMP	PEAK ABSOLUTE DERIVATIVE LIGHTNING
0059	2276	0.147E+09	0.343E+07
0141	2662	0.591E+06	0.138E+05
0434	2502	0.194E+10	0.504E+08
0504	1680	0.989E+08	0.231E+07
0516	2615	0.299E+09	0.492E+07
0594	2584	0.571E+06	0.146E+05
0643	2261	0.159E+09	0.344E+07
0705	2535	0.148E+09	0.925E+07
0715	1798	0.157E+09	0.224E+07
0723	2256	0.270E+09	0.201E+08
0903	1428	0.426E+07	0.118E+06
0918	2550	0.161E+09	0.431E+07
1182	1159	0.237E+09	0.573E+07
1473	1779	0.566E+08	0.236E+07
1660	2545	0.618E+08	0.241E+07
2238	2154	0.374E+09	0.506E+07
2391	1734	0.772E+08	0.264E+07
2426	1306	0.108E+09	0.377E+07
2717	2560	0.473E+09	0.104E+08
2866	2274	0.371E+09	0.211E+08
3313	2521	0.329E+09	0.585E+07
3313	2689	0.149E+09	0.498E+07
3385	1718	0.504E+09	0.581E+07
3473	2607	0.343E+09	0.108E+08
3539	2727	0.103E+09	0.679E+07
3543	2265	0.247E+09	0.390E+07
3615	1675	0.178E+09	0.439E+07
3626	2531	0.255E+09	0.692E+07
3795	2281	0.917E+09	0.106E+08
3884	2255	0.210E+09	0.199E+08
3919	1156	0.166E+10	0.535E+08
4050	1680	0.110E+09	0.183E+07
4225	2671	0.161E+07	0.531E+05
4309	2653	0.189E+09	0.223E+07
4597 4859	2436 2144	0.203E+09 0.305E+09	0.543E+07
4914	2217	0.305E+09 0.145E+09	0.419E+07
4914	2645	0.145E+09 0.161E+09	0.285E+07
5169	2588	0.101E+09 0.285E+09	0.597E+07 0.519E+07
5283	2300 1717	0.205E+09 0.124E+09	0.519E+07 0.271E+07
5352	1234	0.124E+09 0.148E+09	0.271E+07 0.260E+07
	+-V7	U # # TOL ! U J	0.200E10/

Table A-2. Comparison of peak absolute derivatives (Concluded)

TEST POINT	SHOT NUMBER	PEAK ABSOLUTE DERIVATIVE EMP	PEAK ABSOLUTE DERIVATIVE LIGHTNING
5393	2623	0.272£+09	0.143E+08
5415	2700	0.100E+09	0.340E+07
5511	2274	0.124E+10	0.147E+08
5524	2584	0.156E+06	0.504E+04
5584	2687	0.143E+09	0.753E+07
5611	2308	0.617E+08	0.135E+07
5611	2501	0.236E+08	0.366E+06
5727	1180	0.128E+09	0.2205+07
5737	2165	0.603E+09	0.793E+07
5813	2606	0.178E+09	0.489E+07
5869	2271	0.236E+09	0.206E+08
6369	2584	0.492E+07	0.250E+06
6381	1151	0.684E+08	0.310E+07
6482	2501	0.111E+09	0.239E+07
6562	2501	0.440E+09	0.133E+08
6708	2712	0.239E+09	0.729E+07
6732	2712	0.184E+09	0.965E+07
7045	2260	0.248E+09	0.190E+08
7059	2226	0.173E+09	0.667E+07
7171	2504	0.179E+09	0.392E+07
7187	2266	0.219E+09	0.397E+07
7407	2166	0.682E+08	0.430E+07
7513	2638	0.109E+09	0.385E+07
7516	2528	0.481E+09	0.194E+08
7681	1720	0.464E+08	0.155E+07
7873	2626	0.895E+06	0.212E+05
8027	2594	0.140E+06	0.292E+04
8075	2460	0.121E+09	0.370E+07
8524	2151	0.417E+09	0.496E+07
8681	1797	0.842E+08	0.228E+07
8695	2478	0.327E+10	0.629E+08
8806	2197	0.430E+09	0.105E+08
8877	2276	0.756E+08	0.368E+07
9063	2265	0.372E+09	0.585E+07
9082	2609	0.177E+09	0.470E+07
9323	2605	0.176E+07	0.653E+05
9406	2421	0.196E+09	0.413E+07
9461	2628	0.166E+09	0.552E+07
9470	1684	0.369E+08	0.132E+07
9513	2618	0.204E+09	0.553E+07
9786	2697	0.166E+09	0.245E+07
9893	2551	0.146E+09	0.248E+07

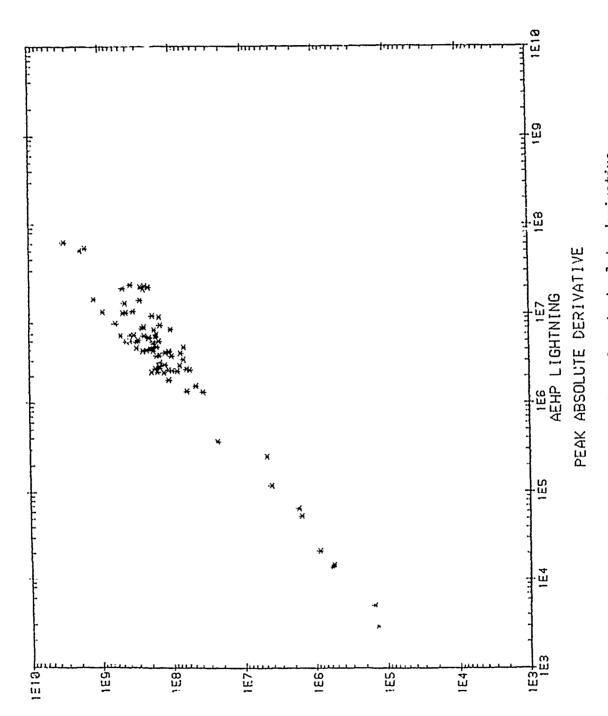
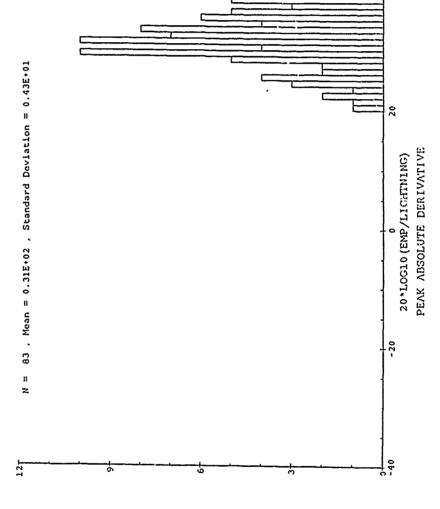


Figure A-3. Scatter plot of peak absolute derivative.

PEAK ABSOLUTE DERIVATIVE



Number of Occurrences

Table A-3. Comparison of peak absolute impulses.

TEST POINT	SHOT NUMBER	PEAK ABSOLUTE IMPULSE EMP	PEAK ABSOLUTE IMPULSE LIGHTNING
0059	2276	0.306E-07	0.177E-06
0141	2662	0.499E-10	0.300E-09
0434	2502	0.140E-06	0.915E-06
0504	1680	0.132E-07	0.116E-06
0516	2615	0.474E-07	0.946E-06
0594	2584	0.102E-09	0.309E-09
0643	2261	0.173E-07	0.611E-07
0705	2535	0.122E-06	0.122E-05
0715	1798	0.571E-08	0.398E-07
0723	2256	0.199E-06	0.843E-07
0903	1428	0.142E-08	0.472E-07
0918	2550	0.338E-07	0.333E-06
1182	1159	0.436E-07	0.379E-06
1473	1779	0.15JE-07	0.257E-07
1660	2545	0.156E-07	0.565E-07
2238	2154	0.123E-07	0.106E-06
2391	1734	0.293E-07	0.750E-07
2426	1306	0.189E-07	0.191E-07
2717	2560	0.651E-07	0.715E-06
2866	2274	0.217E-06	0.134E-06
3313 3313	2521	0.330E-07	0.223E-06
3385	2689 1718	0.195E-07	0.223E-06
3473	2607	0.902E-08 0.883E-07	0.109E-06 0.143E-05
3539	2727	0.597E-07	0.143E-05 0.180E-06
3543	2265	0.171E-07	0.160E-06 0.265E-07
3615	1675	0.1/1E-0/ 0.241E-07	0.487E-06
3626	2531	0.459E-07	0.467E-00
3795	2281	0.143E-07	0.330E-07 0.230E-06
3884	2255	0.209E-06	0.283E-06
3919	1156	0.436E-06	0.902E-05
4050	1680	0.586E-08	0.698E-07
4225	2671	0.293E-09	0.307E-08
4309	2653	0.914E-08	0.100E-06
4597	2436	0.219E-07	0.394E-06
4859	2144	0.966E-08	0.319E-07
4914	2217	0.216E-07	0.555E-07
4924	2645	0.373E-07	0.776E-06
5169	2588	0.284E-07	0.746E-07
5283	1717	0.241E-07	0.543E-06
5352	1234	0.464E-08	0.738E-07

Table A-3. Comparison of peak absolute impulses (Concluded)

TEST POINT	SHOT Number	PEAK ABSOLUTE IMPULSE EMP	PEAK ABSOLUTE IMPULSE LIGHTNING
5393	2623	0.273E-06	0.474E-05
5415	2700	0.393E-07	0.687E-06
5511	2274	0.389E-07	0.834E-07
5524	2584	0.301E-10	0.547E-09
5584	2687	0.496E-07	0.298E-06
5611	2308	0.340E-08	0.418E-07
5611 5727	2501	0.337E-08	0.216E-07
5737	1180 2165	0.505E-08	0.549E-07
5813	2606	0.873E-08 0.402E-07	0.647E-07 0.462E-06
5869	2271	0.402E-07 0.186E-06	0.402E-00 0.123E-05
6369	2584	0.167E-08	0.123L-03 0.920E-08
6381	1151	0.362E-07	0.259E-06
6482	2501	0.109E-07	0.235E-00 0.216E-07
6562	2501	0.593E-07	0.407E-06
6708	2712	0.279E-07	0.143E-06
6732	2712	0.595E-07	0.652E-06
7045	2260	0.199E-06	0.135E-06
7059	2226	0.237E-07	0.193E-06
7171	2504	0.365E-07	0.185E-06
7187	2266	0.198E-07	0.875E-07
7407	2166	0.492E-07	0.145E-06
7513	2638	0.219E-07	0.164E-06
7516	2528	0.132E-06	0.952E-06
7681	1720	0.121E-07	0.484E-07
7873	2626	0.550E-10	0.522E-09
8027	2594	0.390E-10	0.122E-08
8075	2460	0.213E-07	0.140E-06
8524	2151	0.103E-07	0.349E-07
3681	1797	0.134E-07	0.420E-07
8695 8806	2478	0.178E-06	0.154E-05
•	2197	0.322E-07	0.295E-06
8877	2276 2265	0.304E-07 0.206E-07	0.481E-07 0.719E-07
9082	2609	0.200E-07 0.579E-07	0.606E-06
9323	2605	0.579E-07 0.720E-09	0.308E-08
9406	2421	0.720E-09 0.366E-07	0.662E-07
9461	2628	0.107E-06	0.283E-05
9470	1684	0.221E-07	0.115E-06
9513	2618	0.542E-07	0.123E-05
9786	2697	0.862E-08	0.127E-06
9893	2551	0.341E-08	0.483E-07

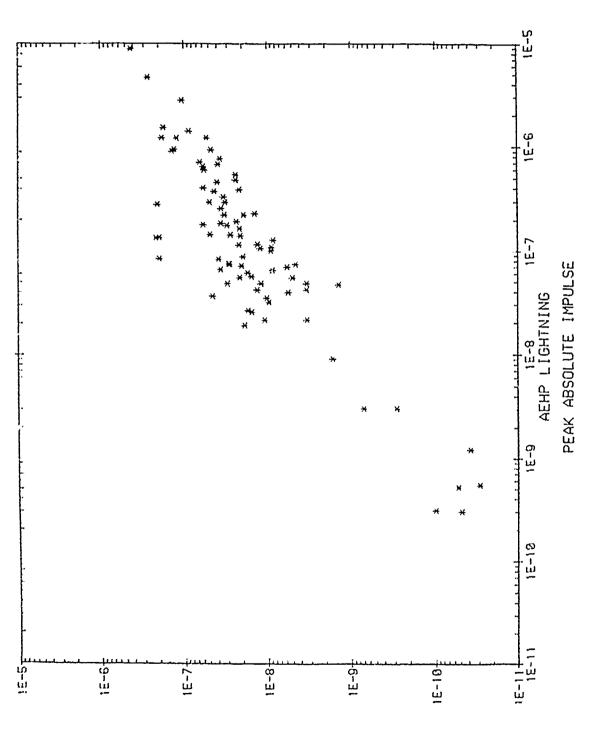
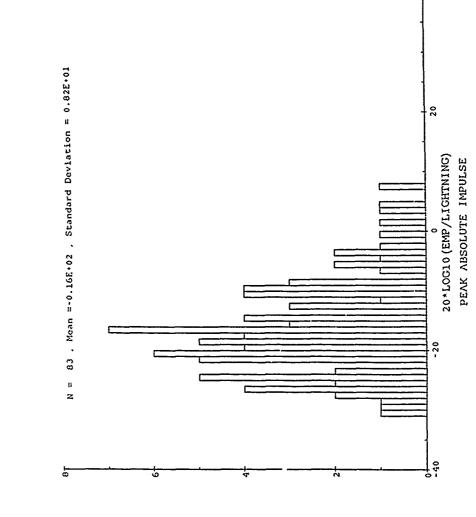


Figure A-5. Scatter plot of peak absolute impulse.

EWb

PEAK ABSOLUTE IMPULSE



Histogram of peak absolute impulse.

Figure A-6.

Number of Occurrences

Table A-4. Comparison of rectified impulses.

TEST POINT	SHOT NUMBER	RECTIFIED IMPULSE	RECTIFIED IMPULSE
		EMP	LIGHTNING
0059	2276	0.322E-06	0.330E-06
0141	2662	0.769E-09	0.586E-09
0434	2502	0.292E-05	0.211E-05
0504	1680	0.237E-06	0.187E-06
0516	2615	0.322E-06	0.995E-06
0594	2584	0.197E-08	0.419E-09
0643	2261	0.378E-06	0.149E-06
0705	2535	0.922E-06	0.157E-05
0715	1798	0.124E-06	0.502E-07
0723 0903	2256 1428	0.194E-05 0.876E-08	0.552E-06 0.525E-07
0903	2550	0.382E-06	0.559E-06
1182	1159	0.682E-06	0.559E-06
1473	1779	0.220E-06	0.561E-07
1660	2545	0.361E-06	0.111E-06
2238	2154	0.104E-06	0.114E-06
2391	1734	0.428E-06	0.167E-06
2426	1306	0.444E-06	0.108E-06
2717	2560	0.113E-05	0.778E-06
2866	2274	0.243E-05	0.620E-06
3313	2521	0.562E-06	0.248E-06
3313	2689	0.429E-06	0.292E-06
3385	1718	0.179E-06	0.127E-06
3473	2607	0.985E-06	0.170E-05
3539	2727	0.104E-05	0.427E-06
3543	2265	0.504E-06	0.111E-06
3615	1675	0.292E-06	0.585E-06
3626	2531	0.578E-06	0.162E-06
3795	2281	0.183E-06	0.254E-06
3884	2255	0.225E-05	0.714E-06
3919	1156	0.330E-05	0.944E-05
4050 4225	1680 2671	0.159E-06 0.584E-08	0.111E-06 0.480E-08
4309	2671 2653	0.157E-06	0.480E-08 0.143E-06
4597	2003 2436	0.157E-06 0.440E-06	0.510E-06
4859	2144	0.440E-00	0.627E-07
4914	2217	0.436E-06	0.185E-06
4924	2645	0.398E-06	0.826E-06
5169	2588	0.397E-06	0.170E-06
5283	1717	0.250E-06	0.657E-06
5352	1234	0.982E-07	0.773E-07

Table A-4. Comparison of rectified impulses (Concluded)

TEST POINT	SHOT Number	RECTIFIED IMPULSE EMP	RECTIFIED IMPULSE LIGHTNING
5393	2623	0.983E-06	0.499E-05
5415	2700	0.470E-06	0.772E-06
5511	2274	0.751E-06	0.772E=06
5524	2584	0.417E-09	0.115E-08
5584	2687	0.622E-06	0.522E-06
5611	2308	0.022E-00 0.411E-07	
5611	2501	0.411E-07 0.312E-07	0.584E-07
			0.446E-07
5727	1180	0.981E-07	0.696E-07
5737	2165	0.206E-06	0.746E-07
5813	2606	0.600E-06	0.579E-06
5869	2271	0.223E-05	0.219E-05
6369	2584	0.288E-07	0.225E-07
6381	1151	0.374E-06	0.282E-06
6482	2501	0.244E-06	0.479E-07
6562	2501	0.114E-05	0.438E-06
6708	2712	0.397E-06	0.222E-06
6732	2712	0.763E-06	0.843E-06
7045	2260	0.197E-05	0.520E-06
7059	2226	0.436E-06	0.225E-06
7171	2504	0.551E-06	0.311E-06
7187	2266	0.518E-06	0.197E-06
7407	2166	0.661E-06	0.274E-06
7513	2638	0.411E-06	0.288E-06
7516	2528	0.175E-05	0.210E-05
7681	1720	0.245E-06	0.106E-06
7873	2626	0.146E-08	0.103E-U8
8027	2594	0.297E-09	0.131E-08
8075	2460	0.356E-06	0.211E-06
8524	2151	0.144E-06	0.578E-07
8681	1797	0.230E-06	0.932E-07
8695	2478	0.297E-05	0.293E-05
8806	2197	0.304E-06	0.389E-06
8877	2276	0.363E-06	0.175E-06
9063	2265	0.453E-06	0.154E-06
9082	2609	0.589E-06	0.724E-06
9323	2605	0.822E-08	0.530E-08
9406	2421	0.563E-06	0.261E-06
9461	2628	0.650E-06	0.357E-05
9470	1684	0.257E-06	0.283E-06
9513	2618	0.362E-06	0.134E-05
9786	2697	0.711E-07	0.155E-06
9893	2551	0.818E-07	0.698E-07

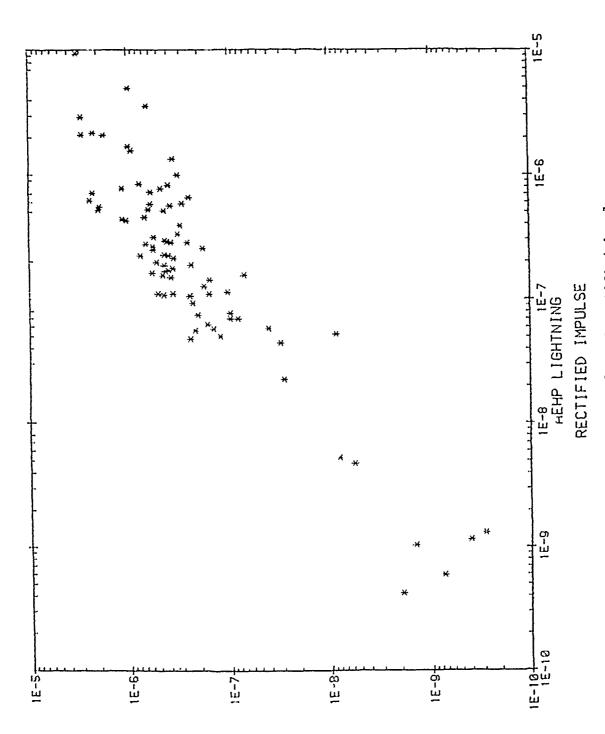


Figure A-7. Scatter plot of rectified impulse.

RECTIFIED IMPULSE

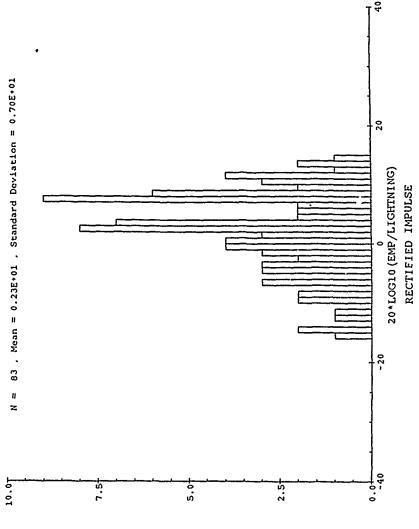


Figure A-8. Histogram of rectified impulse.

Number of Occurrences

Table A-5. Comparison of root action integrals.

TEST POINT	SHOT Number	ROOT ACTION INTEGRAL EMP	ROOT ACTION INTEGRAL LIGHTNING
0059	2276	0.255E-03	0.186E-03
0141	2662	0.643E-06	0.287E-06
0434	2502	0.244E-02	0.109E-02
0504	1680	0.174E-03	0.947E-04
0516	2615	0.273E-03	0.486E-03
0594	2584	0.141E-05	0.284E-06
0643	2261	0.279E-03	0.808E-04
0705	2535	0.803E-03	0.817E-03
0715	1798	0.934E-04	0.251E-04
0723	2256	0.170E-02	0.415E-03
0903	1428	0.658E-05	0.262E-04
0918	2550	0.298E-03	0.284E-03
1182	1159	0.524E-03	0.224E-03
1473	1779	0.184E-03	0.400E-04
1660	2545	0.253E-03	0.618E-04
2238	2154	0.977E-04	0.599E-04
2391	1734	0.289E-03	0.101E-03
2426	1306	0.332E-03	0.662E-04
2717	2560	0.848E-03	0.413E-03
2866	2274	0.205E-02	0.482E-03
3313	2521	0.403E-03	0.134E-03
3313	2689	0.321E-03	0.158E-03
3385	1718	0.152E-03	0.609E-04
3473	2607	0.686E-03	0.809E-03
3539	2727	0.808E-03	0.246E-03
3543	2265	0.363E-03	0.672E-04
3615	1675	0.235E-03	0.296E-03
3626 3795	2531 2281	0.517E-03 0.207E-03	0.111E-03
3884	2255	0.207E-03 0.191E-02	0.125E-03
3919	1156	0.191E-02 0.289E-02	0.469E-03 0.505E-02
4050	1680	0.128E-03	0.555E-04
4225	2671	0.128E-03 0.437E-05	0.555E-04 0.245E-05
4309	2653	0.437E-03 0.116E-03	0.245E-05 0.729E-04
4597	2436	0.338E-03	0.729E-04 0.257E-03
4859	2144	0.117E-03	0.237E-03 0.333E-04
4914	2217	0.267E-03	0.112E-03
4924	2645	0.343E-03	0.112E-03 0.390E-03
5169	2588	0.310E-03	0.940E-04
5283	1717	0.182E-03	0.318E-03
5352	1234	0.986E-04	0.384E-04

Table A-5. Comparison of root action integrals (Concluded)

TEST POINT	SHOT Number	ROOT ACTION INTEGRAL EMP	ROOT ACTION INTEGRAL LIGHTNING
5393	2623	0.967E-03	0.260E-02
5415	2700	0.349E-03	0.401E-03
5511	2274	0.575E-03	0.134E-03
5524	2584	0.364E-06	0.556E-06
5584	2687	0.552E-03	0.264E-03
5611	2308	0.452E-04	0.297E-04
5611	2501	0.259E-04	0.219E-04
5727	1180	0.836E-04	0.371E-04
5737	2165	0.203E-03	0.389E-04
5813	2606	0.481E-03	0.287E-03
5869	2271	0.185E-02	0.110E-02
6369	2584	0.242E-04	0.113E-04
6381	1151	0.289E-03	0.141E-03
6482	2501	0.176E-03	0.299E-04
6562	2501	0.927E-03	0.278E-03
6708	2712	0.302E-03	0.142E-03
6732	2712	0.688E-03	0.419E-03
7045	2260	0.171E-02	0.422E-03
7059	2226	0.360E-03	0.108E-03
7171	2504	0.355E-03	0.177E-03
7187	2266	0.362E-03	0.967E-04
7407	2166	0.459E-03	0.174E-03
7513	2638	0.289E-03	0.143E-03
7516	2528	0.153E-02	0.103E-02
7681	1720	0.163E-03	0.562E-04
7873 8027	2626	0.120E-05	0.511E-06
8075	2594 2460	0.213E-06 0.288E-03	0.653E-06
8524	2151	0.200E-03 0.118E-03	0.109E-03 0.321E-04
8681	1797	0.118E-03	0.521E-04 0.524E-04
8695	2478	0.183E-03 0.260E-02	0.145E-02
8806	2197	0.284E-03	0.145E-02 0.207E-03
8877	2276	0.204E=03 0.312E=03	0.925E-04
9063	2265	0.352E-03	0.923L-04 0.847E-04
9082	2609	0.469E-03	0.344E-03
9323	2605	0.435E-05	0.344E-05
9406	2421	0.372E-03	0.137E-03
9461	2628	0.469E-03	0.171E-02
9470	1684	0.155E-03	0.166E-03
9513	2618	0.290E-03	0.648E-03
9786	2697	0.694E-04	0.796E-04
9893	2551	0.775E-04	0.346E-04

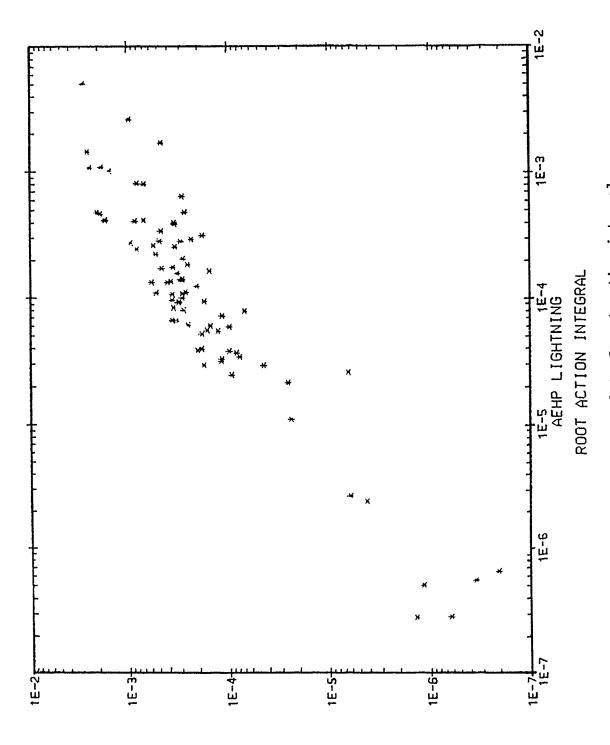


Figure A-9. Scatter plot of root action integral.

ROOT ACTION INTEGRAL

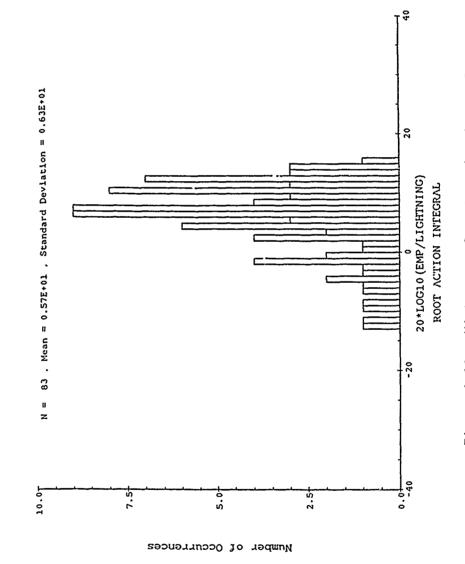
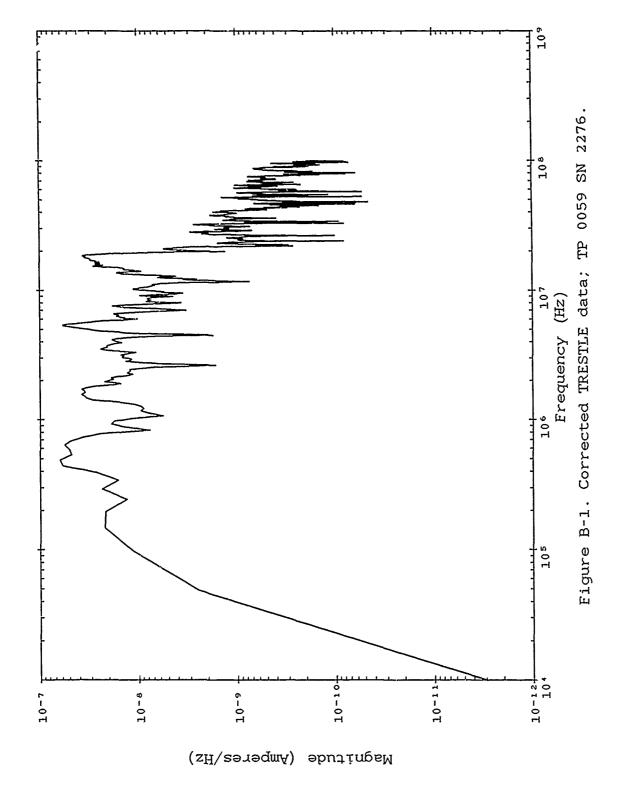
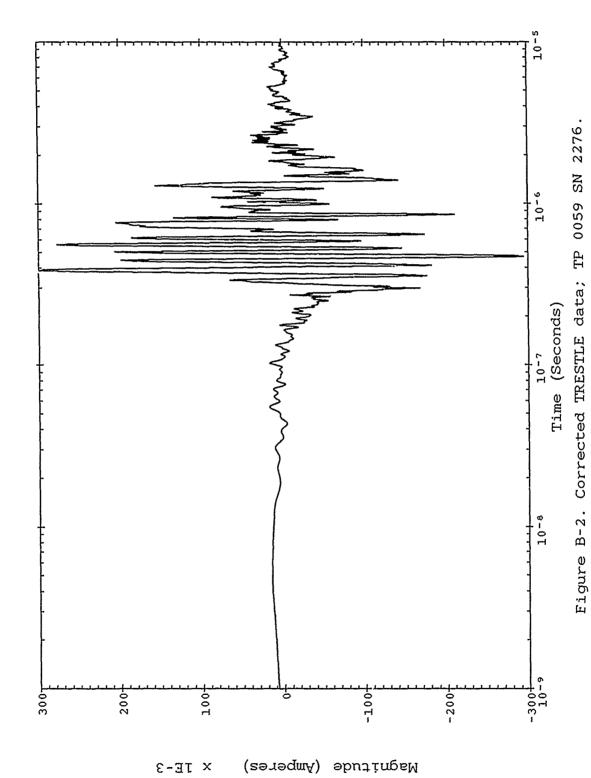
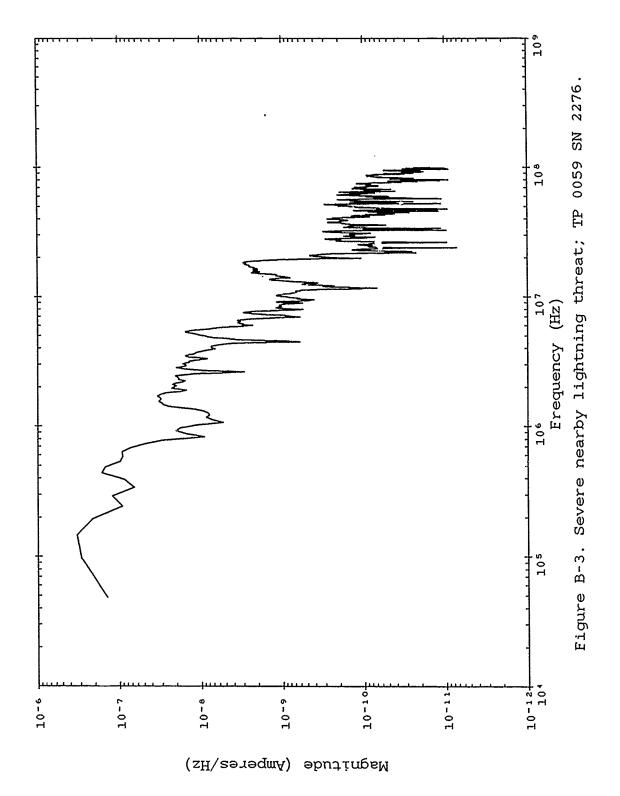


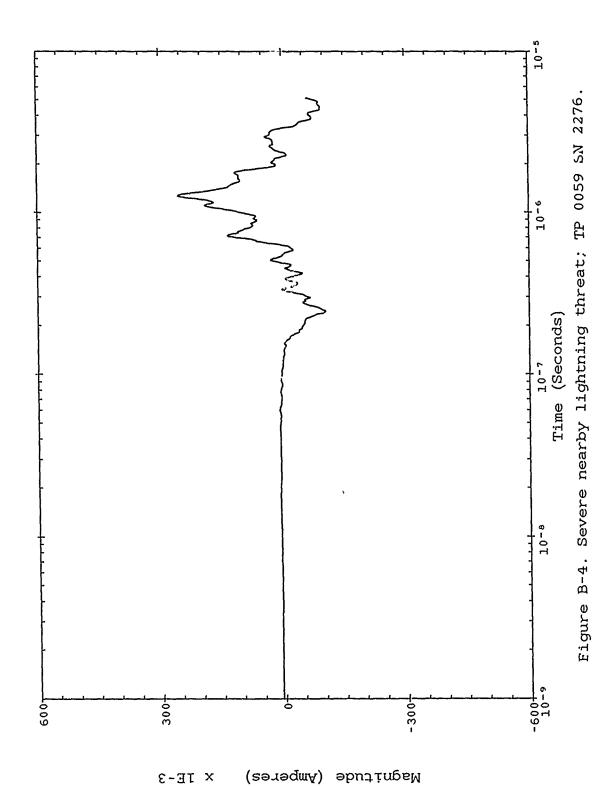
Figure A-10. Histogram of root action integral.

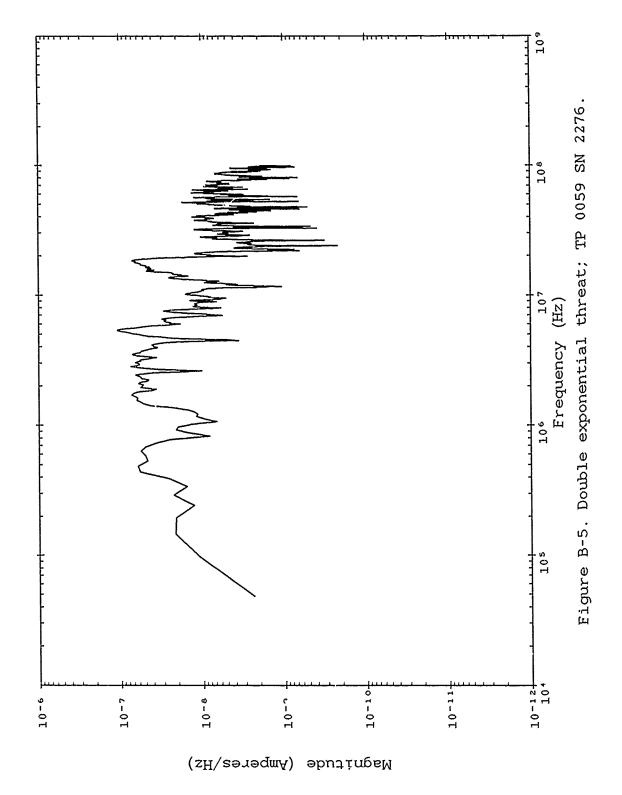
APPENDIX B
DATA PLOTS

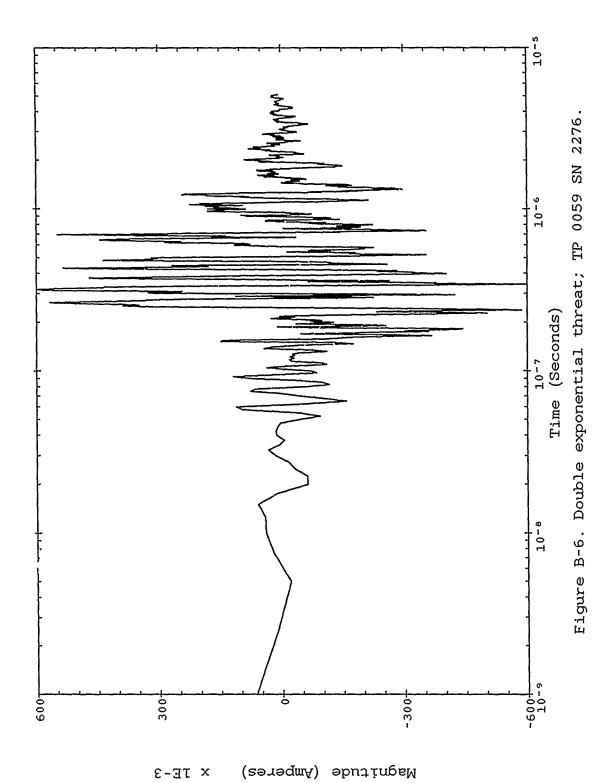


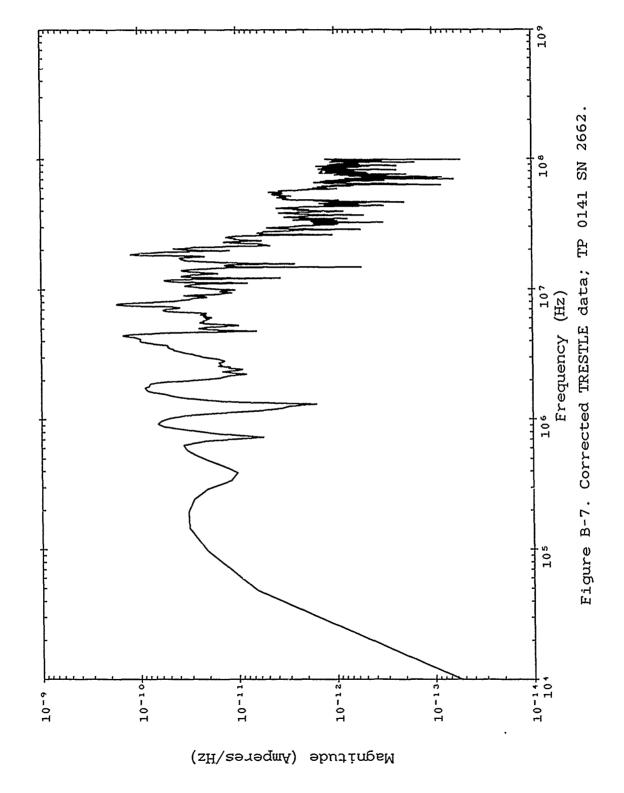


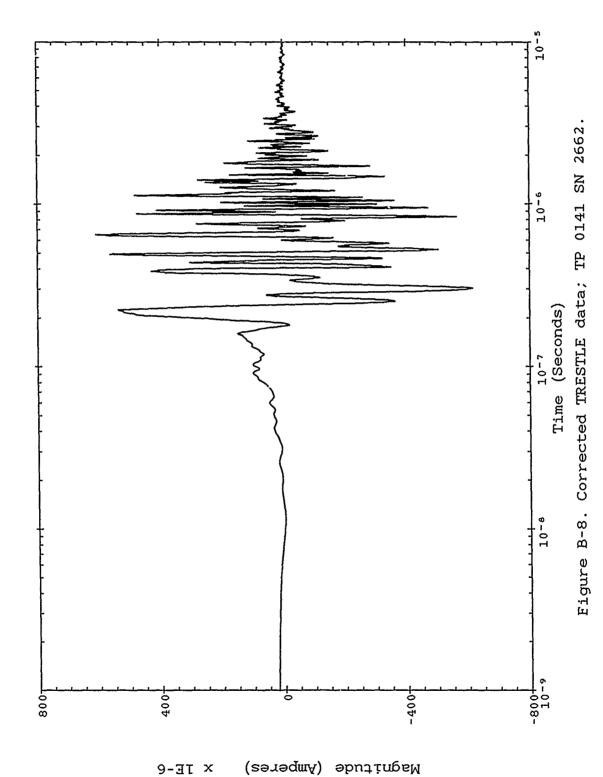


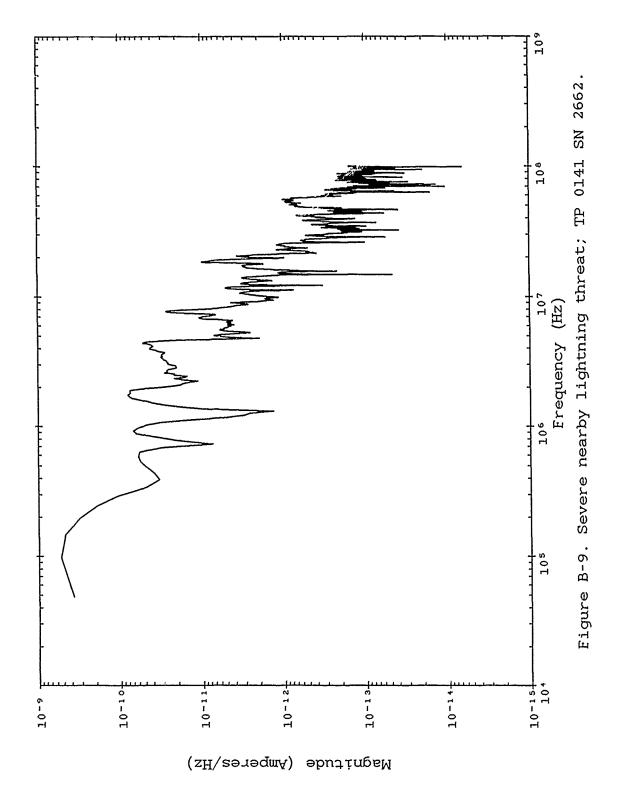


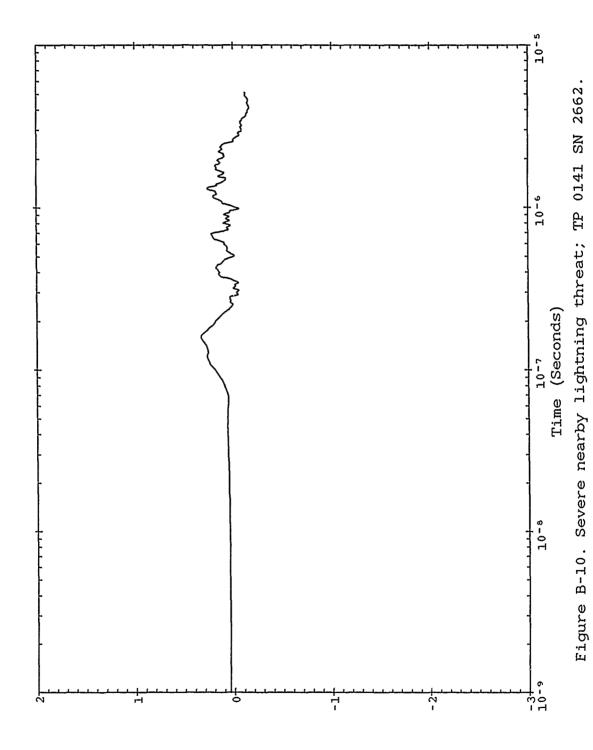






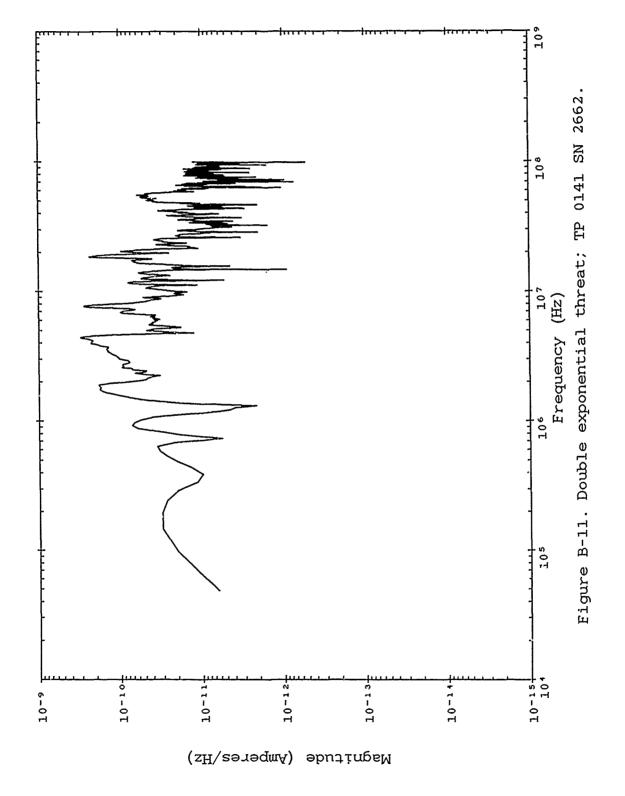


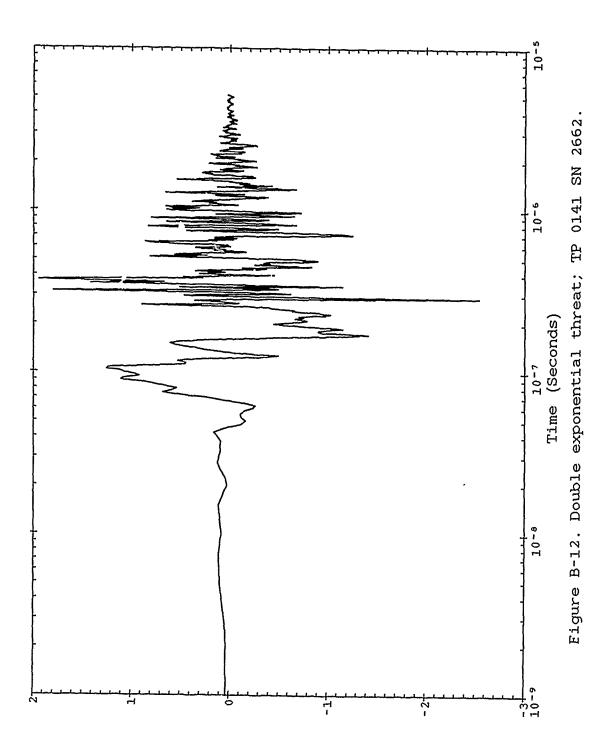




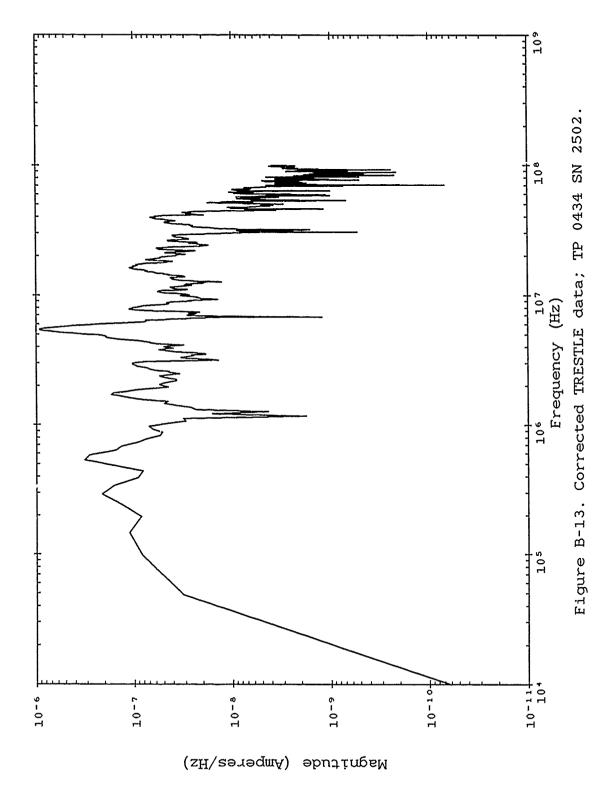
Magnitude (Amperes)

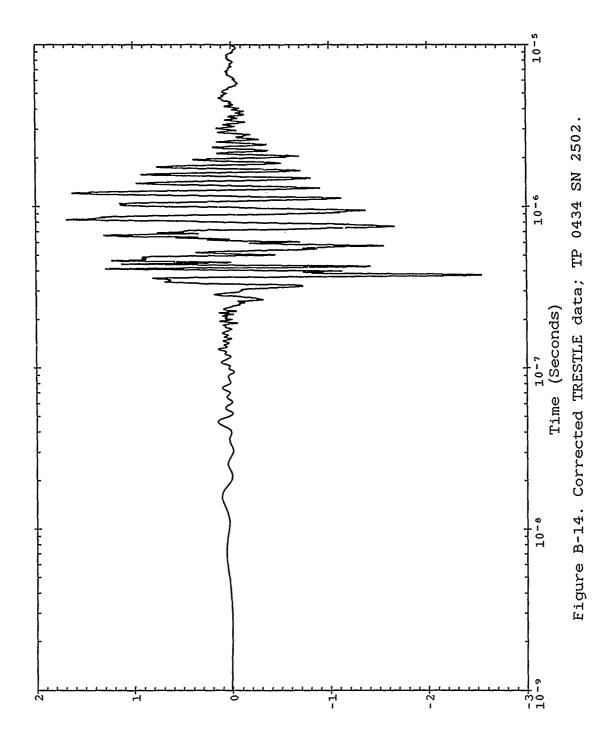
× TE-3

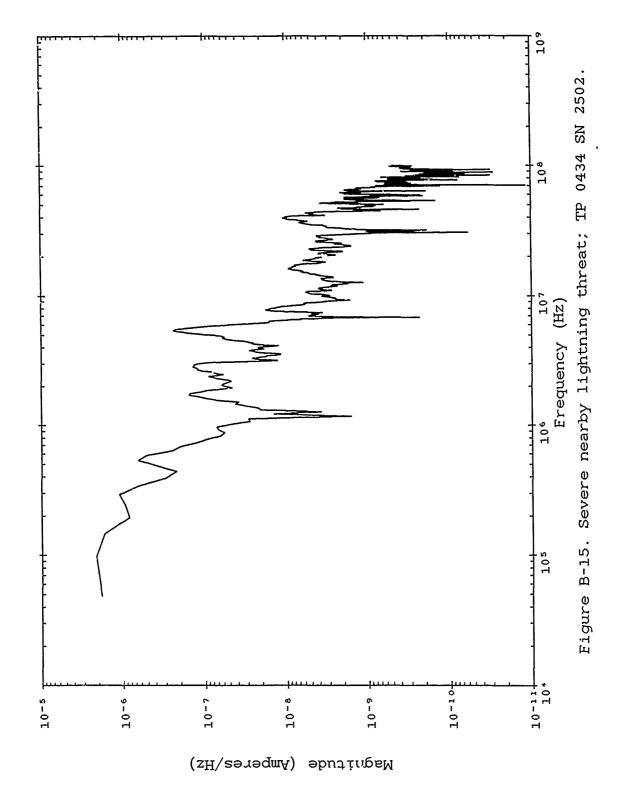


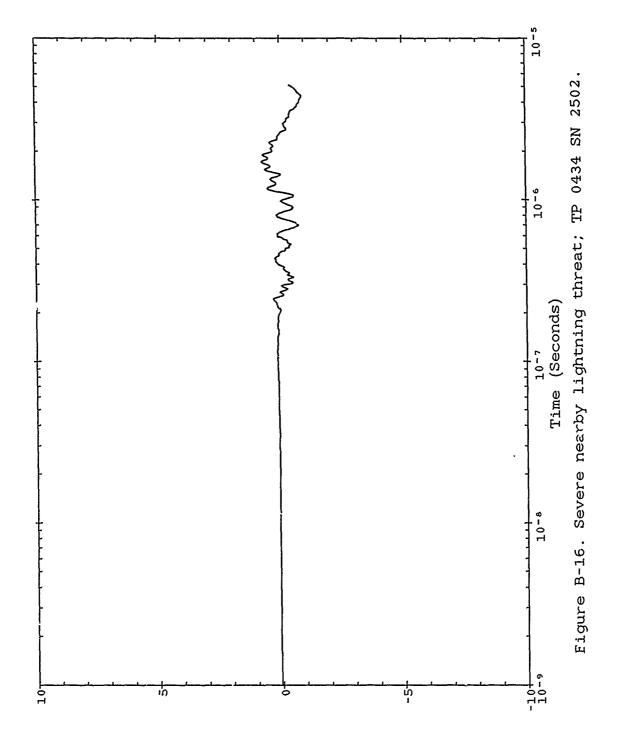


Wagnitude (Amperes) \times 1E-3

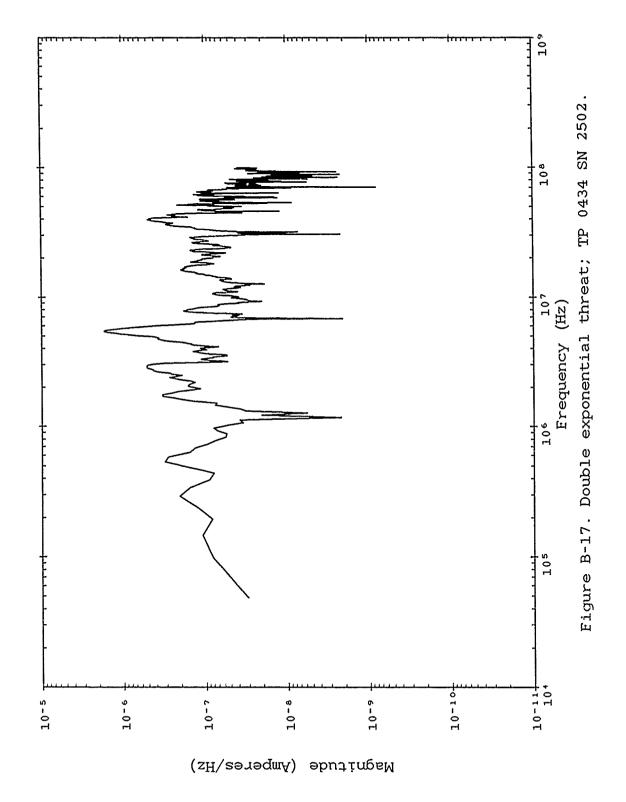


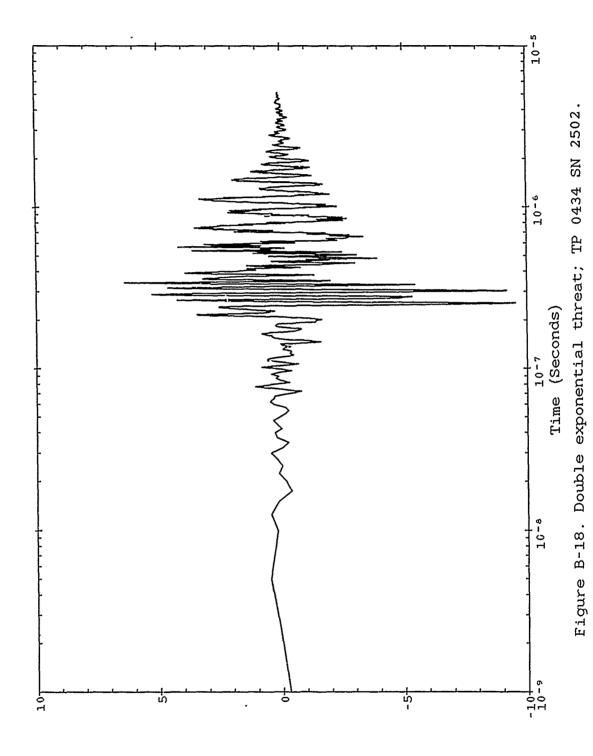




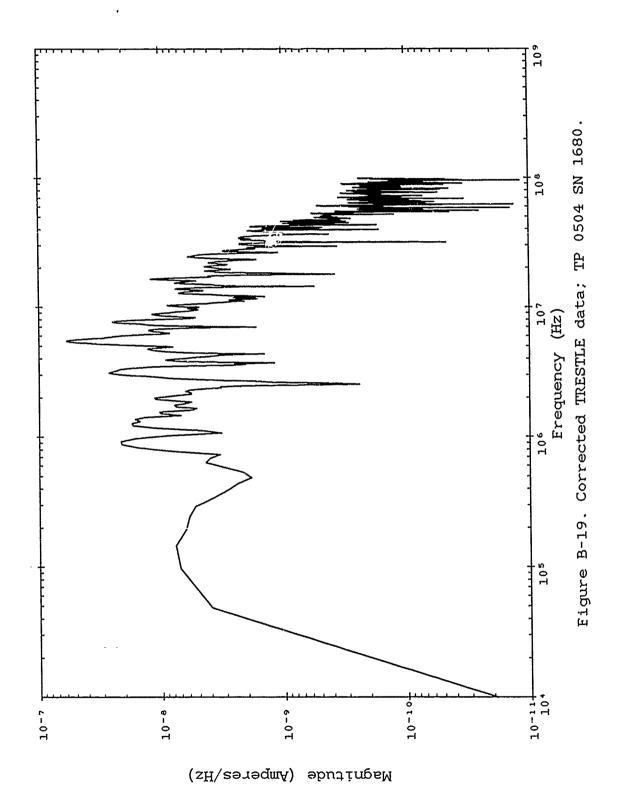


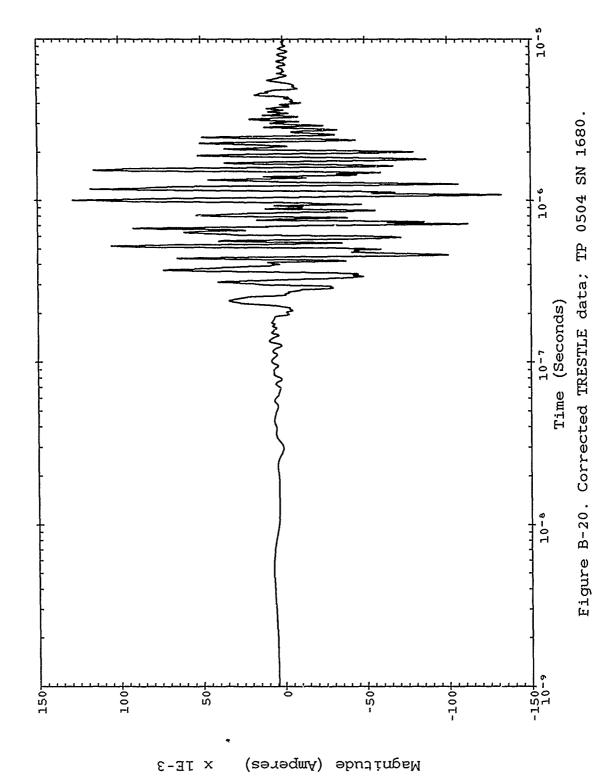
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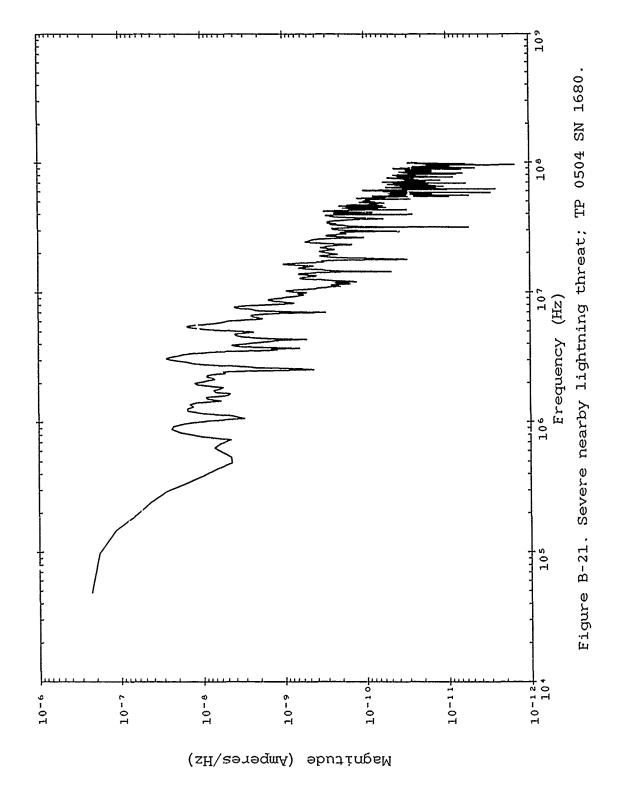


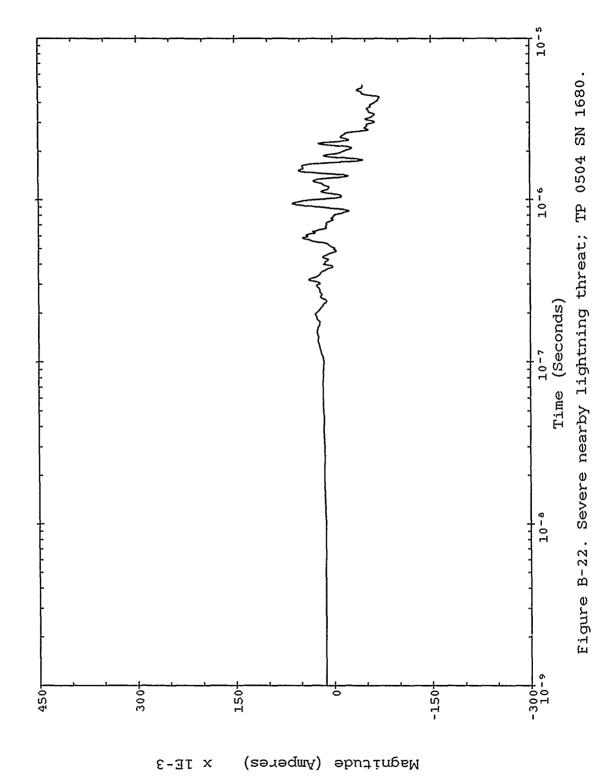


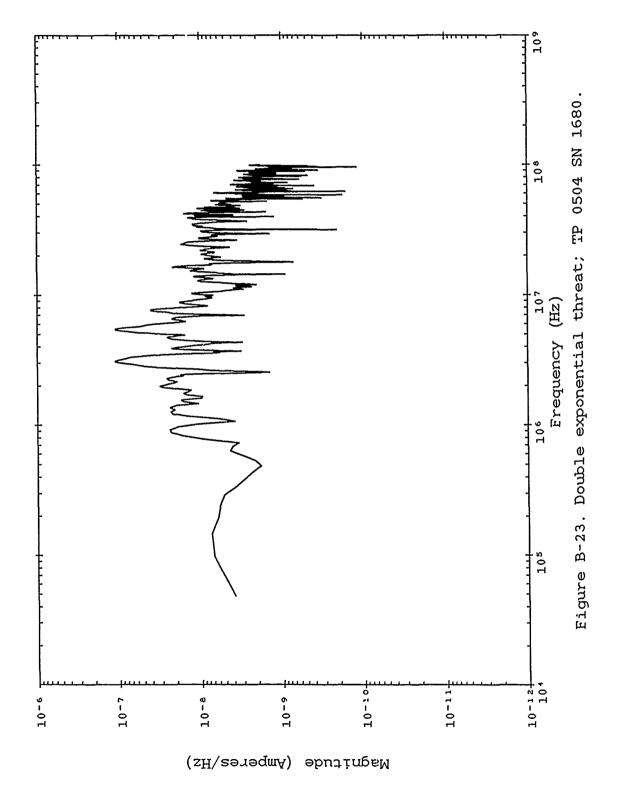
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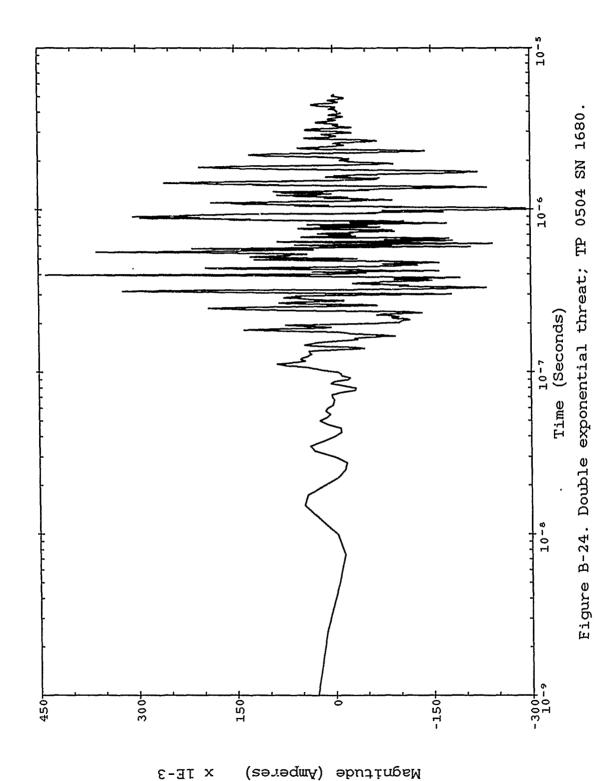


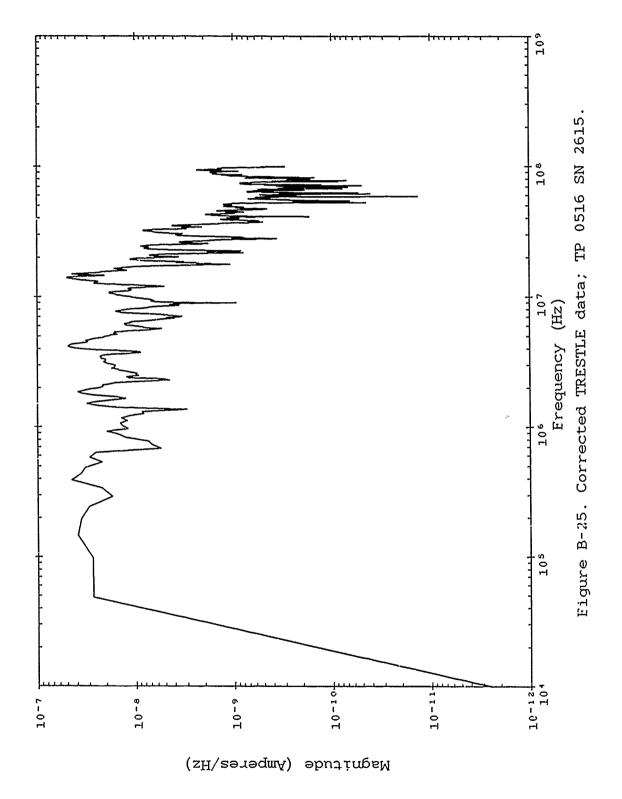


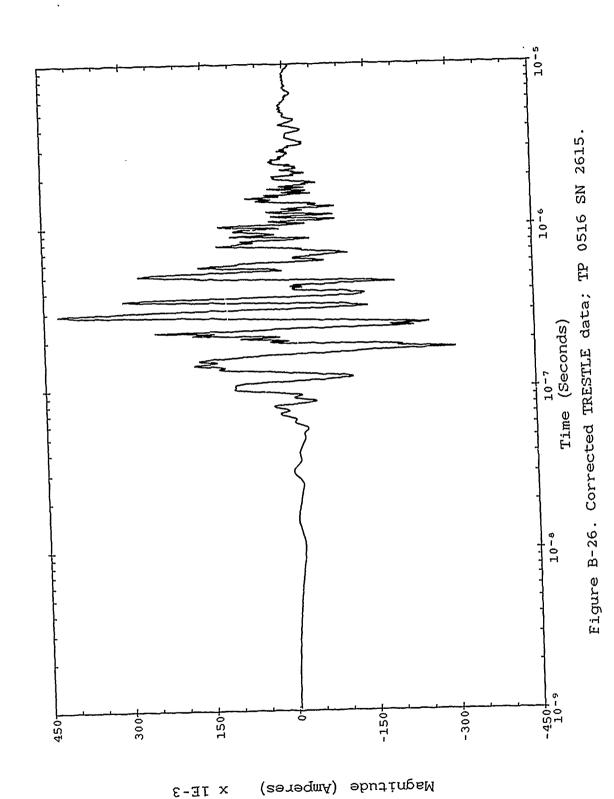


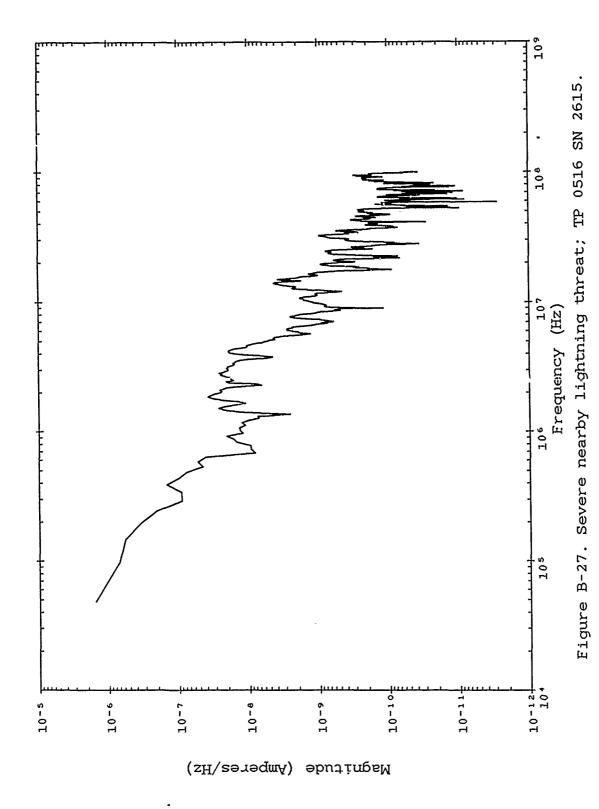


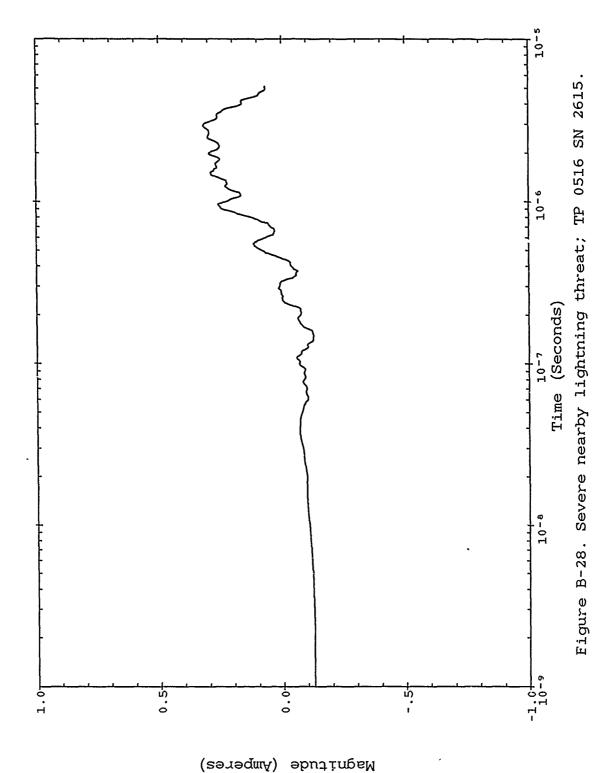


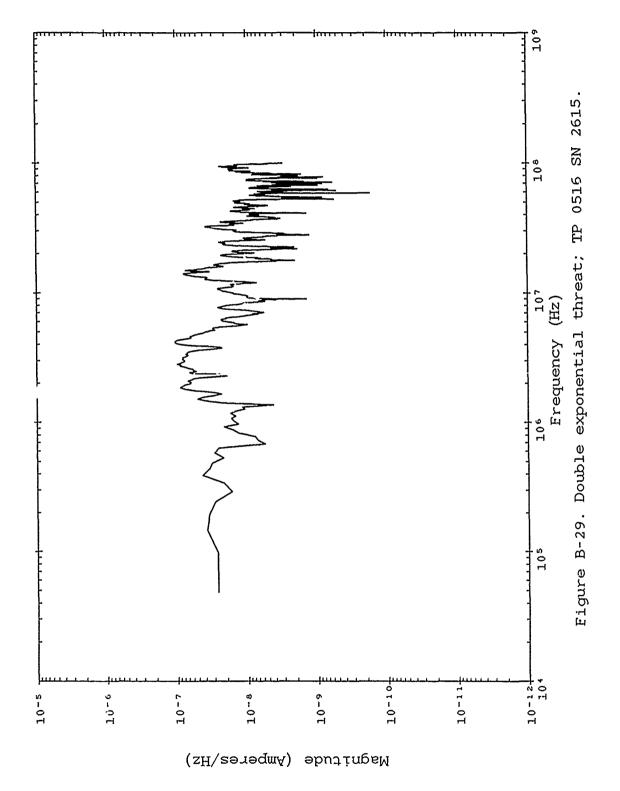


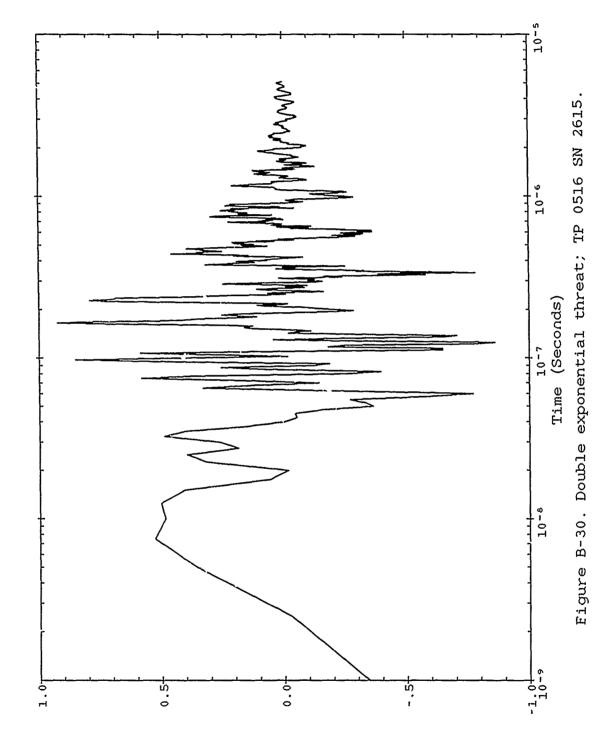




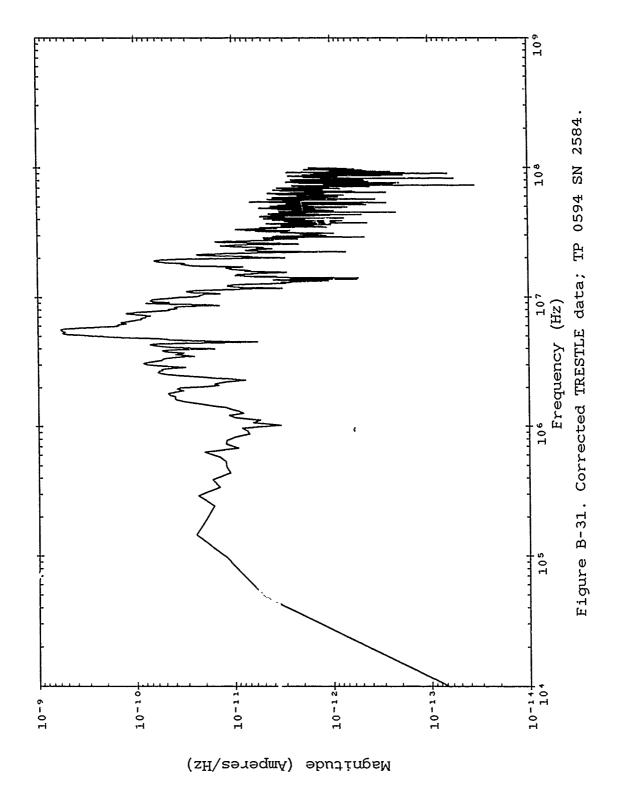


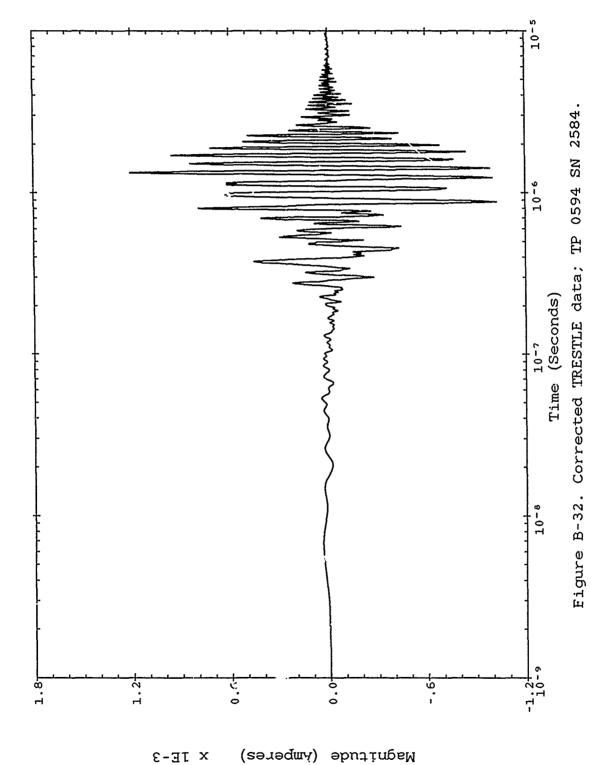


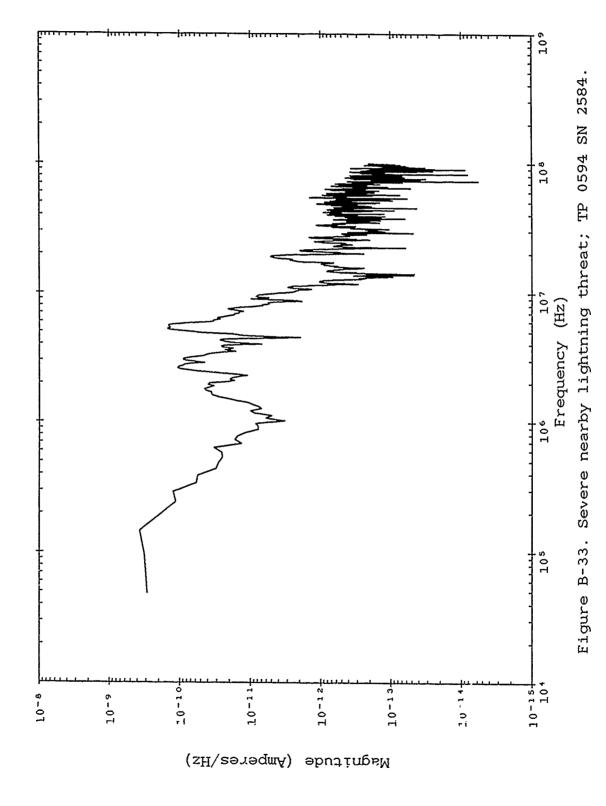


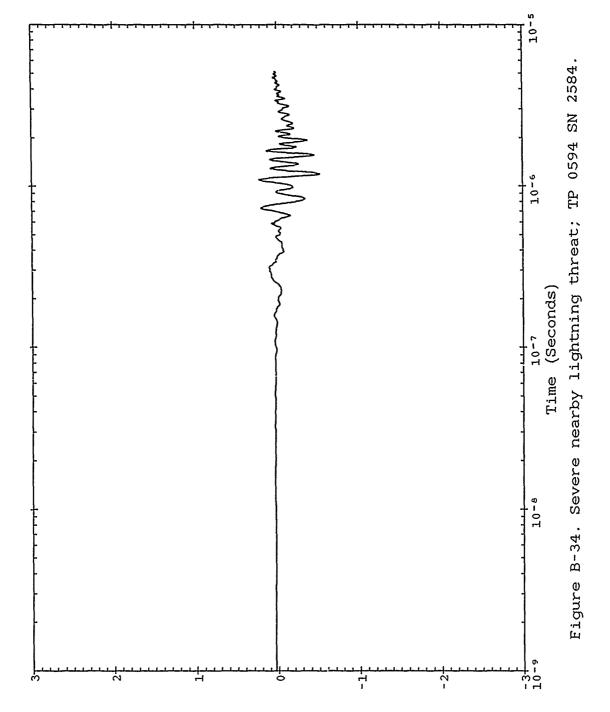


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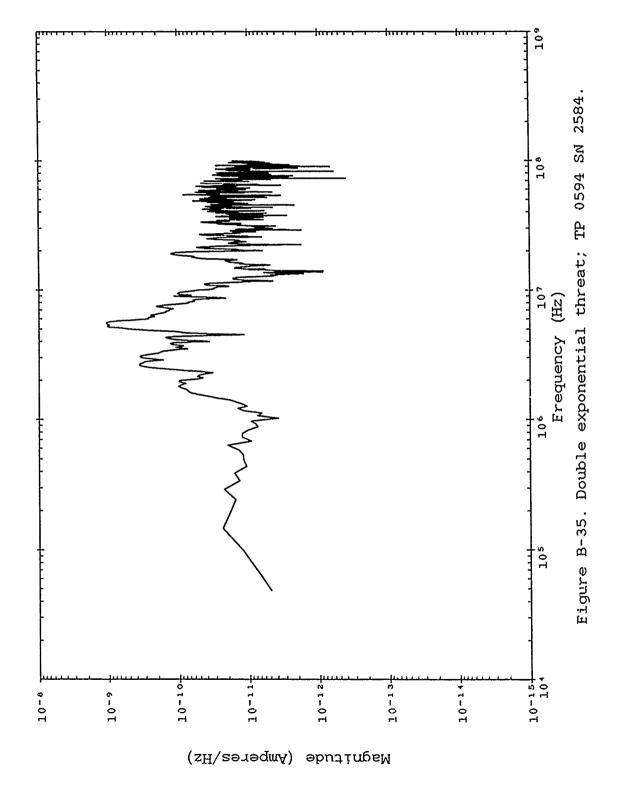


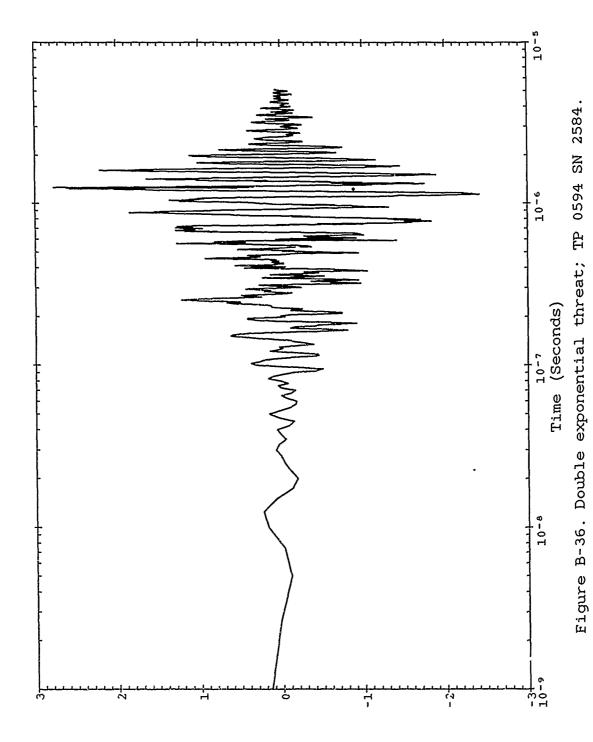




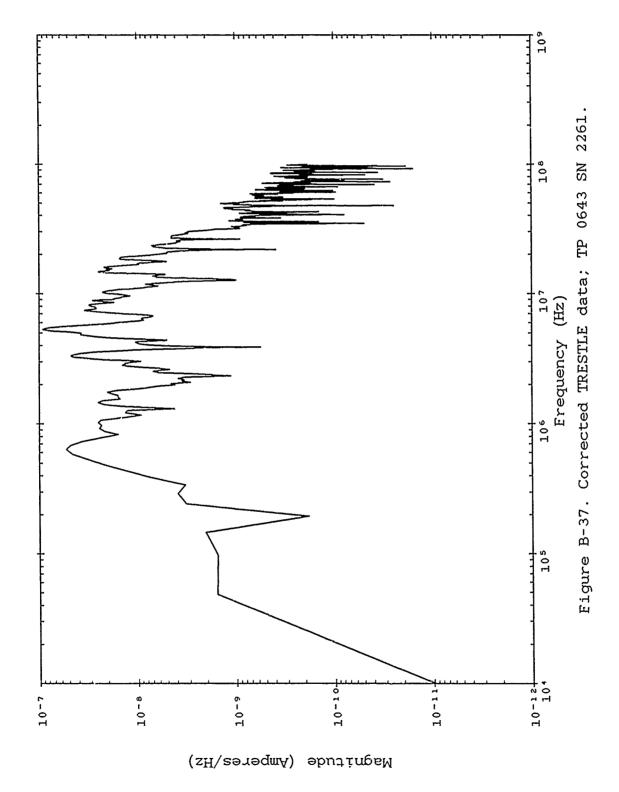
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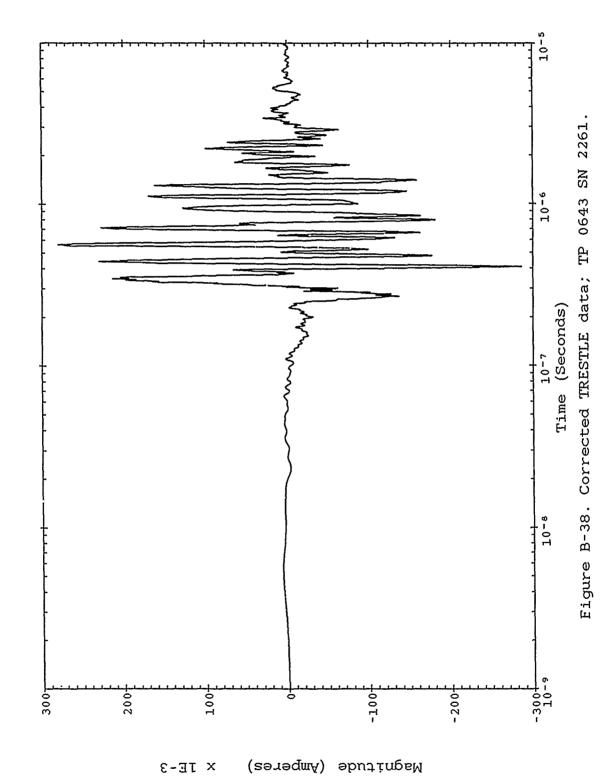
x TE-3

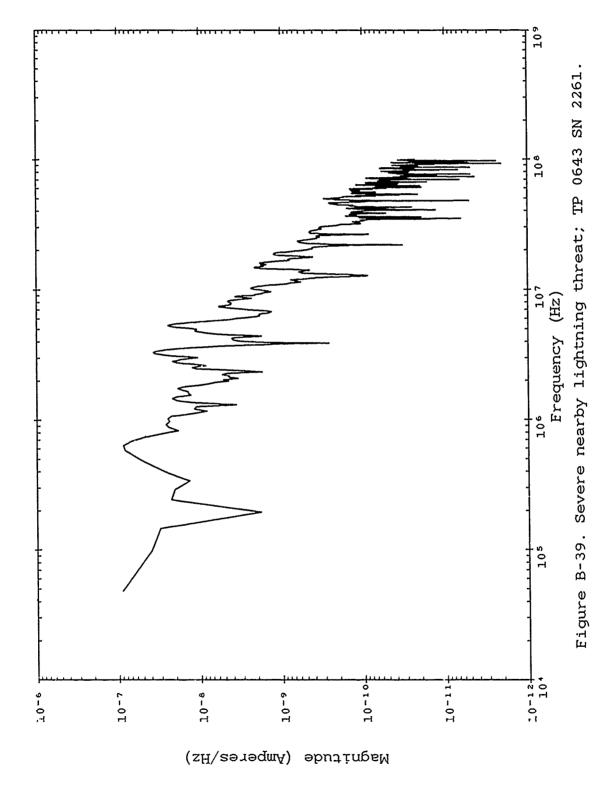




Wagnitude (Amperes) x 1E-3

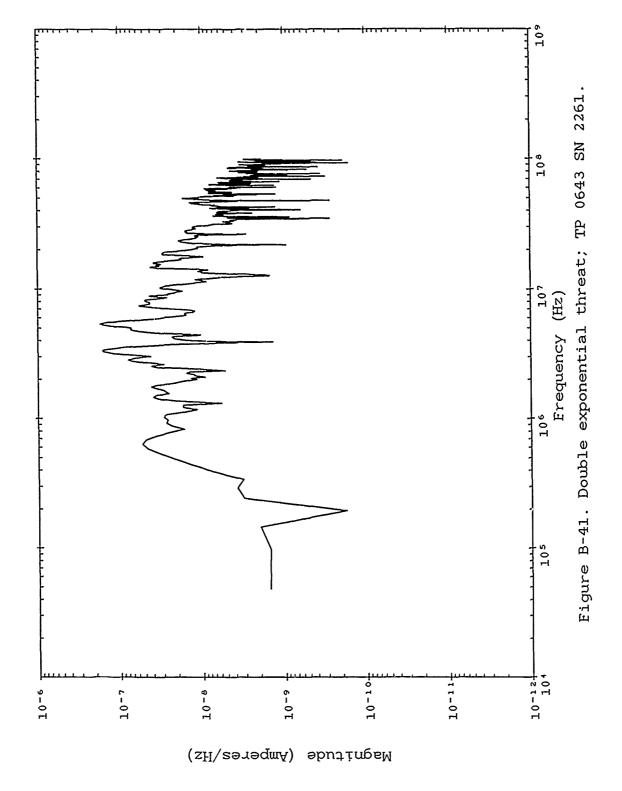


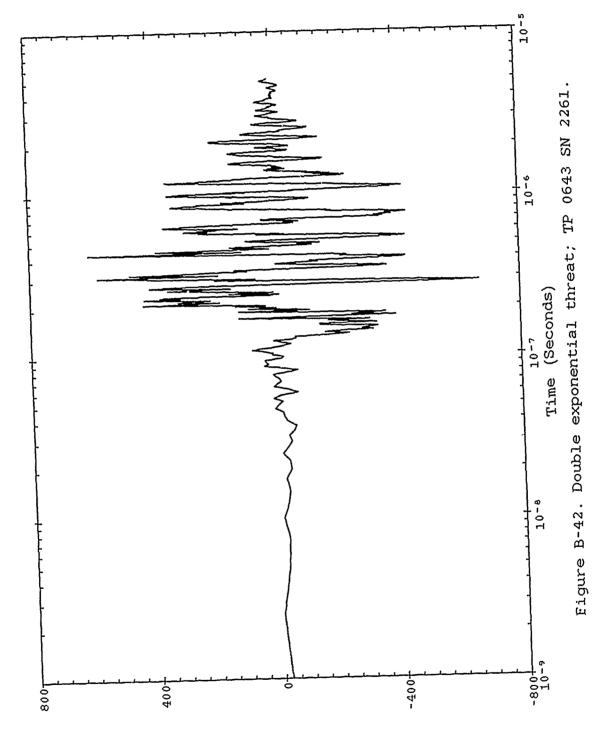


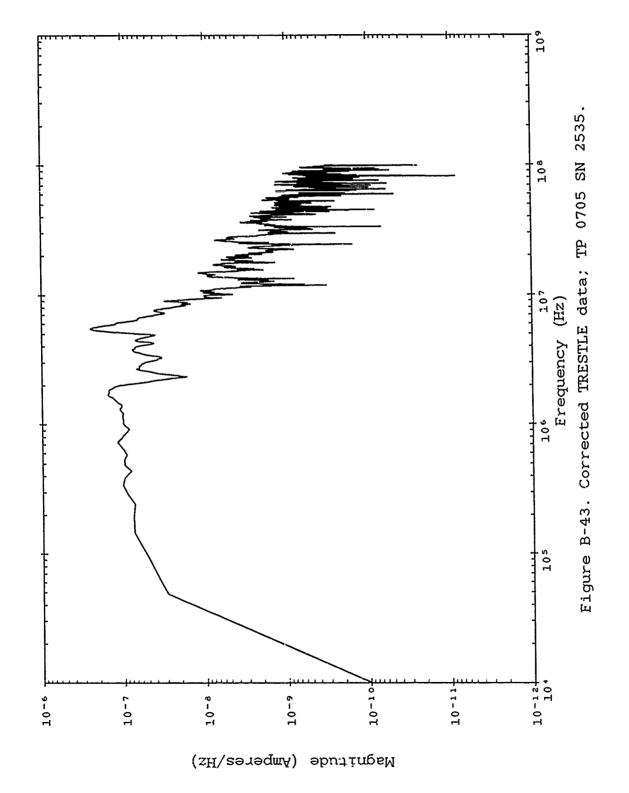


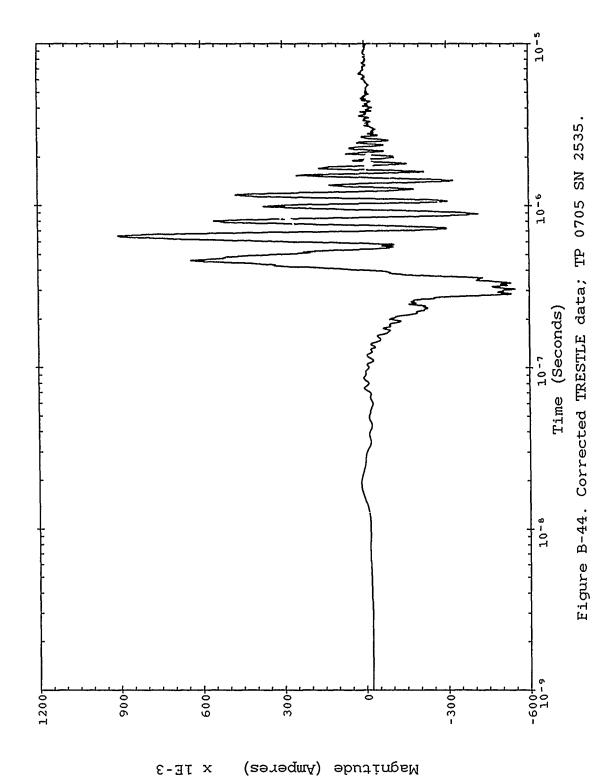
Magnitude (Amperes)

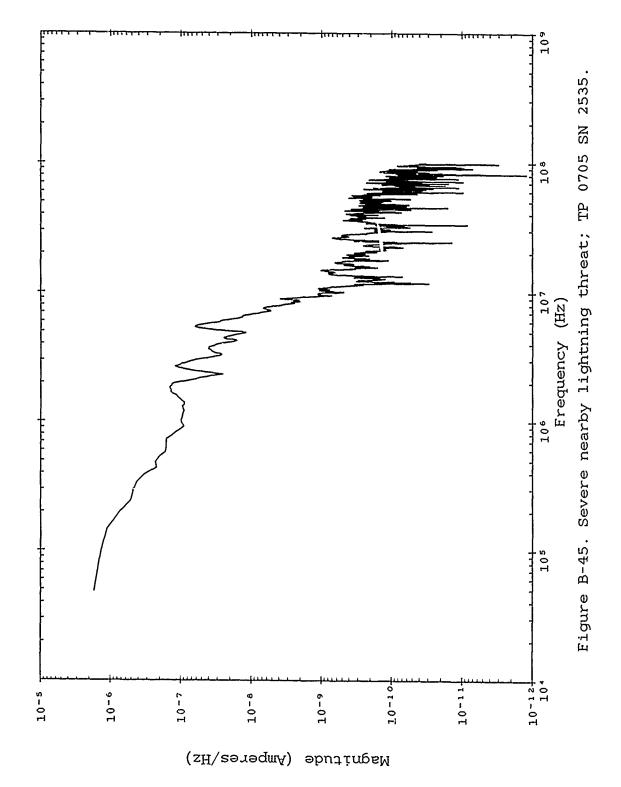
× TE-3

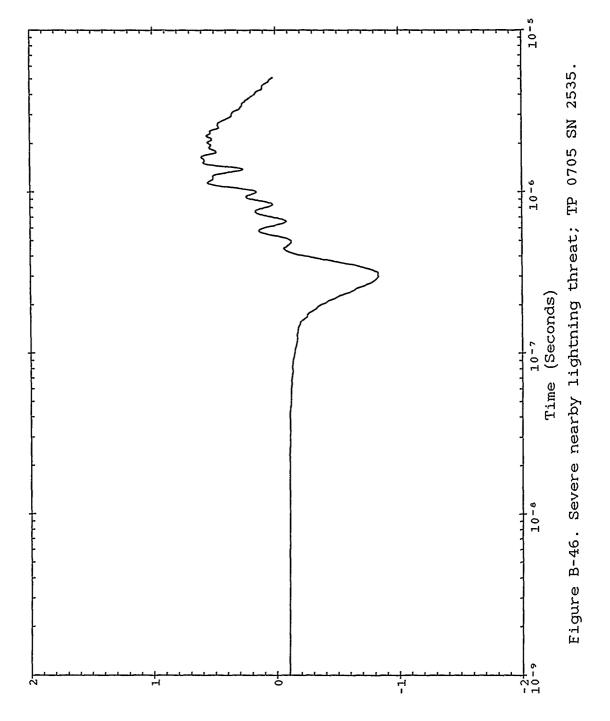




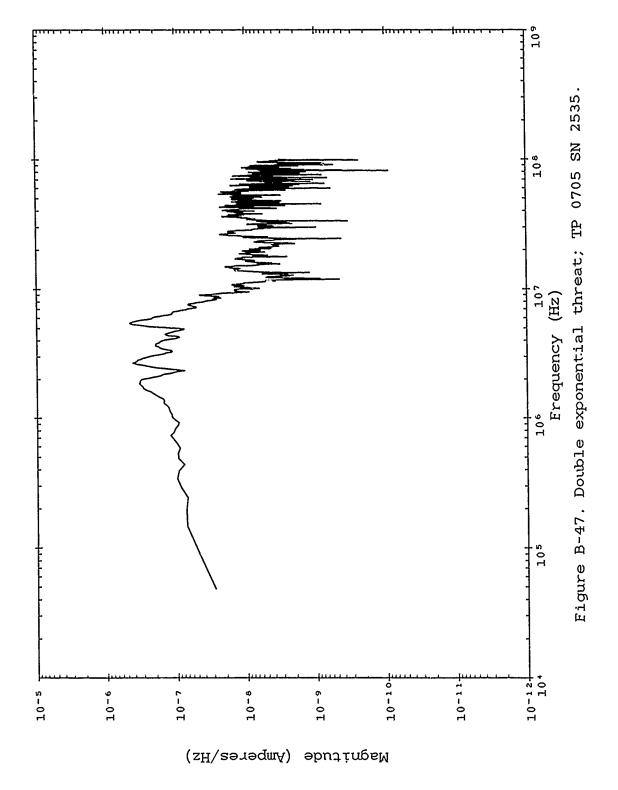


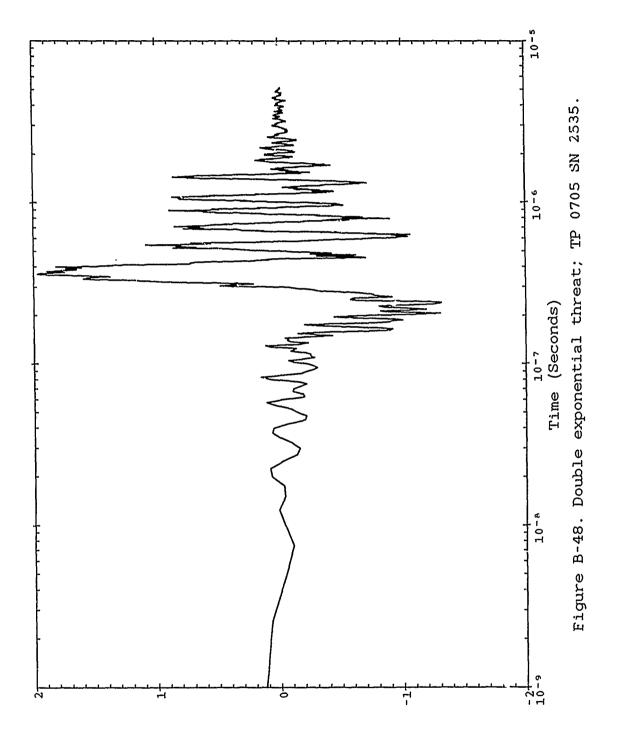




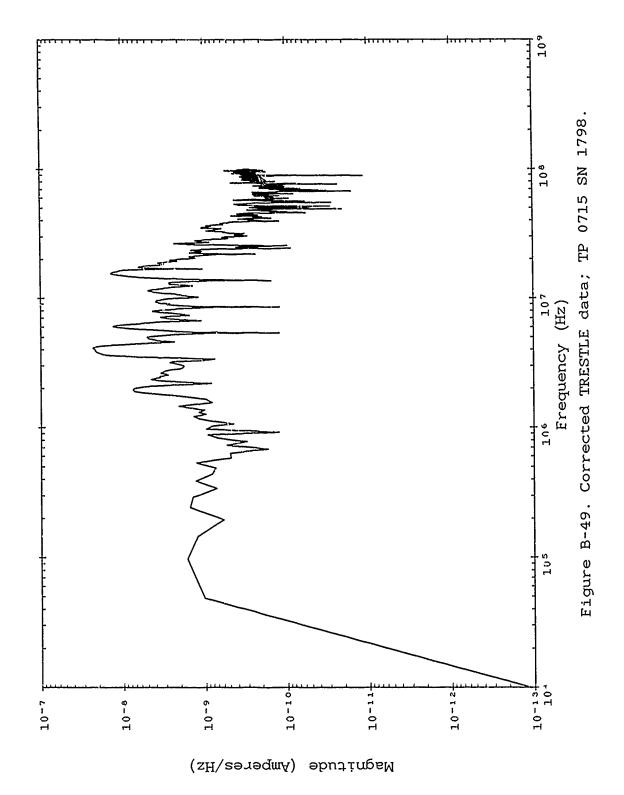


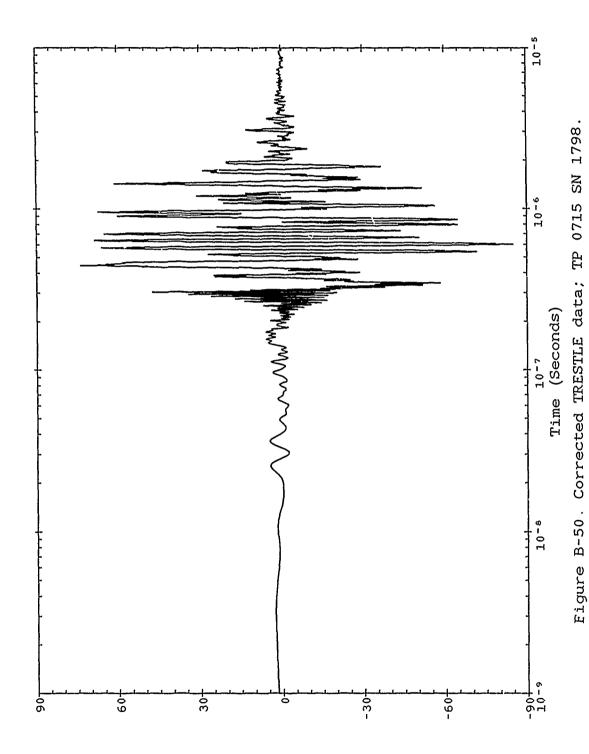
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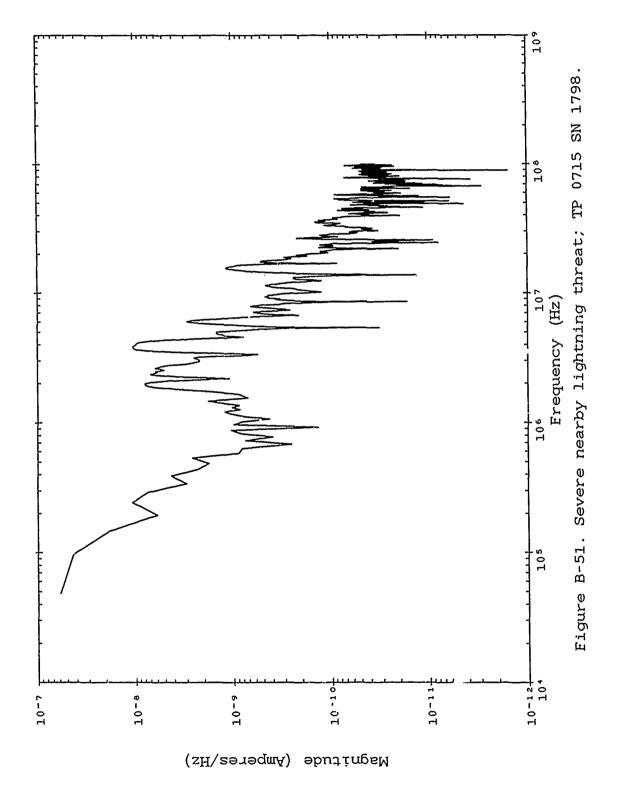


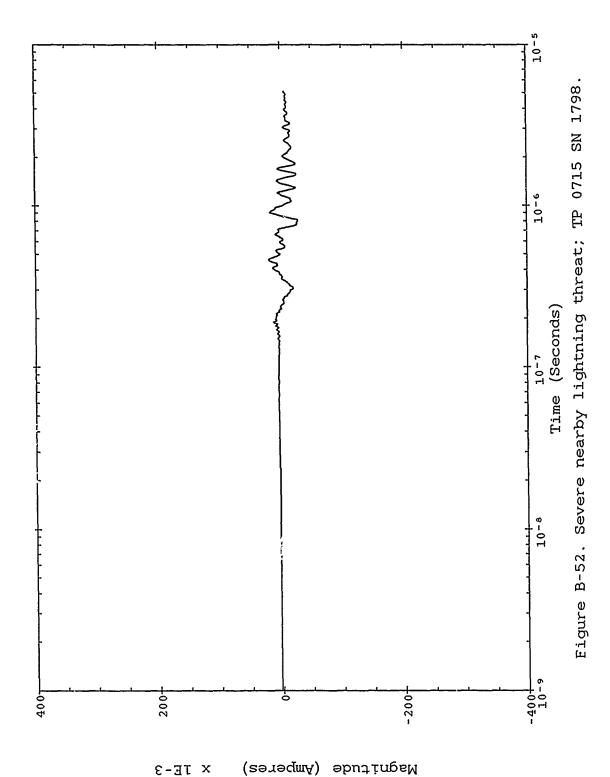
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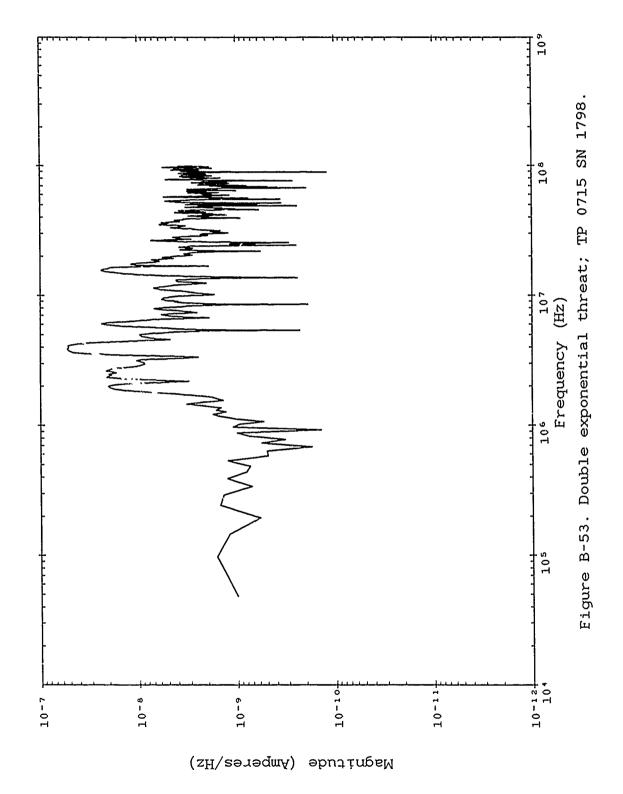


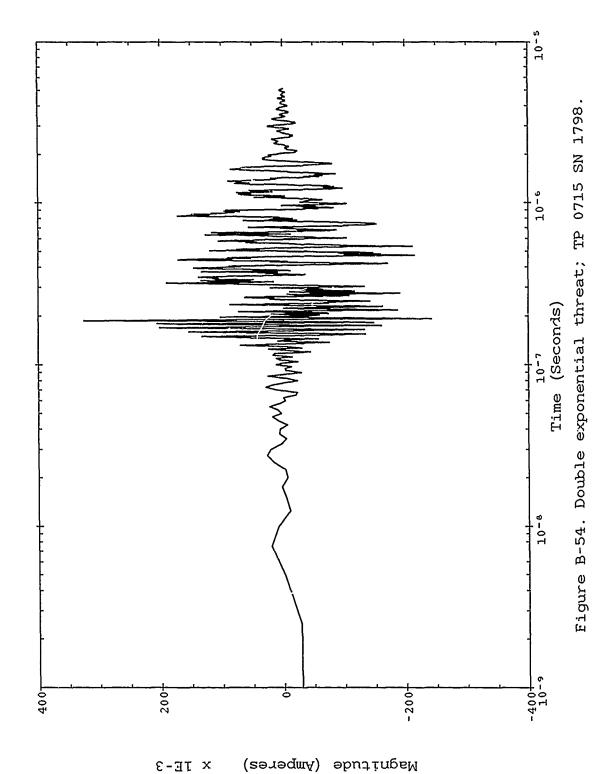
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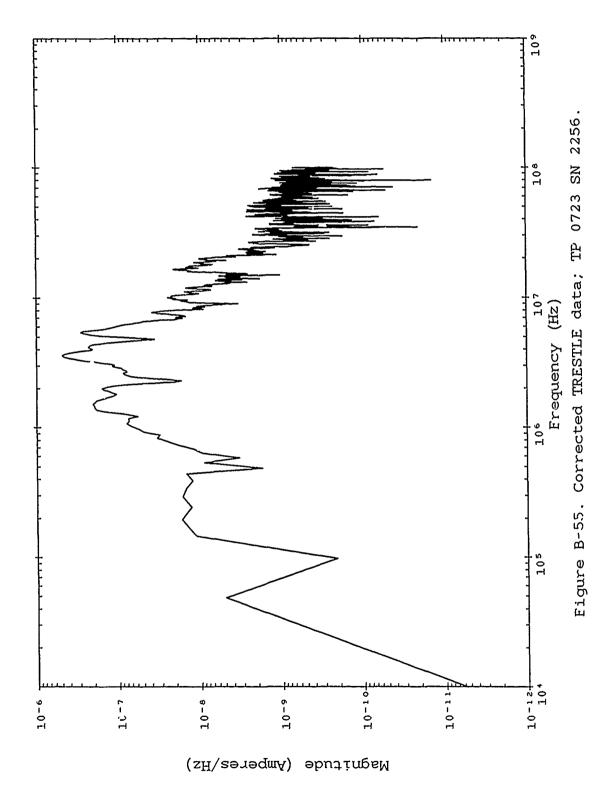


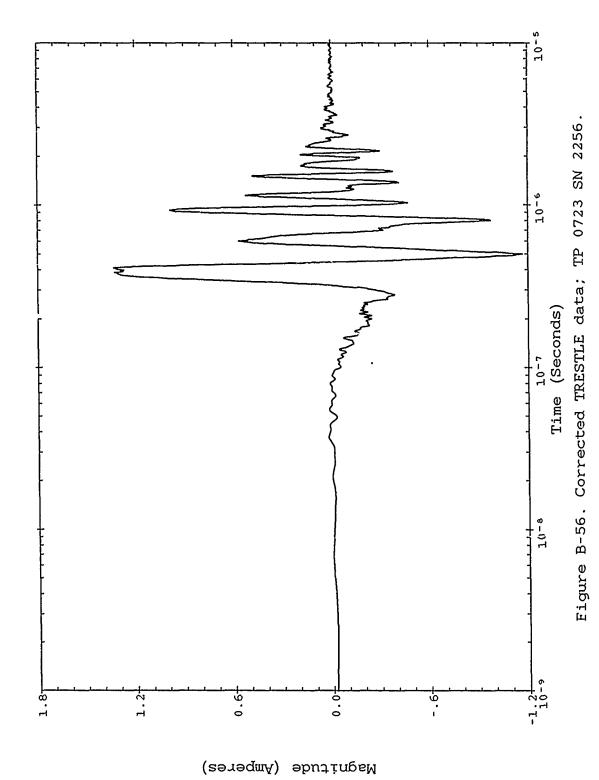


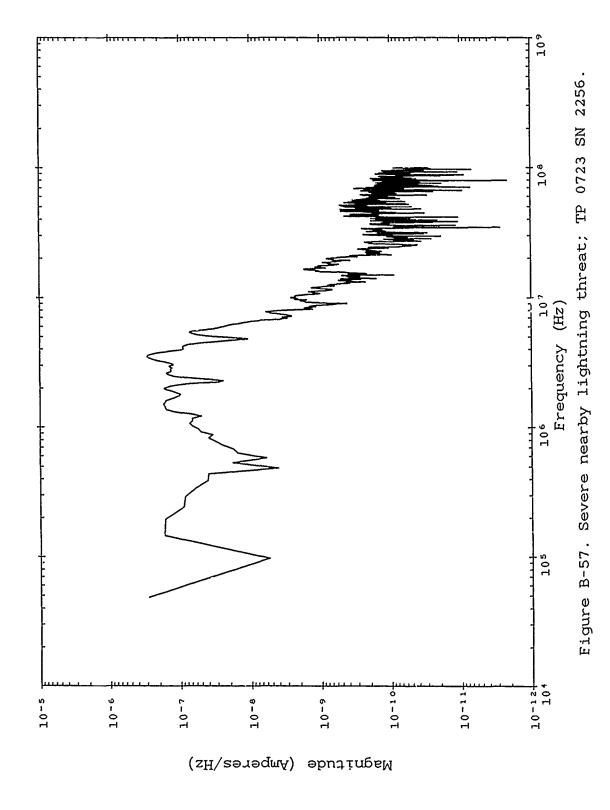
x JE-3

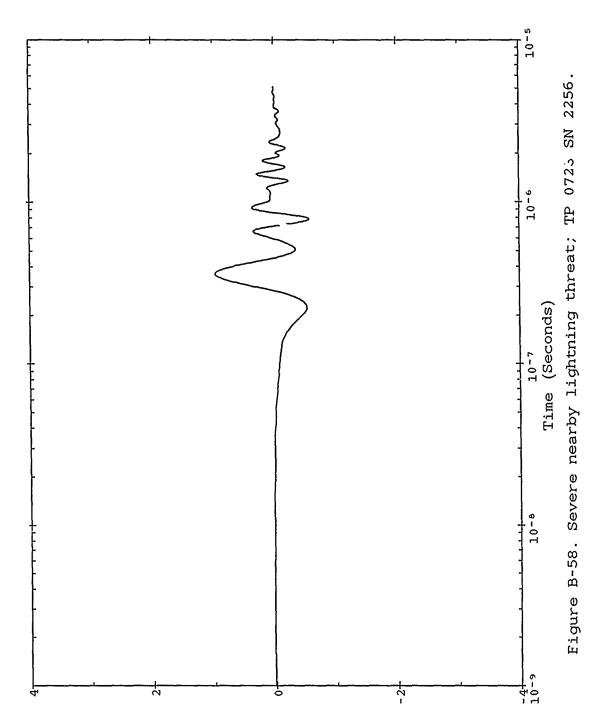




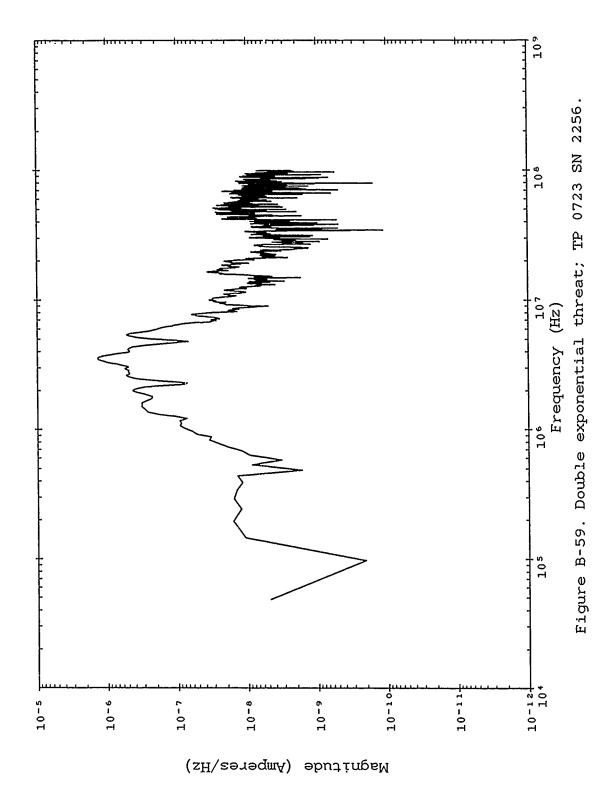


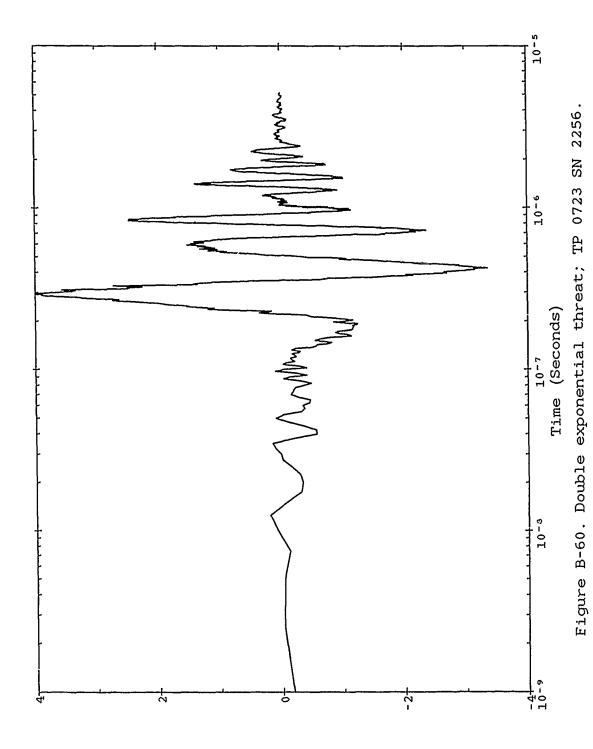




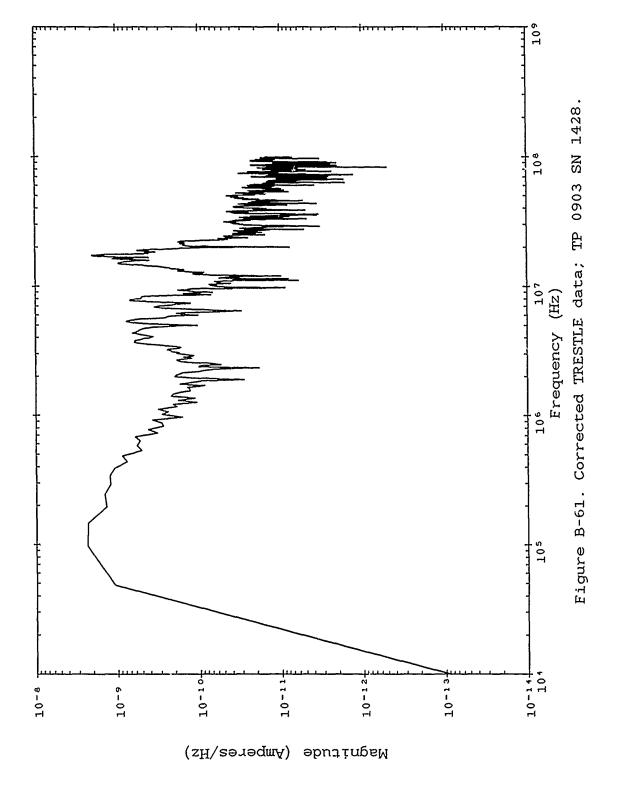


Magnitude (Amperes)





Magnitude (Amperes)



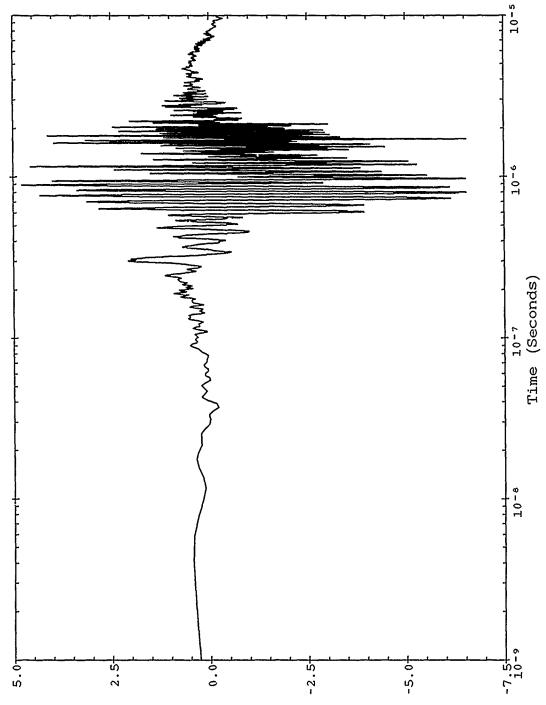
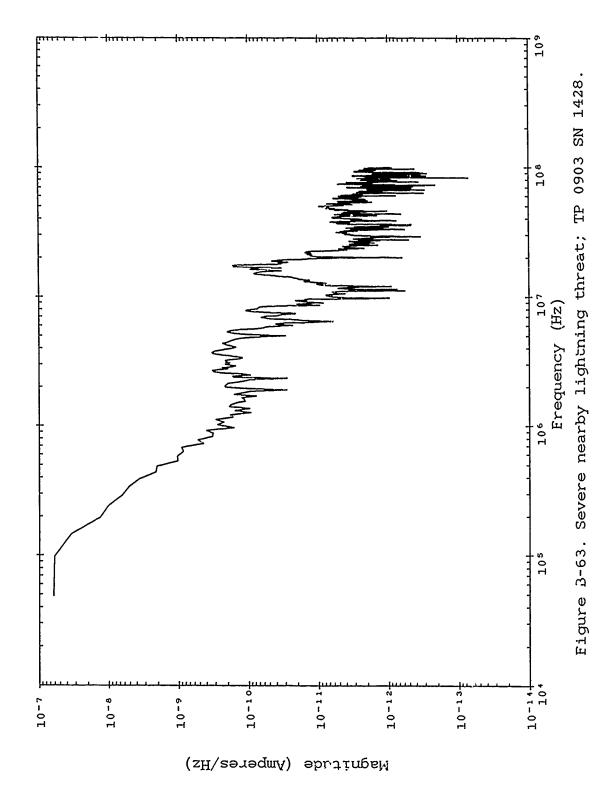
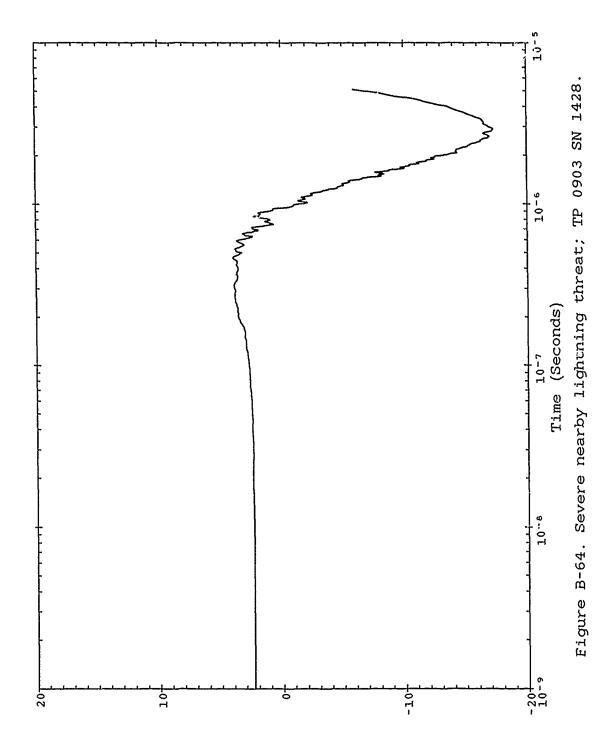


Figure B-62. Corrected TRESTLE data; TP 0903 SN 1428.

Magnitude (Amperes)

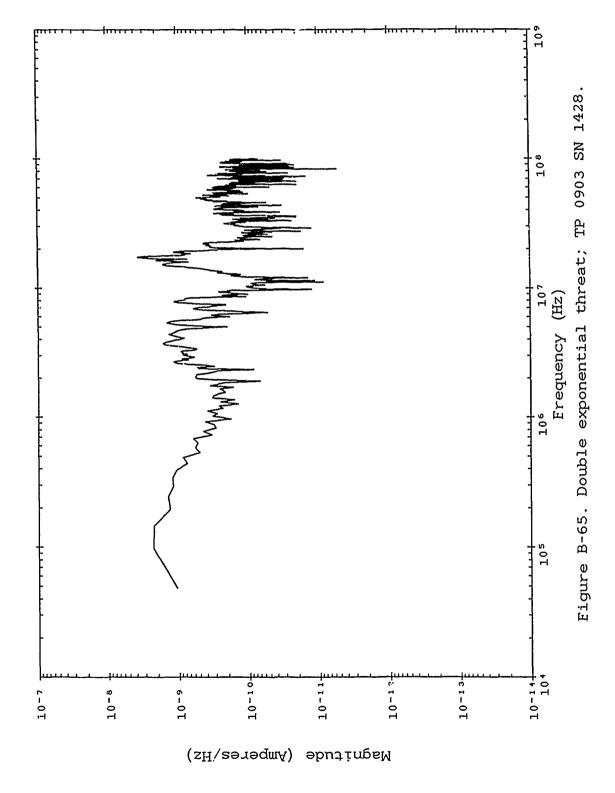
× TE-3

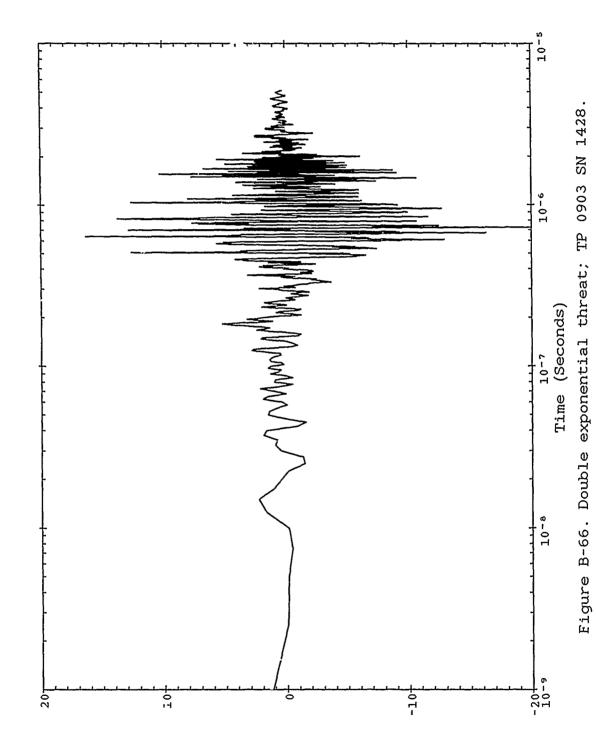




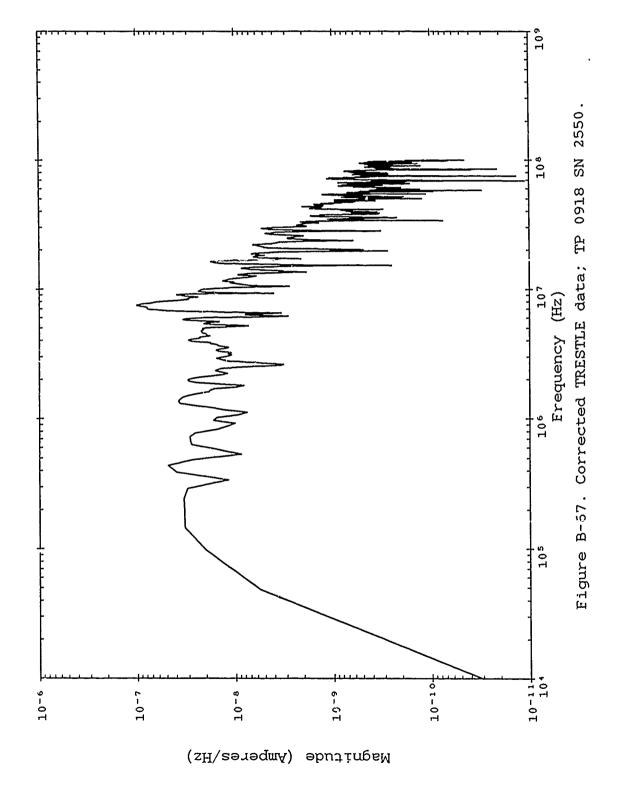
Magnitude (Amperes)

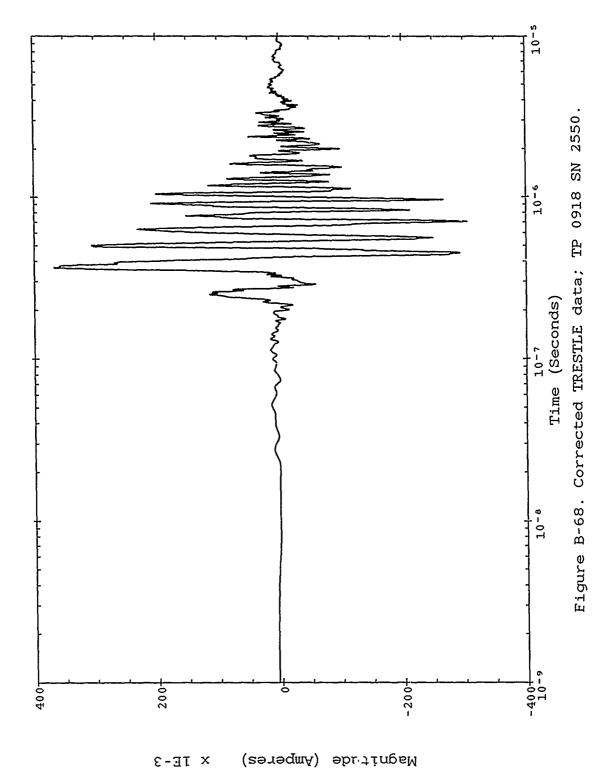
x IE-3

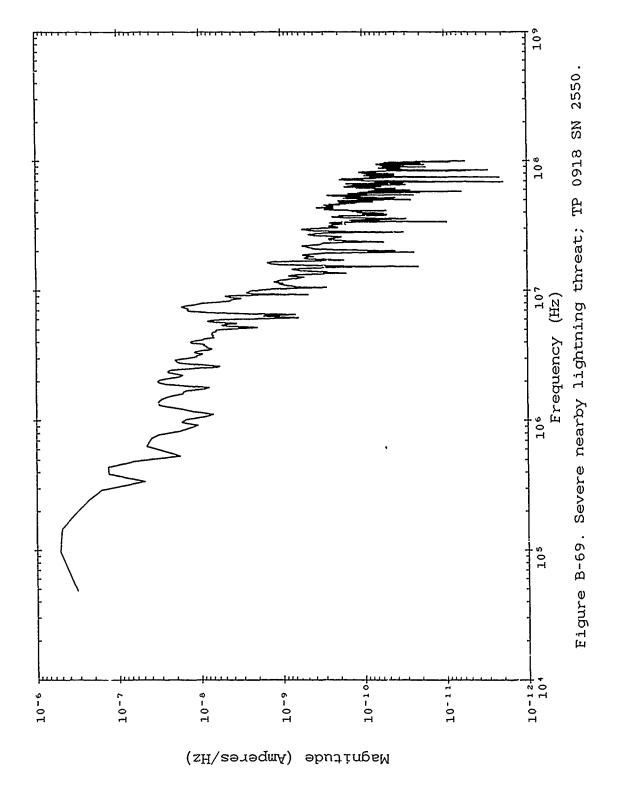


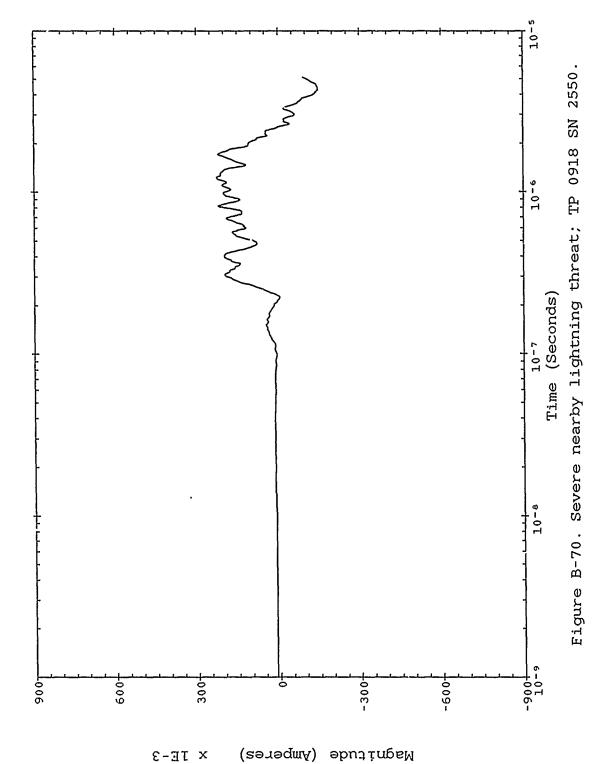


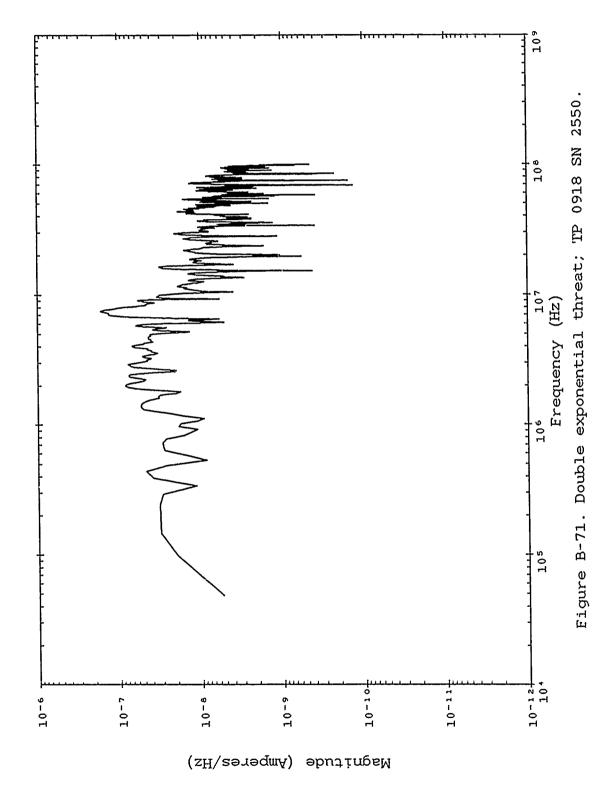
Magnitude (Amperes) x 1E-3

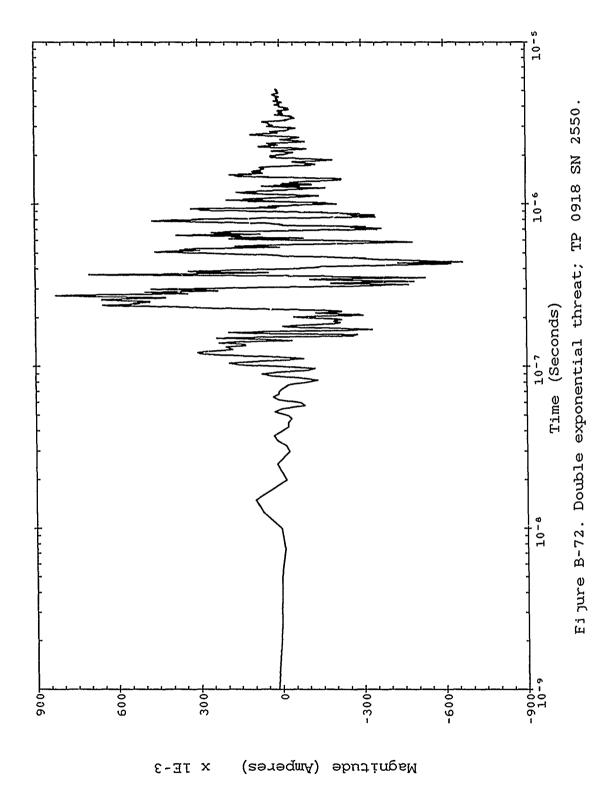


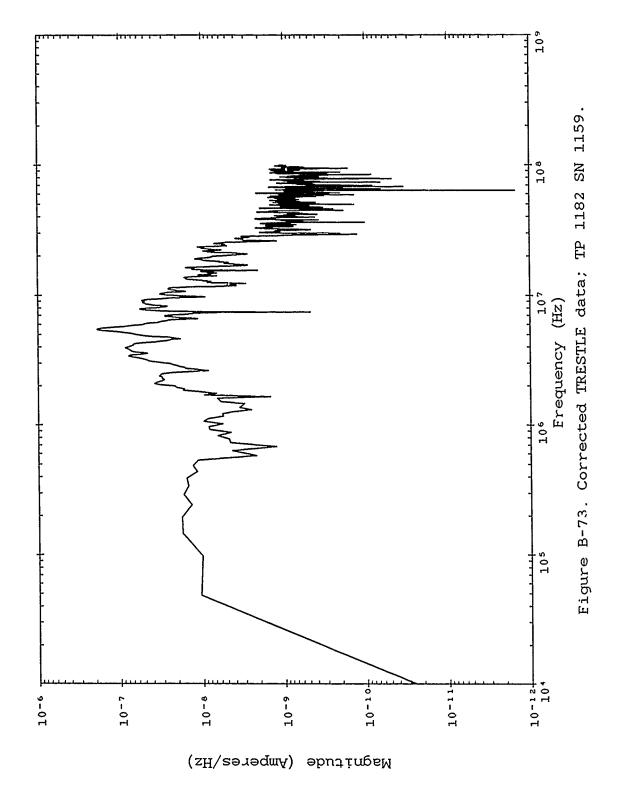


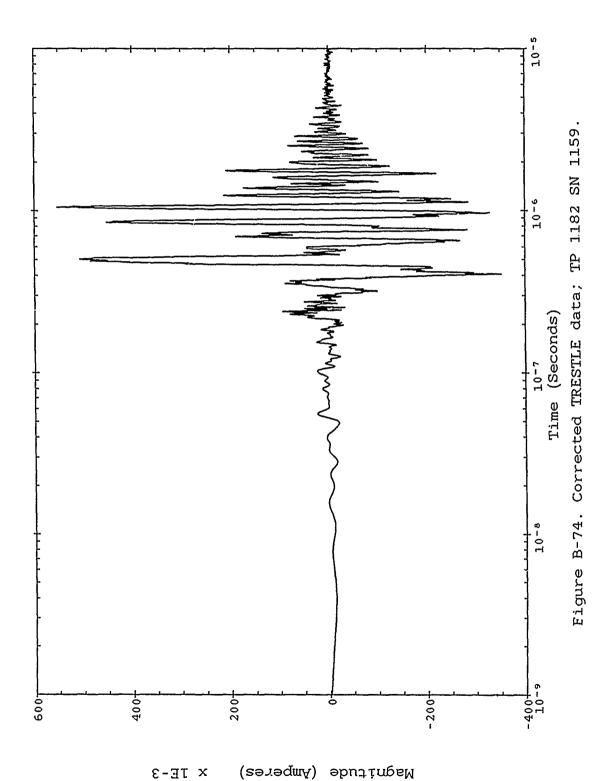




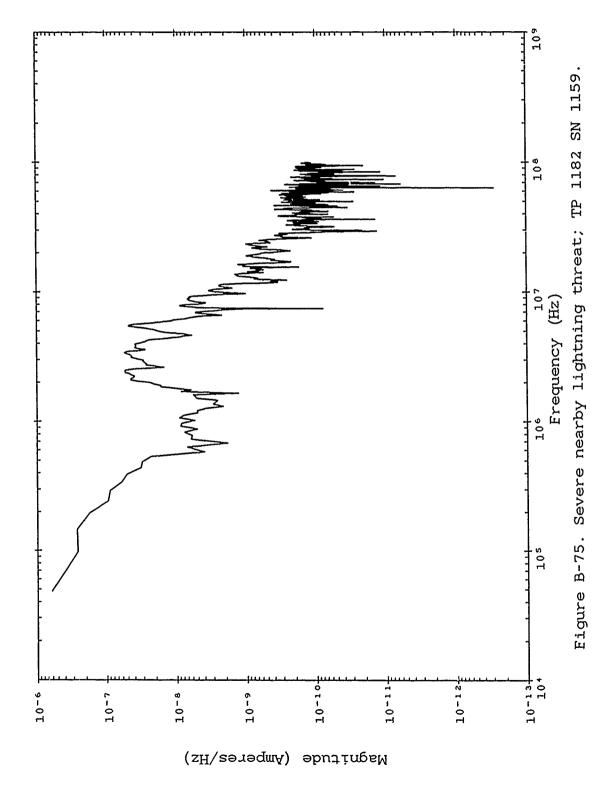


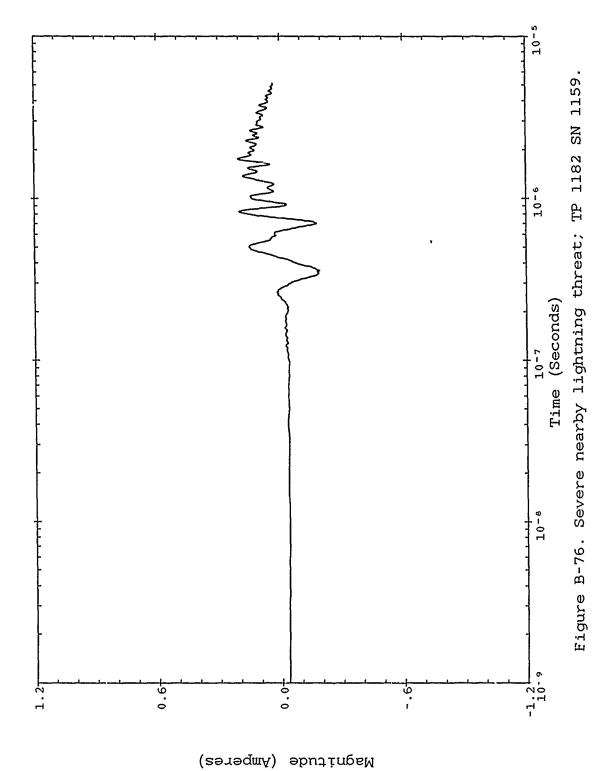


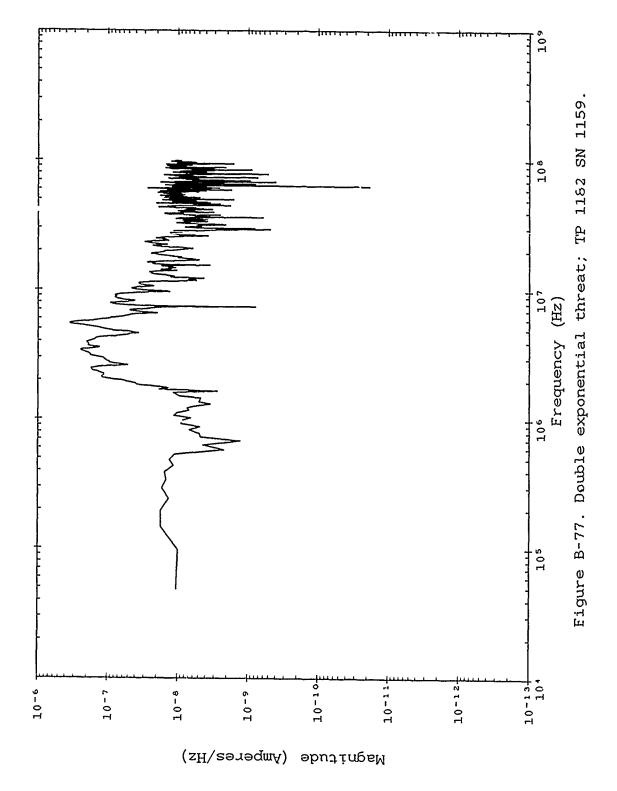


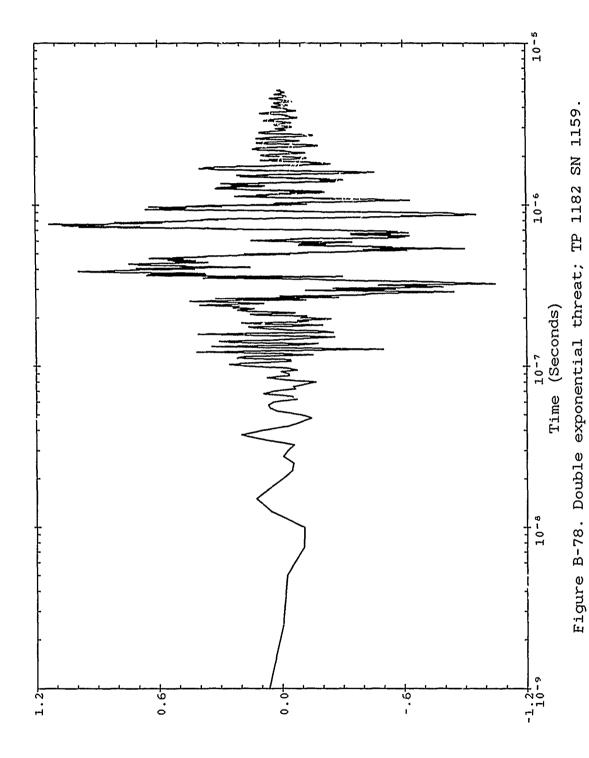


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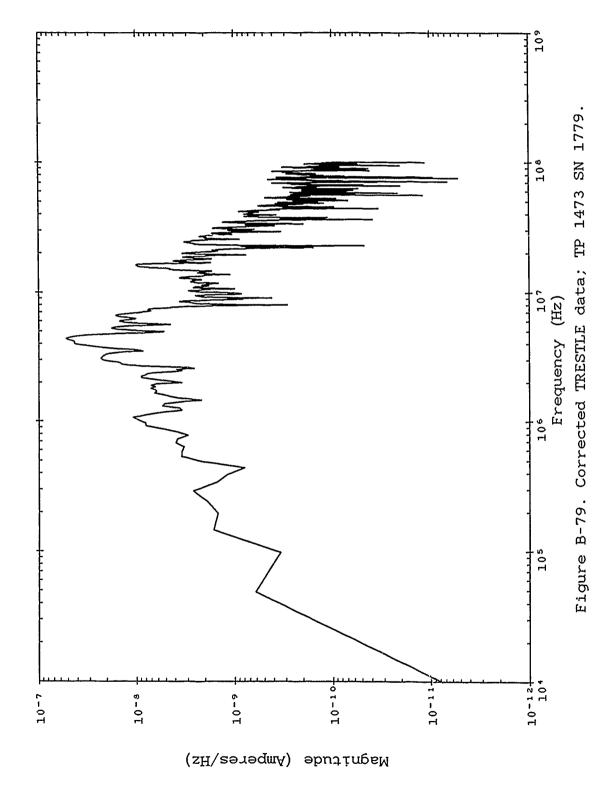


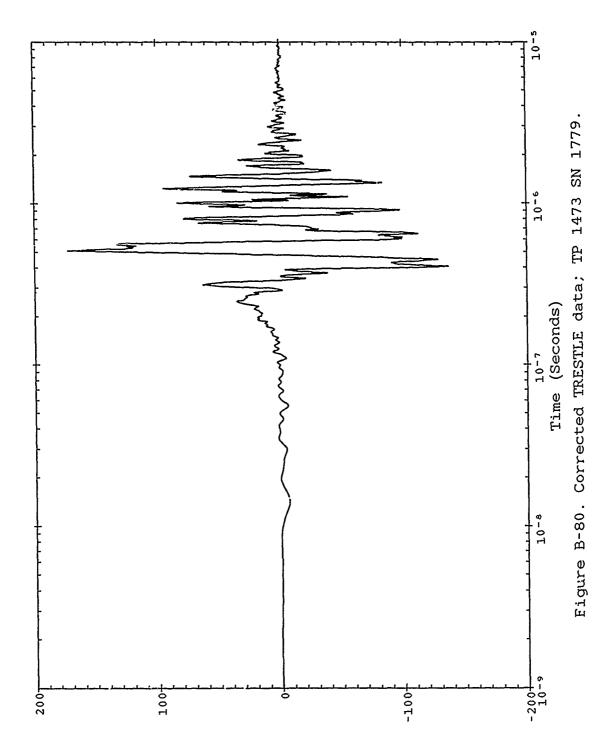






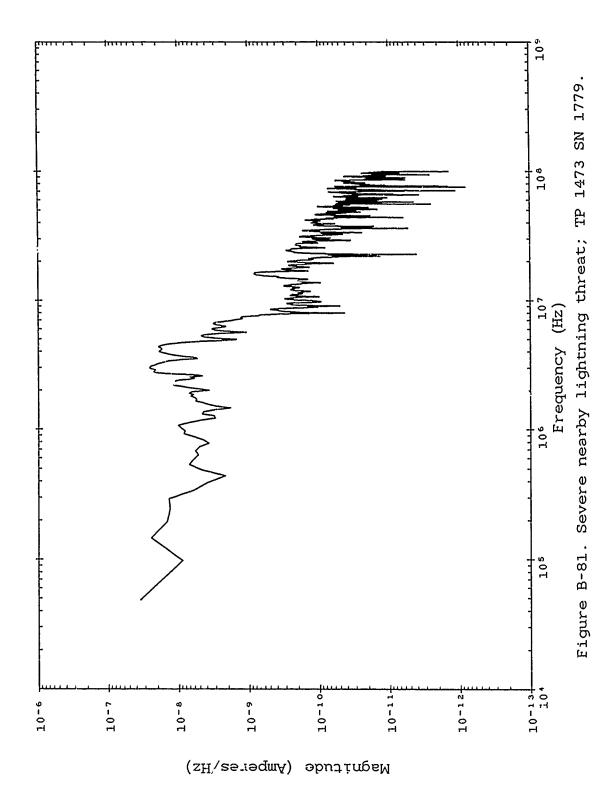
Magnitude (Amperes)





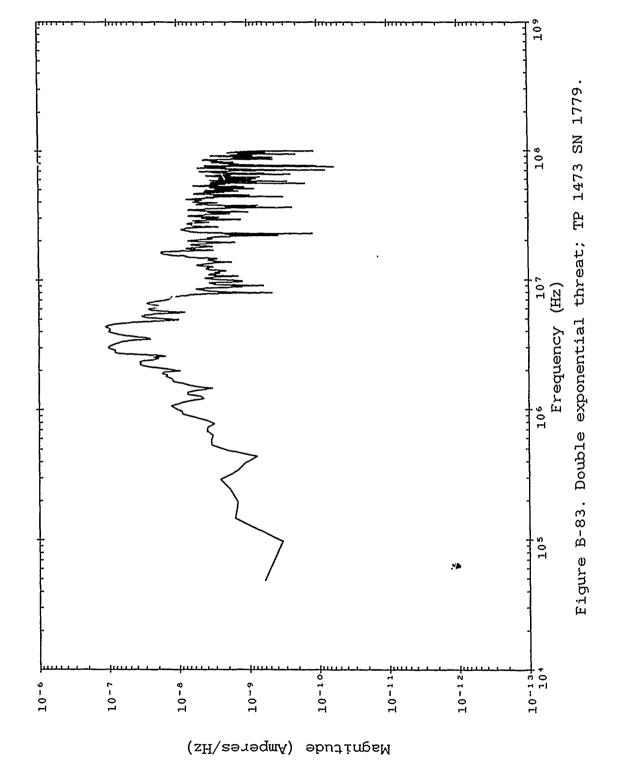
Magnitude (Amperes)

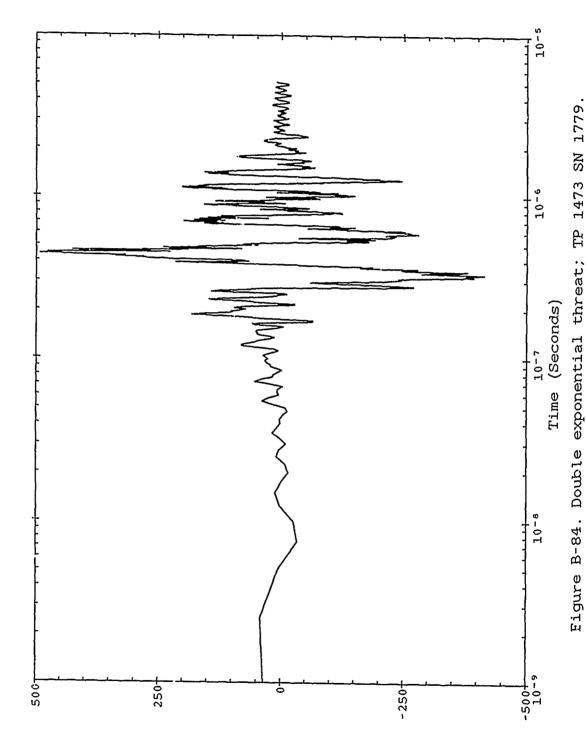
× TE-3



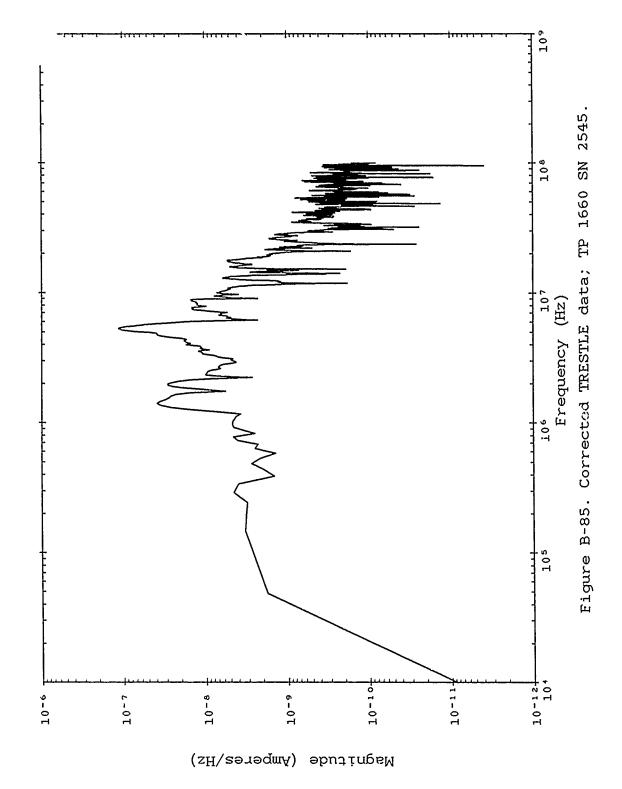
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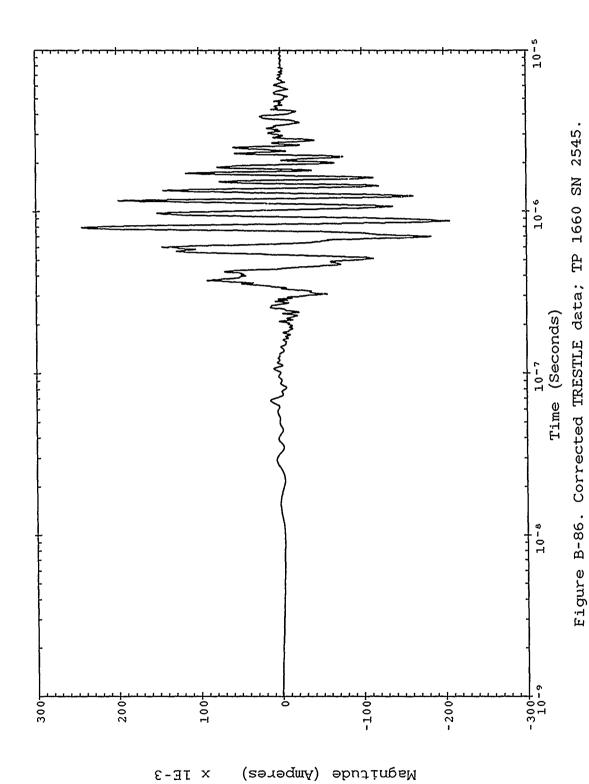
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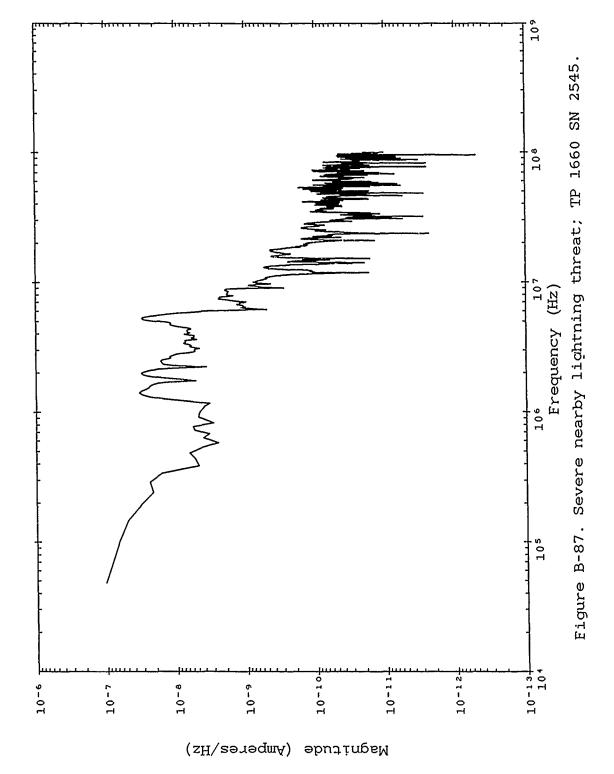


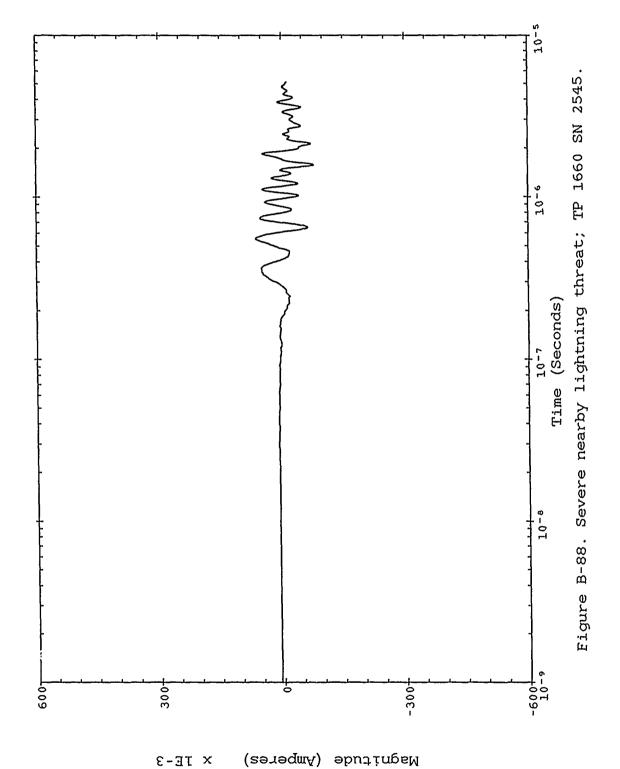


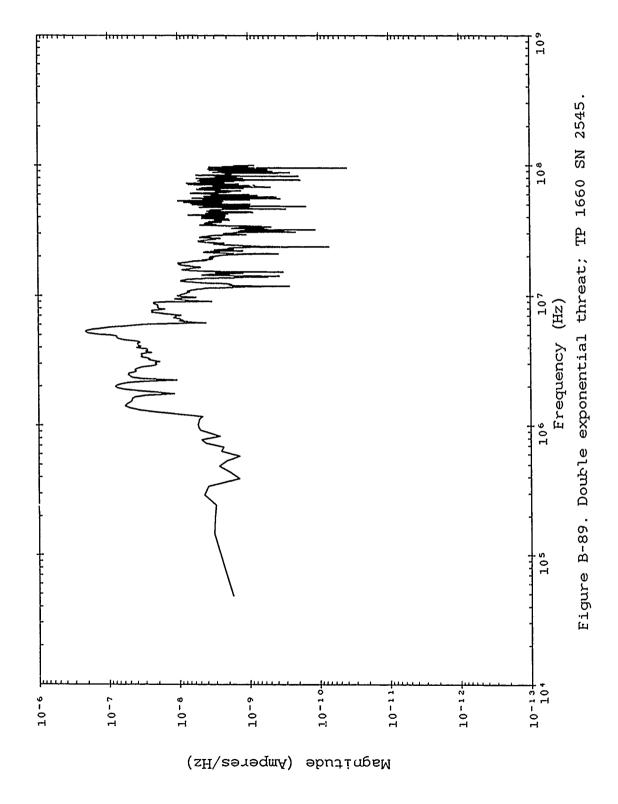
Wagnitude (Amperes) \times 1E-3

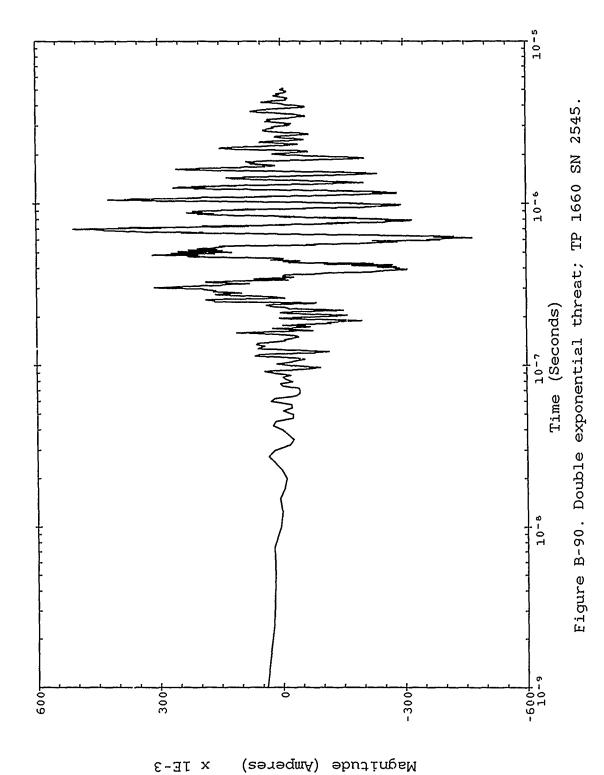


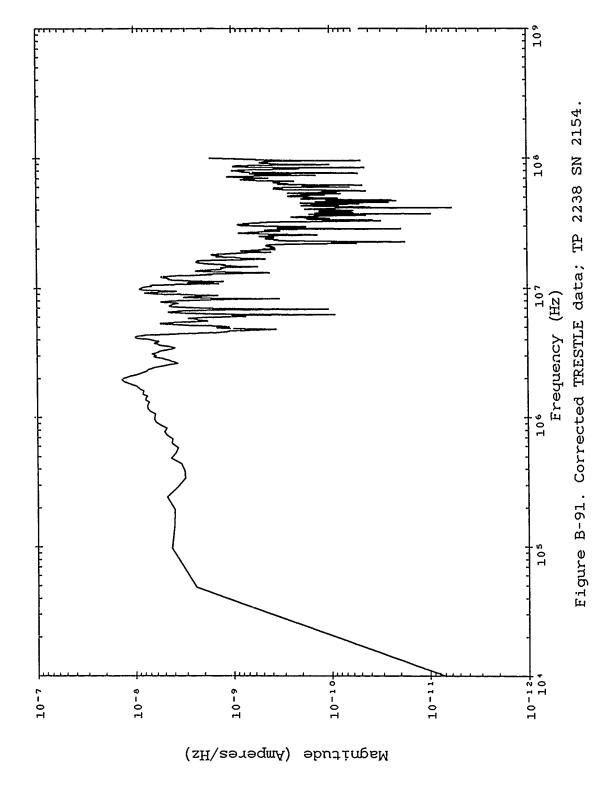


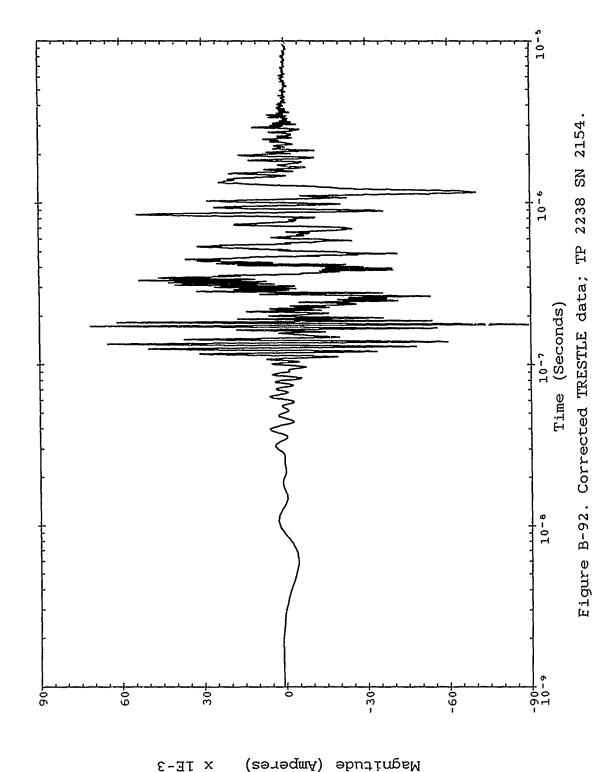






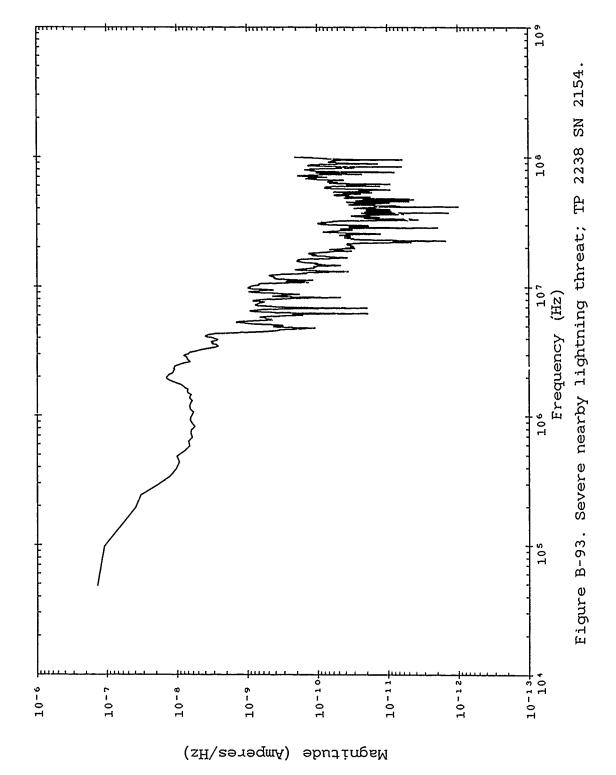


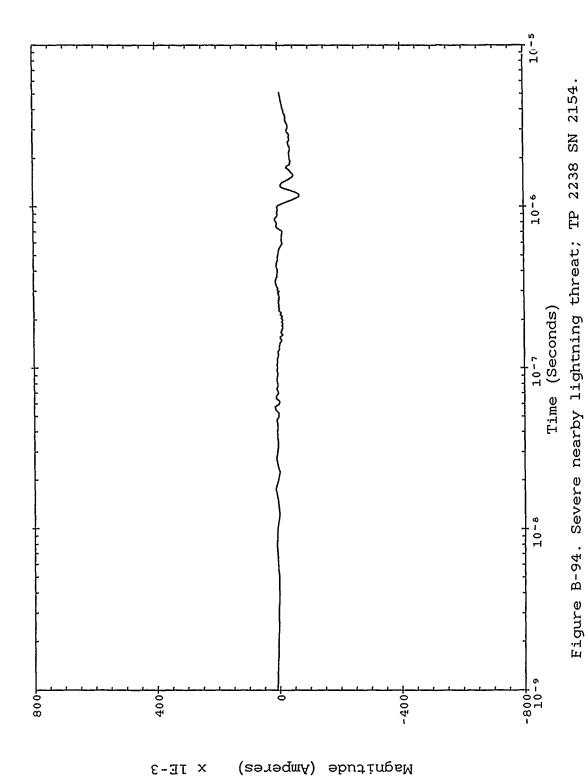


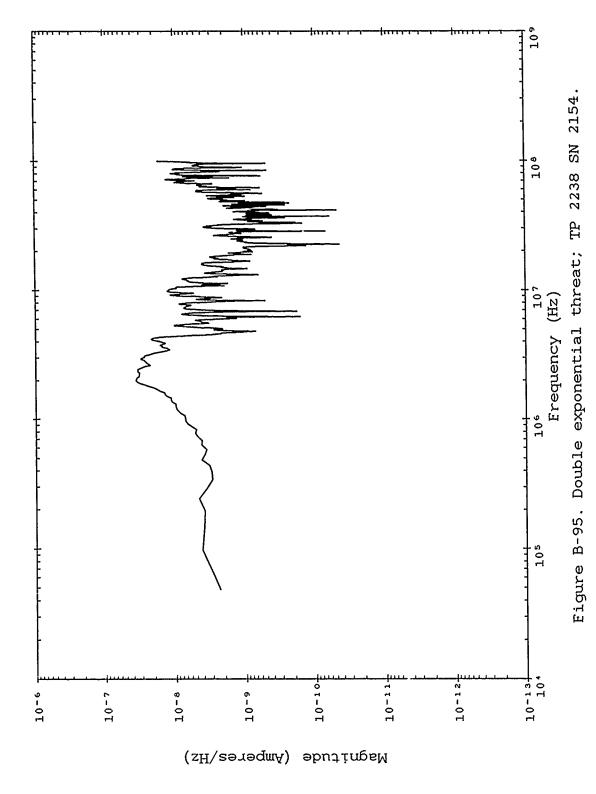


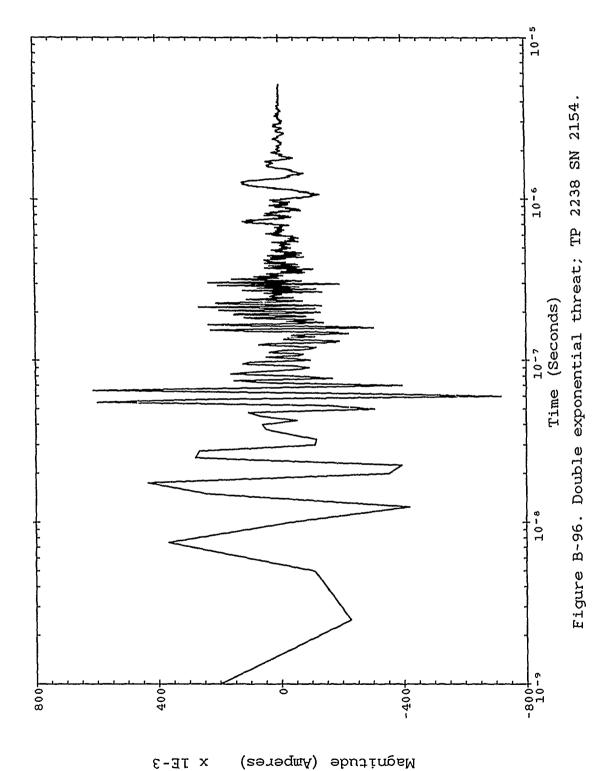
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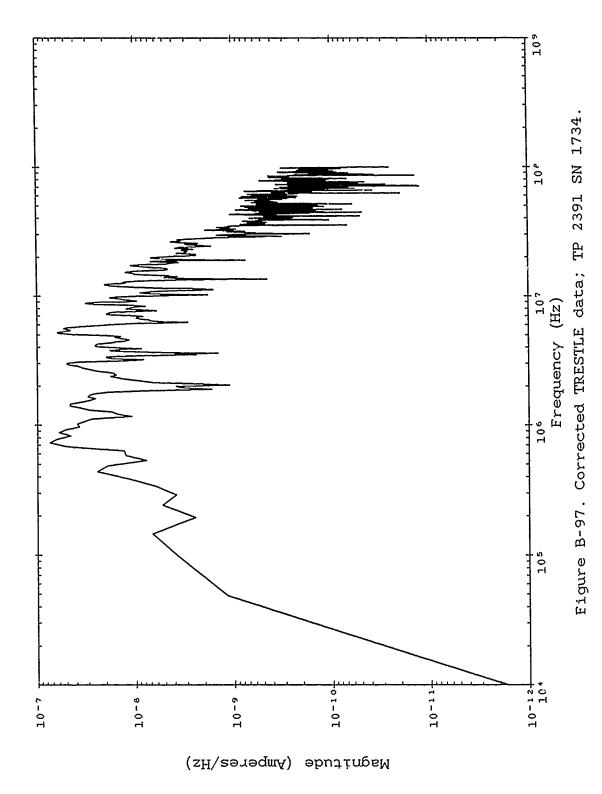
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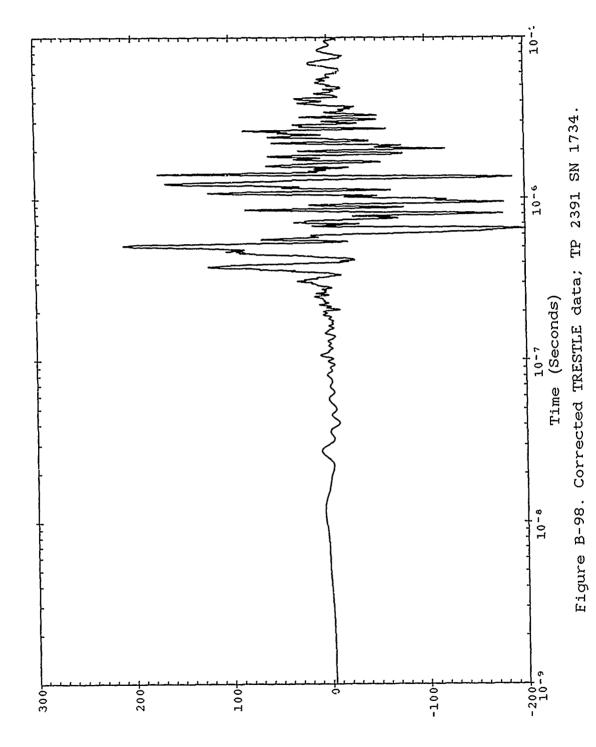




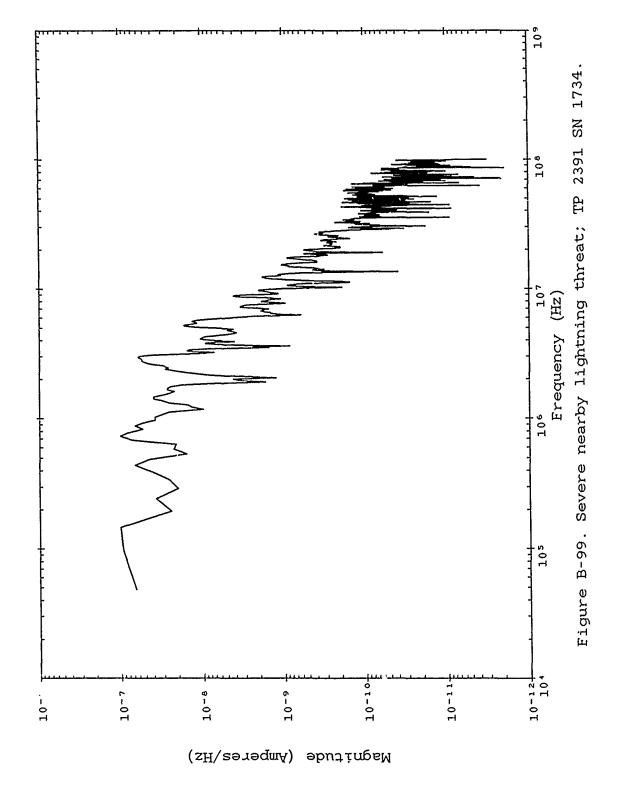






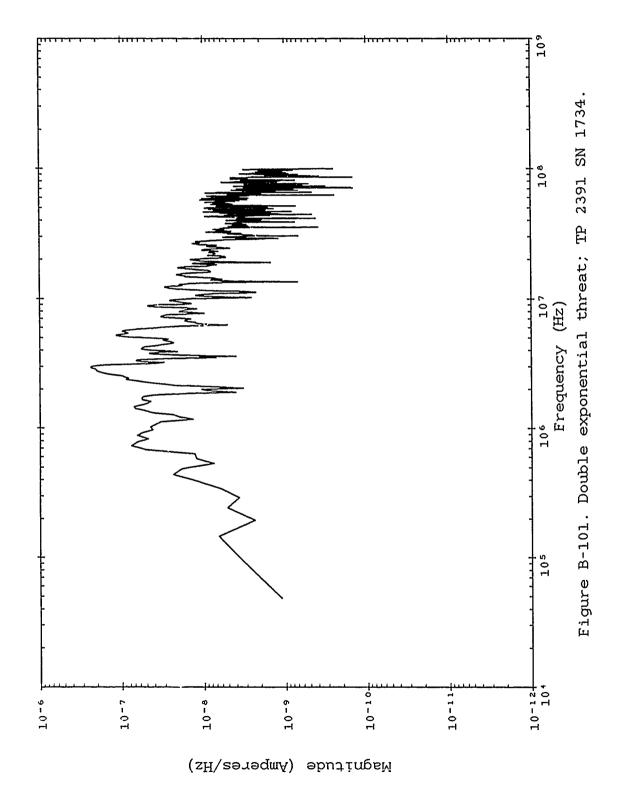


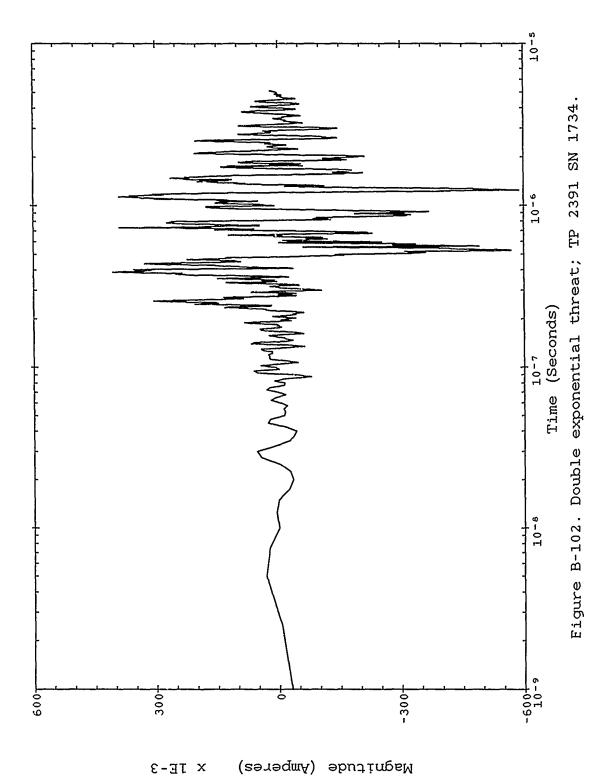
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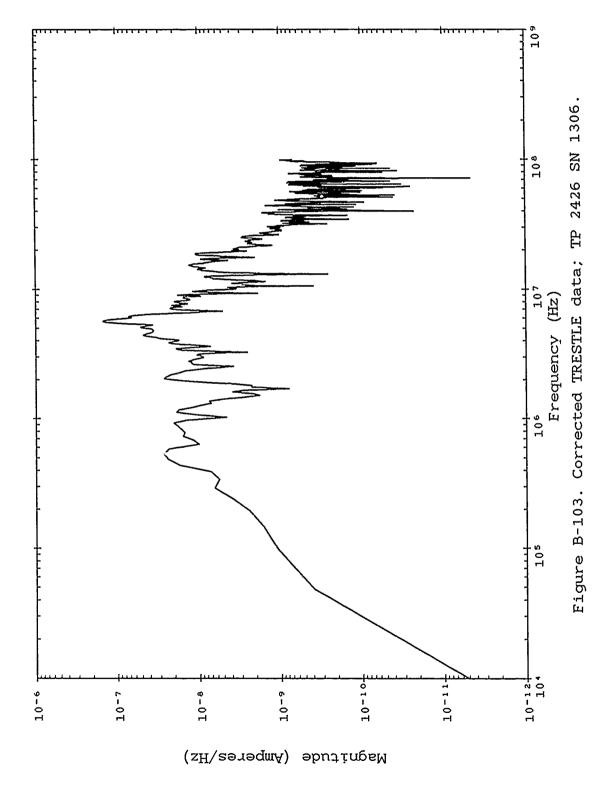


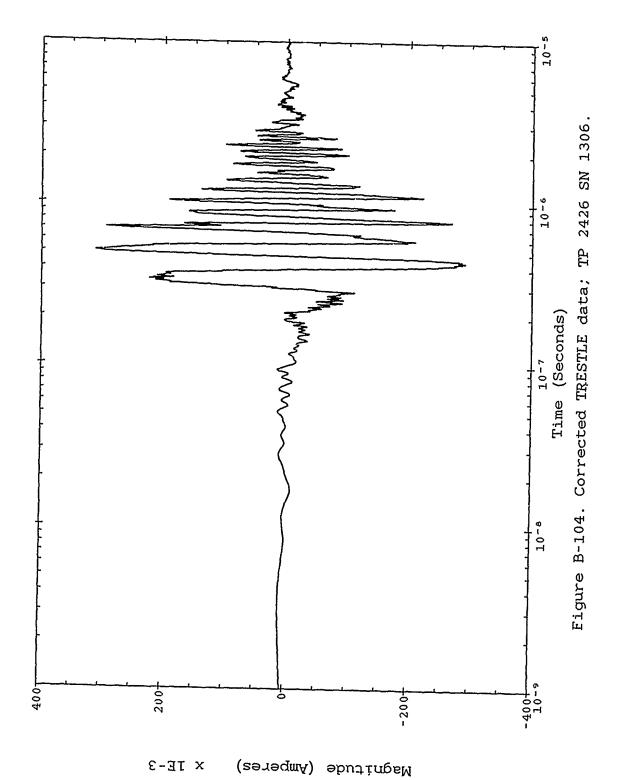
Magnitude (Amperes)

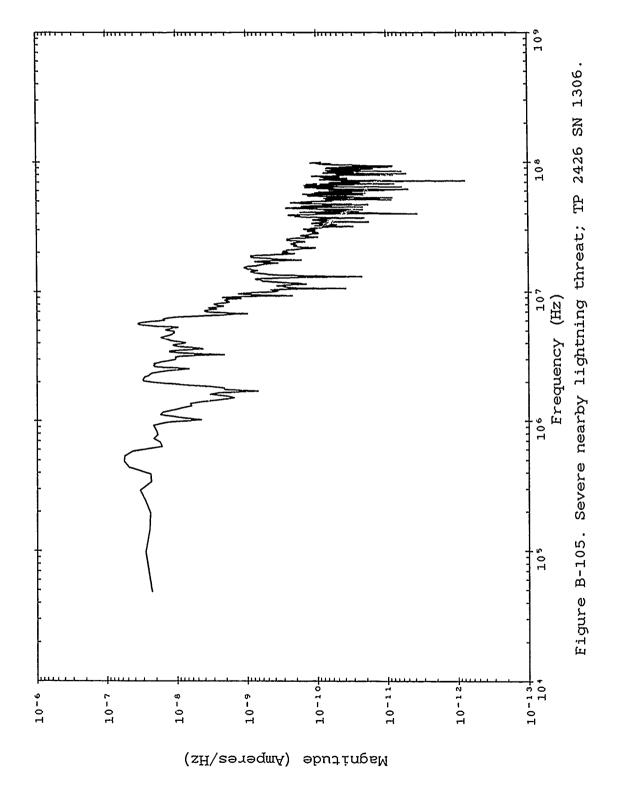
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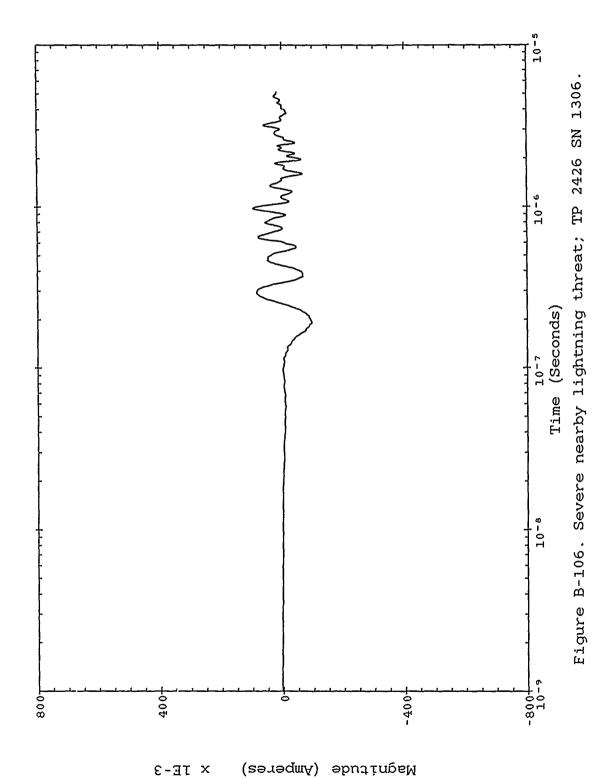


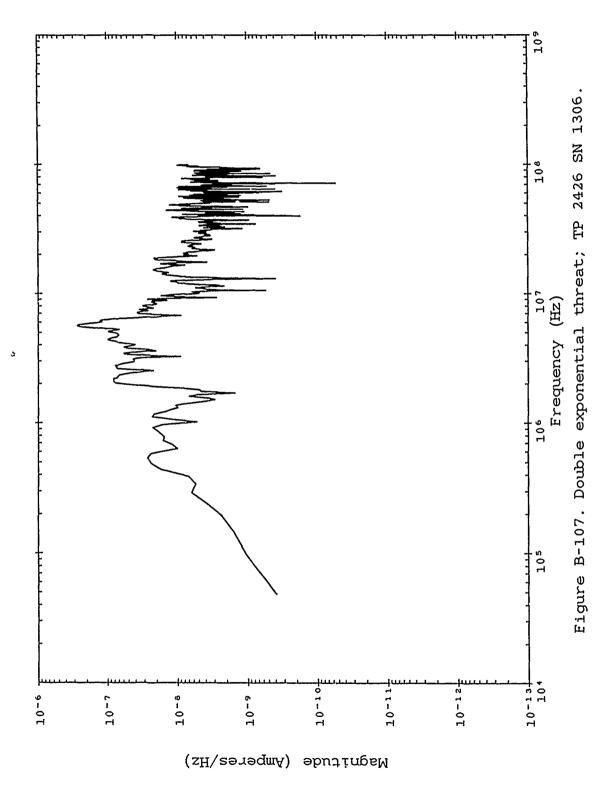


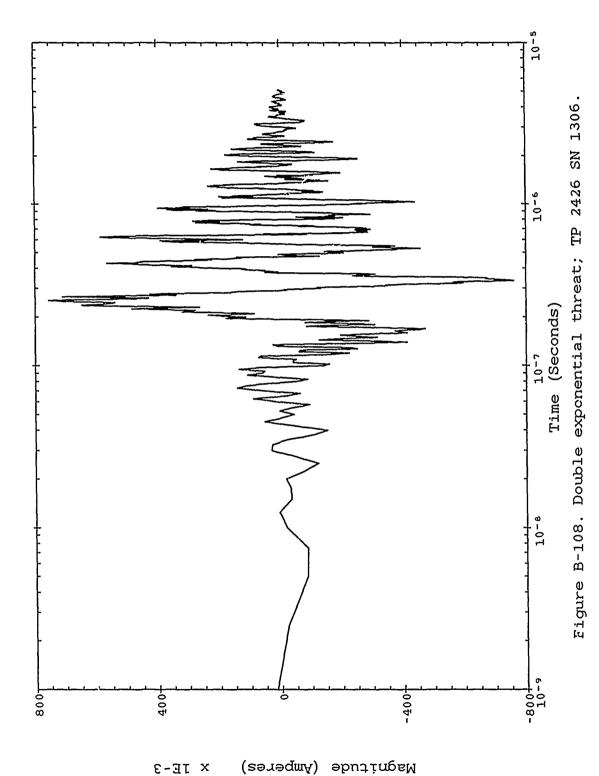


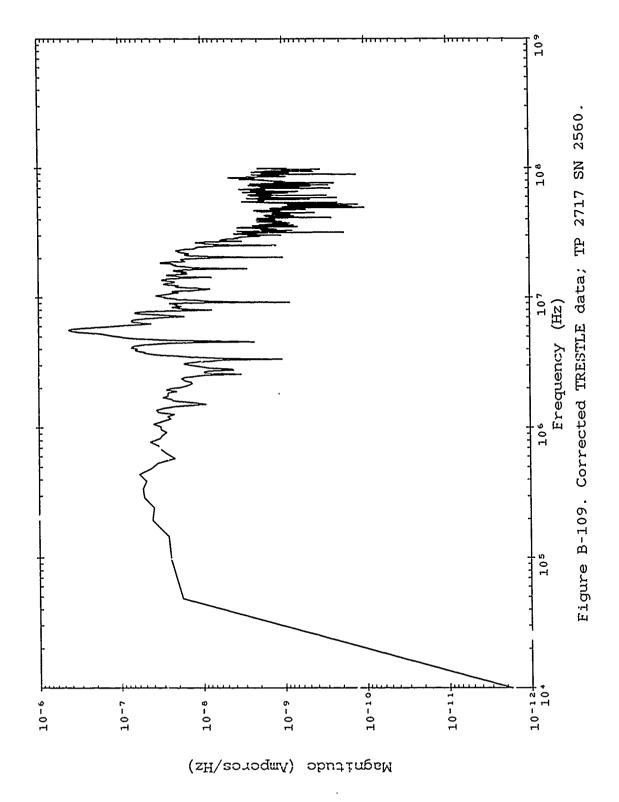


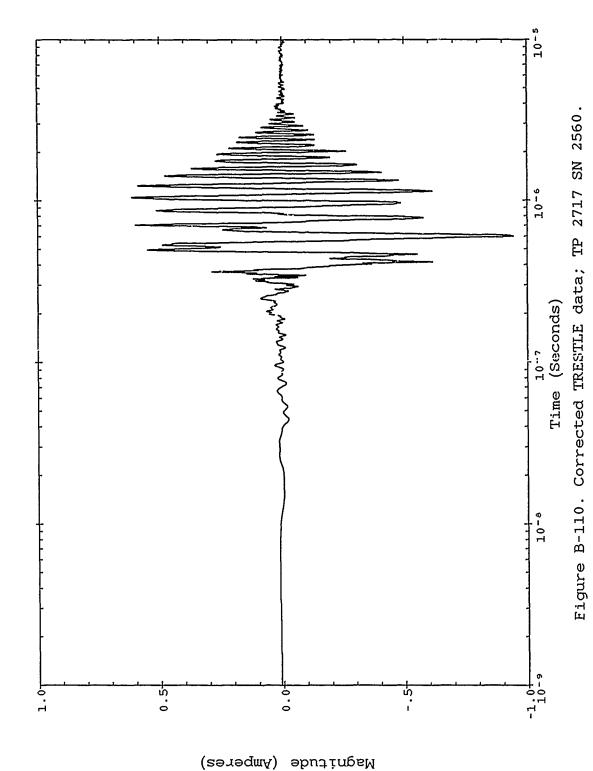


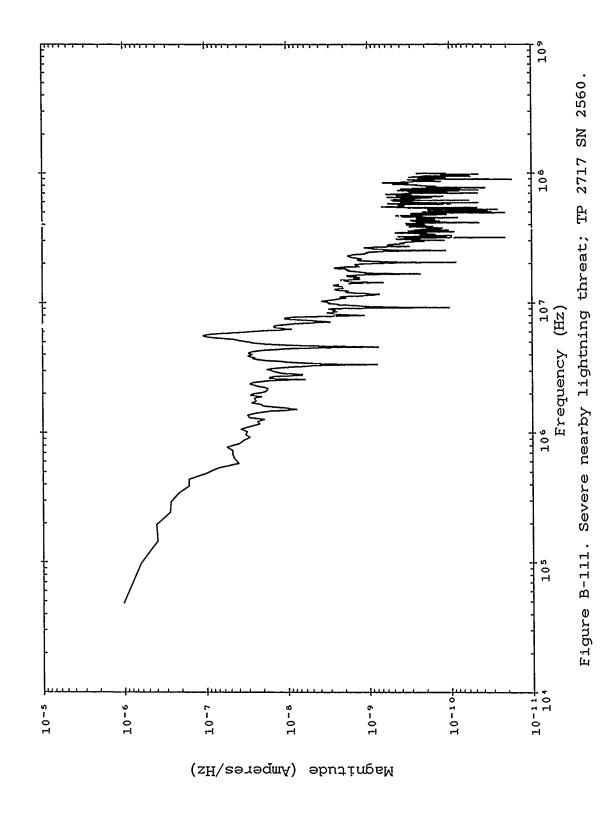


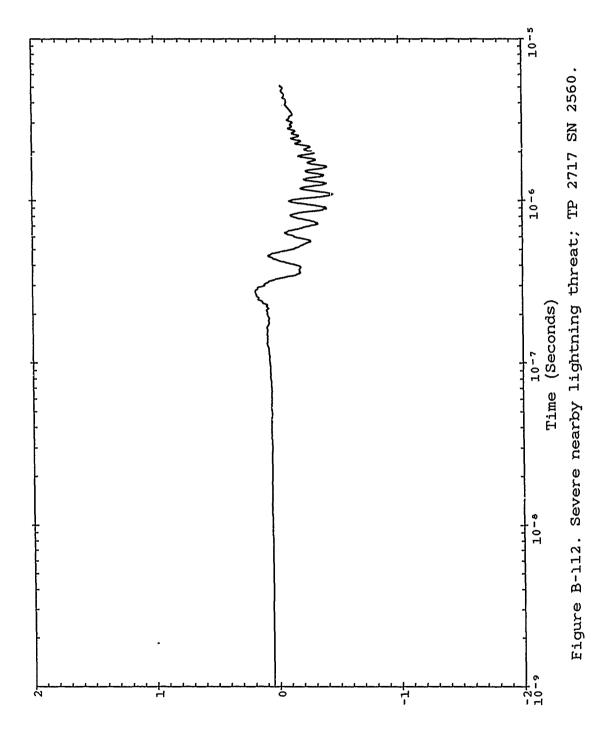




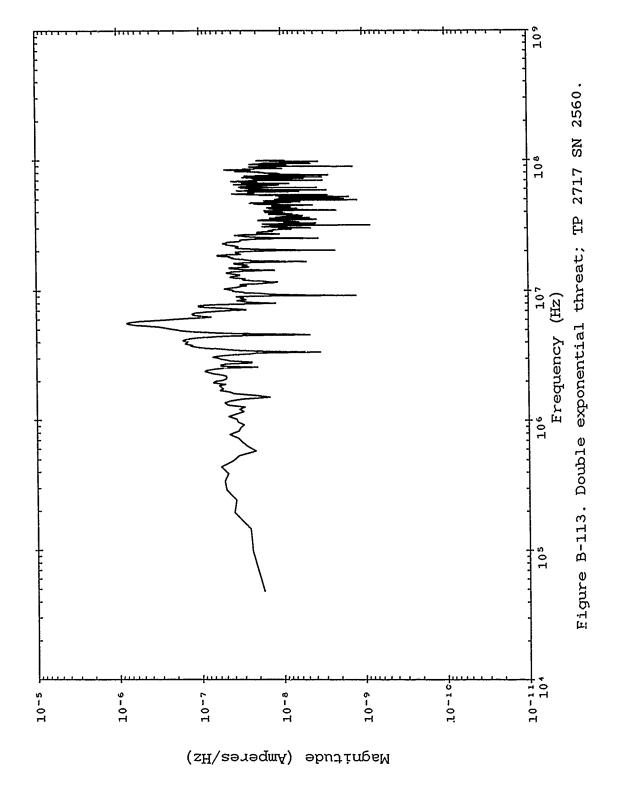


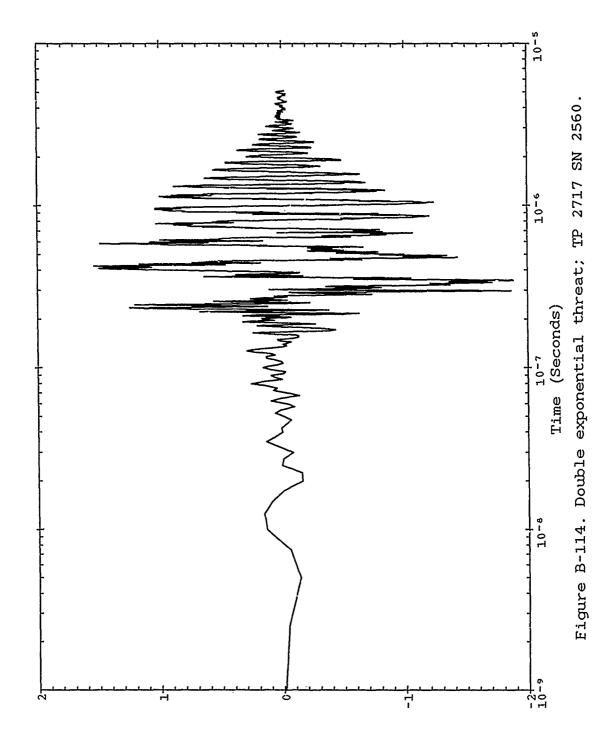






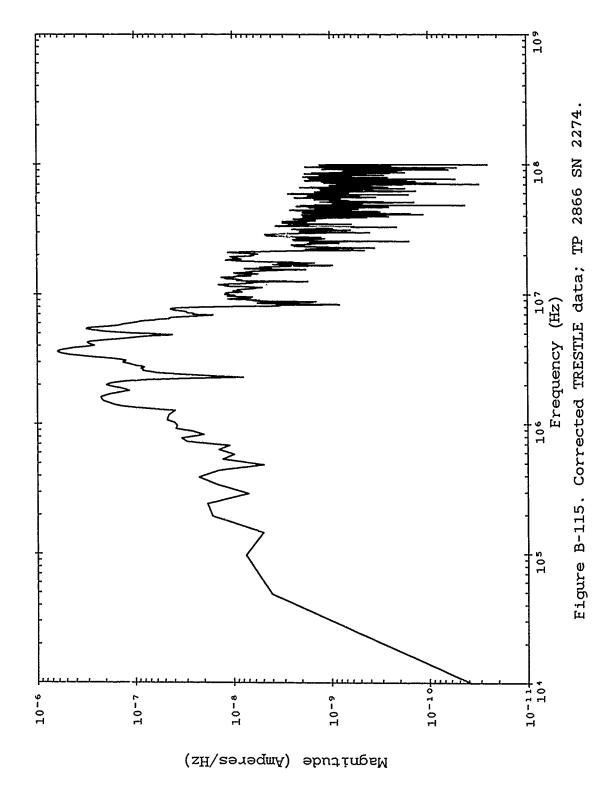
Magnitude (Amperes)

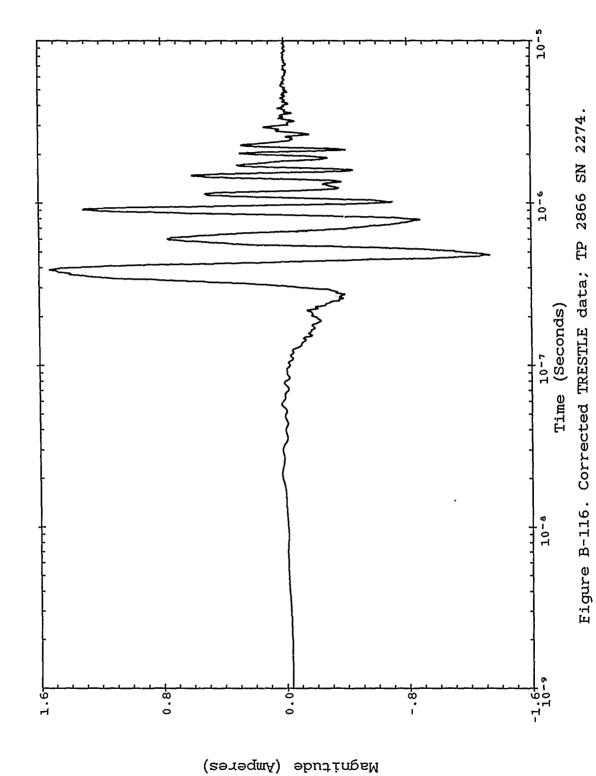




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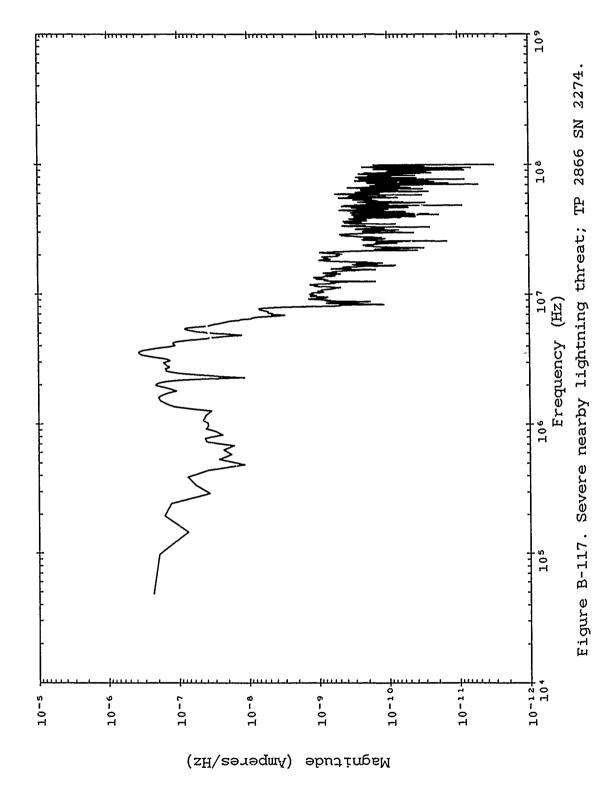
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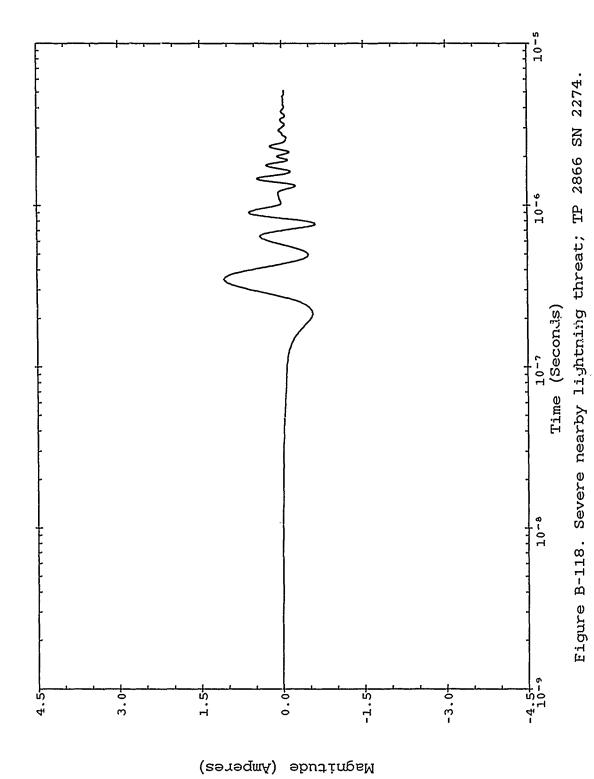


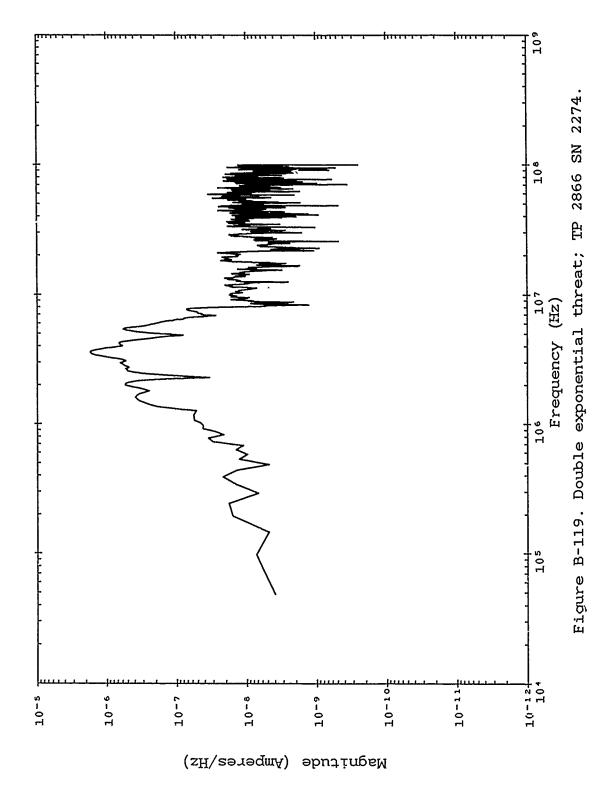


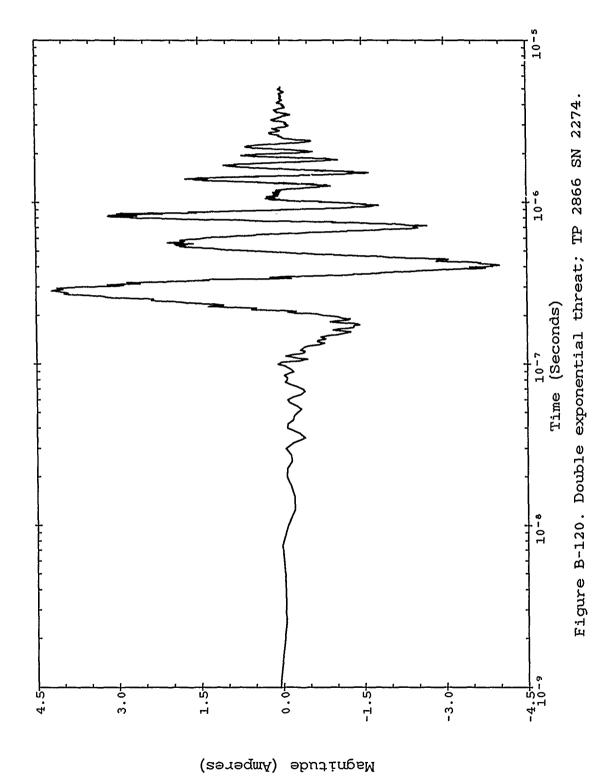
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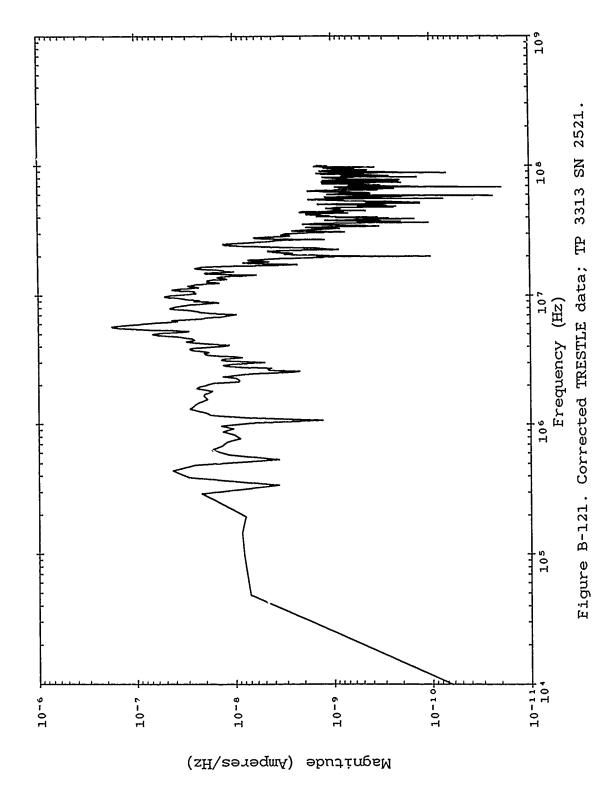
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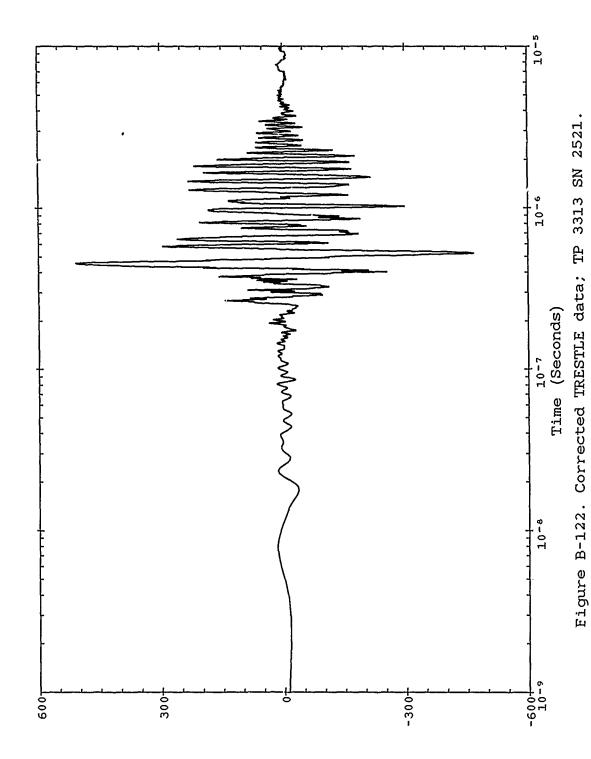






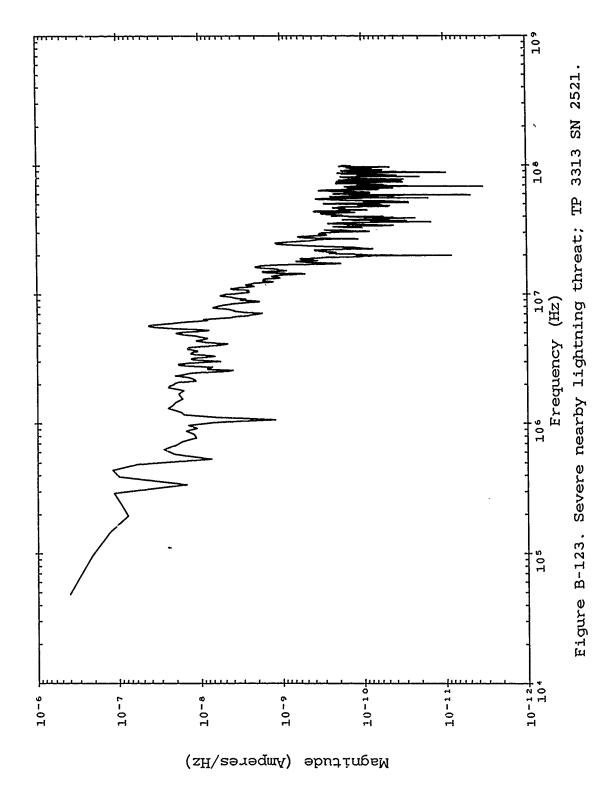




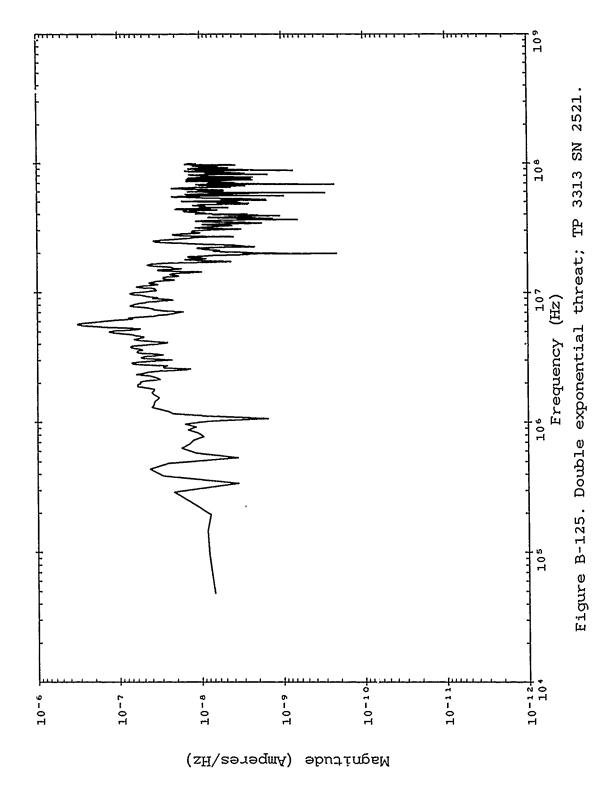


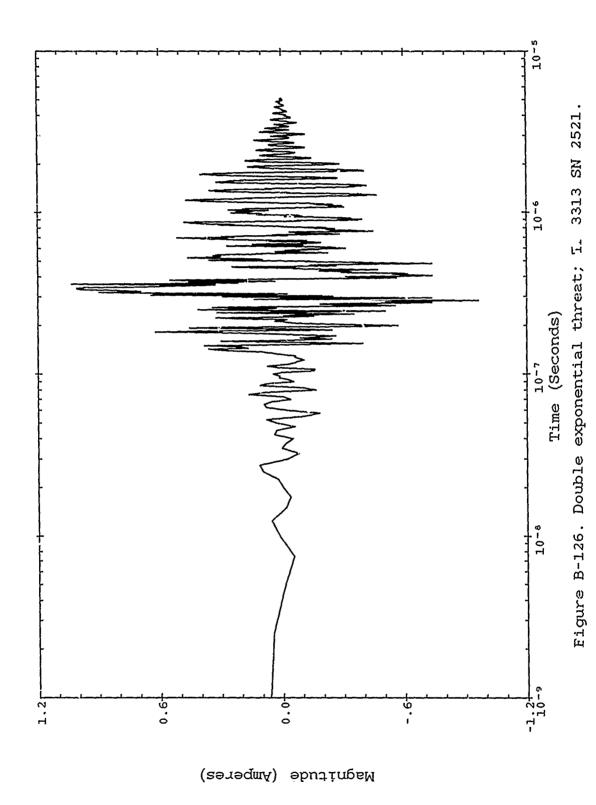
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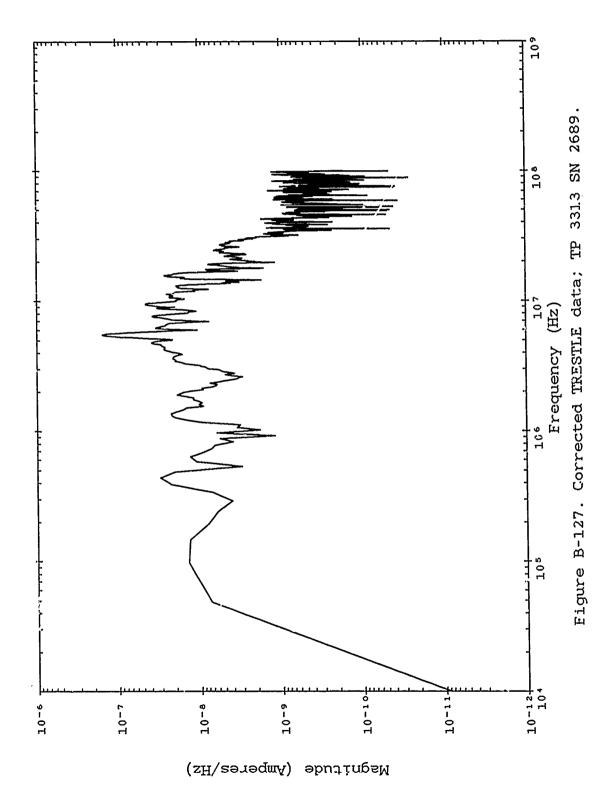
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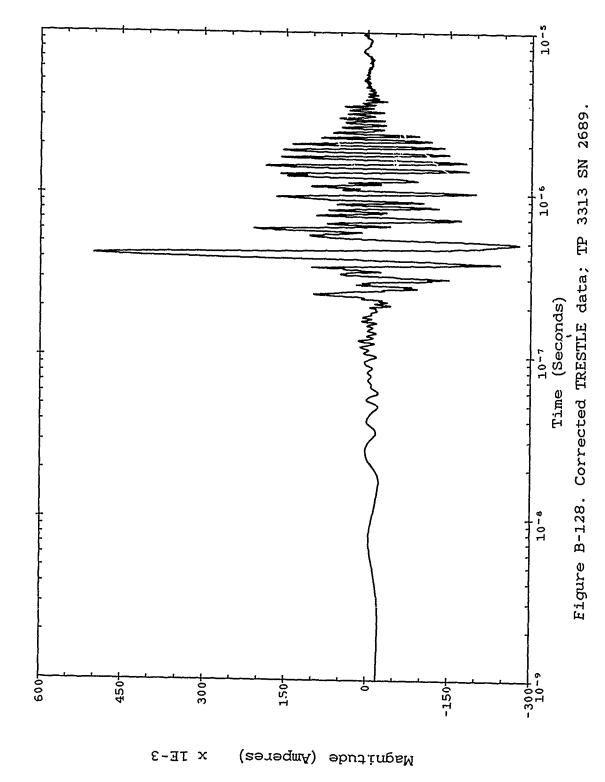


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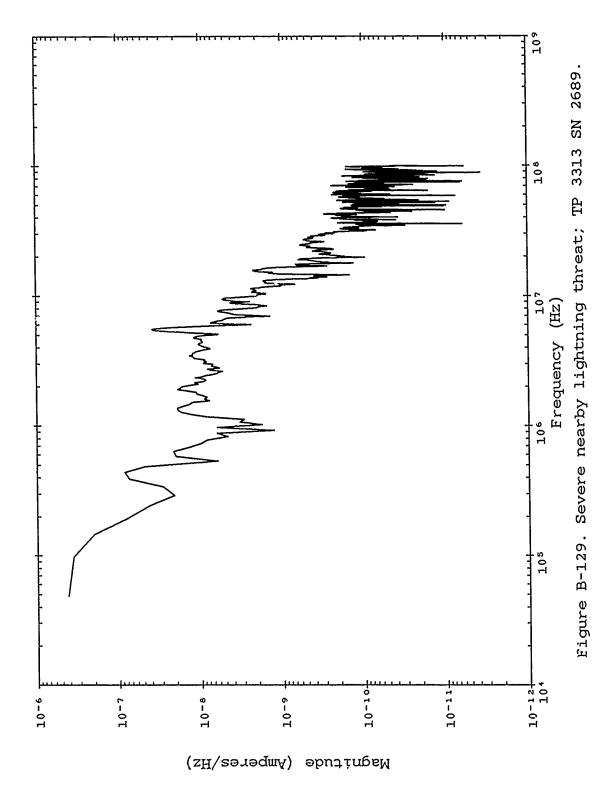


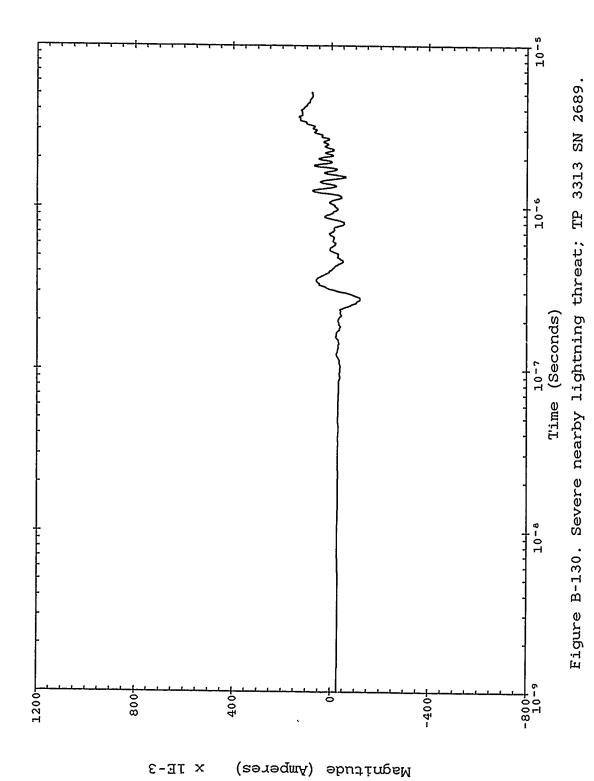
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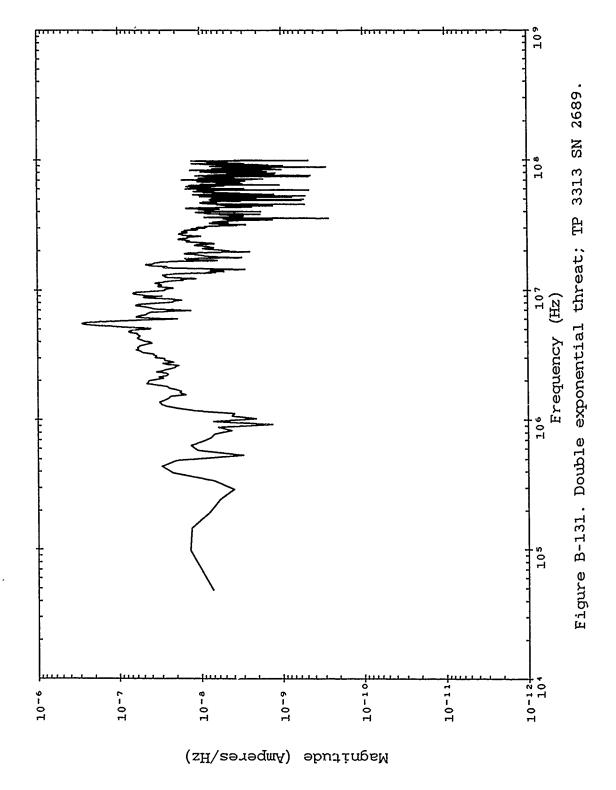


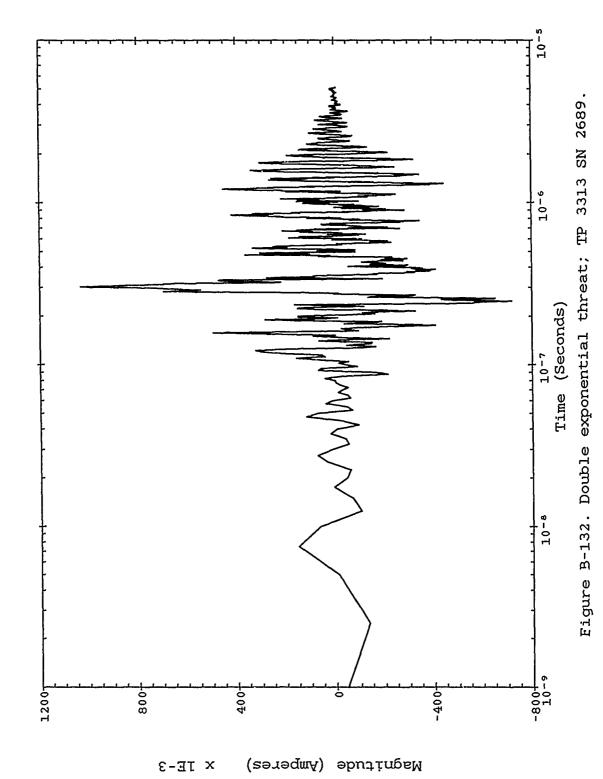
CONTRACTOR OF CONTRACTOR OF STREET

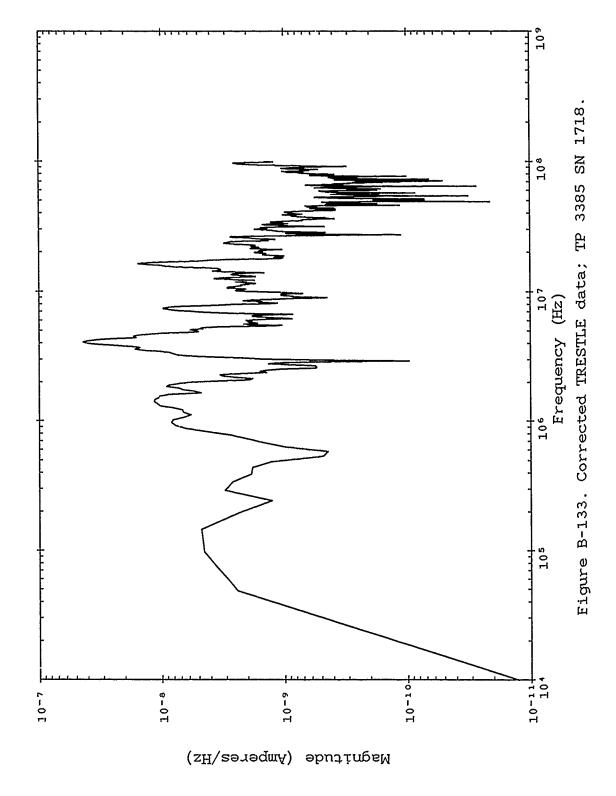
STATES TO SERVICE AND SERVICE

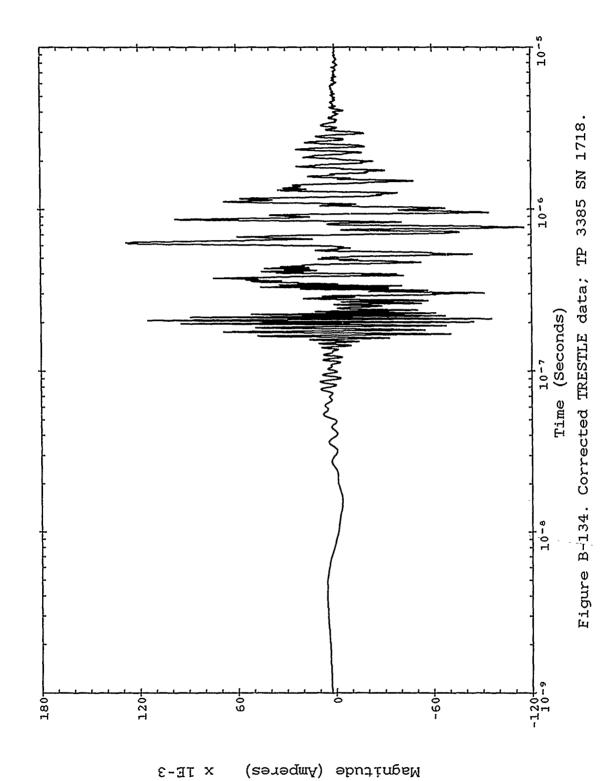


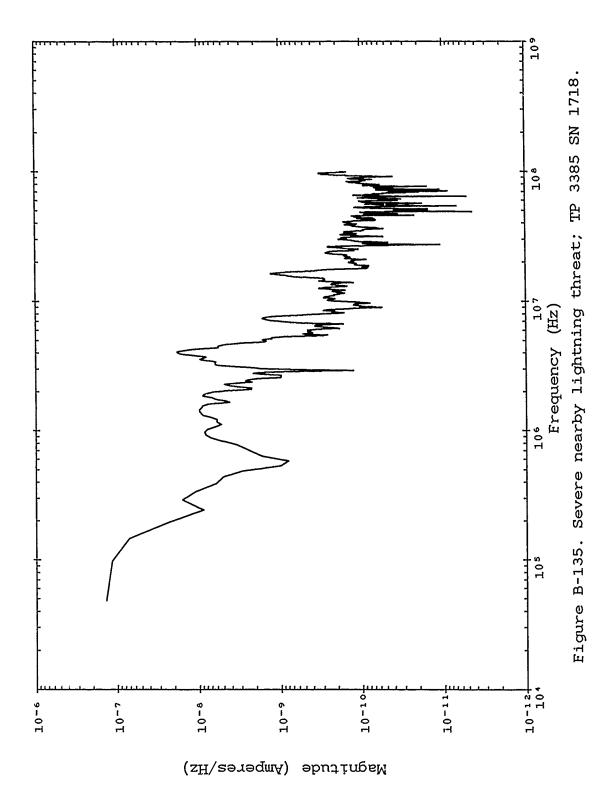


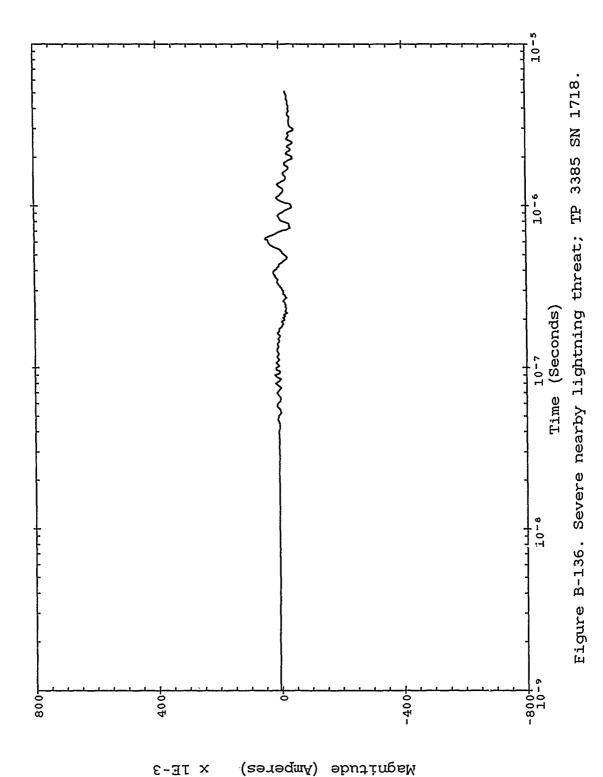


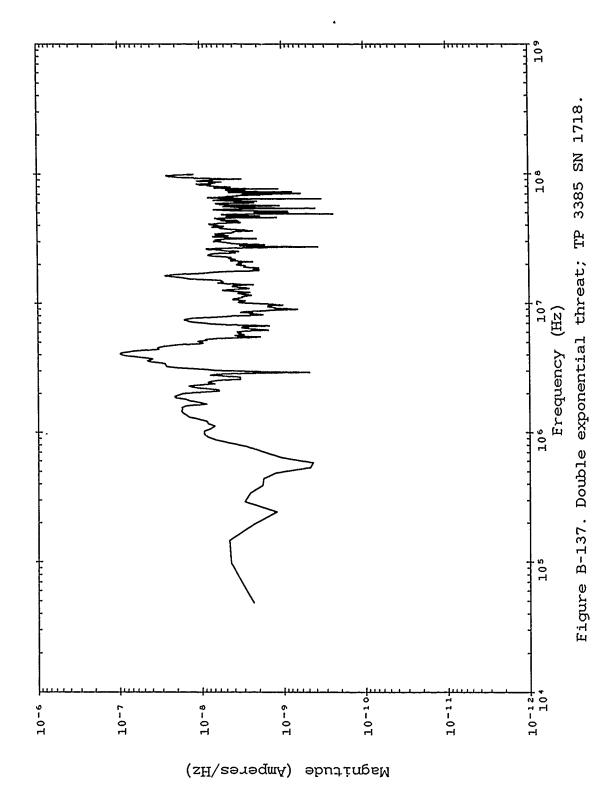


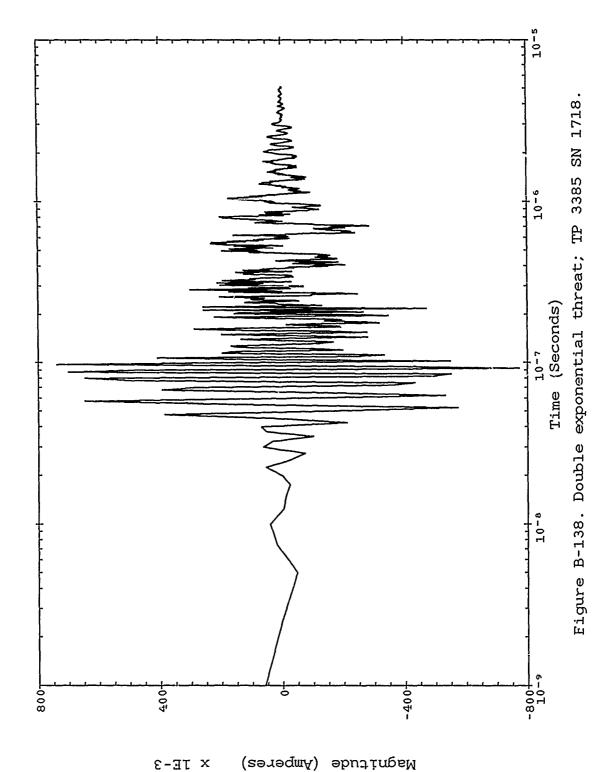


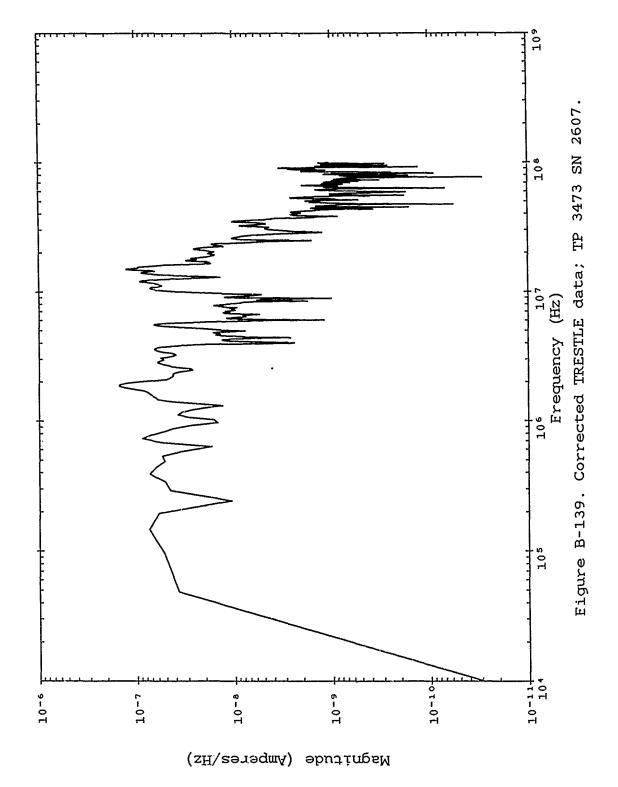


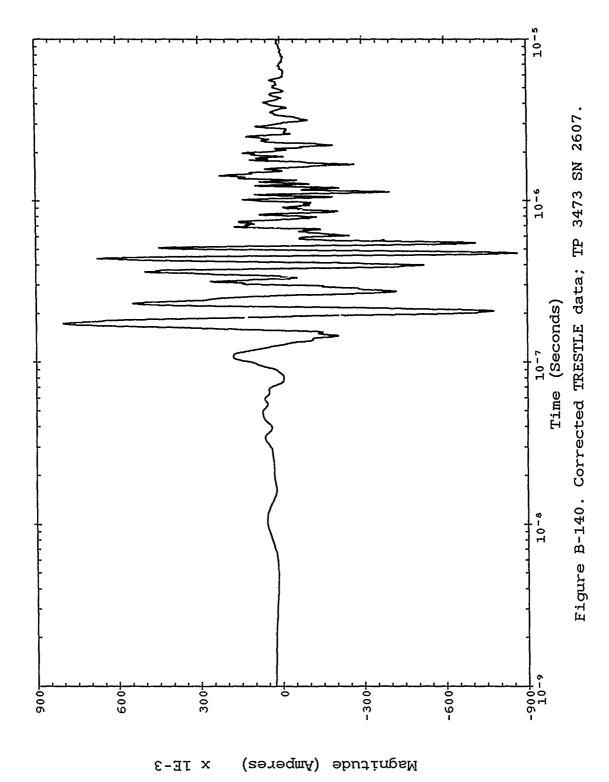


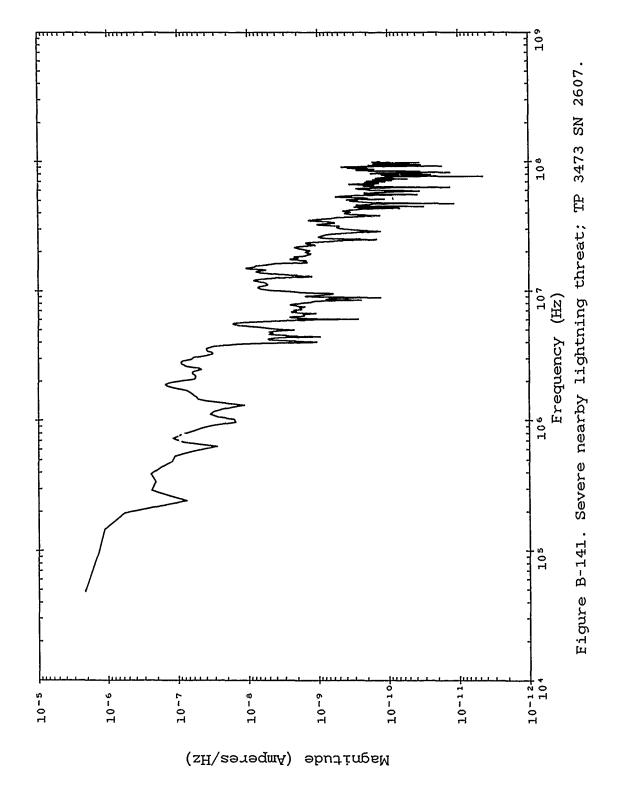


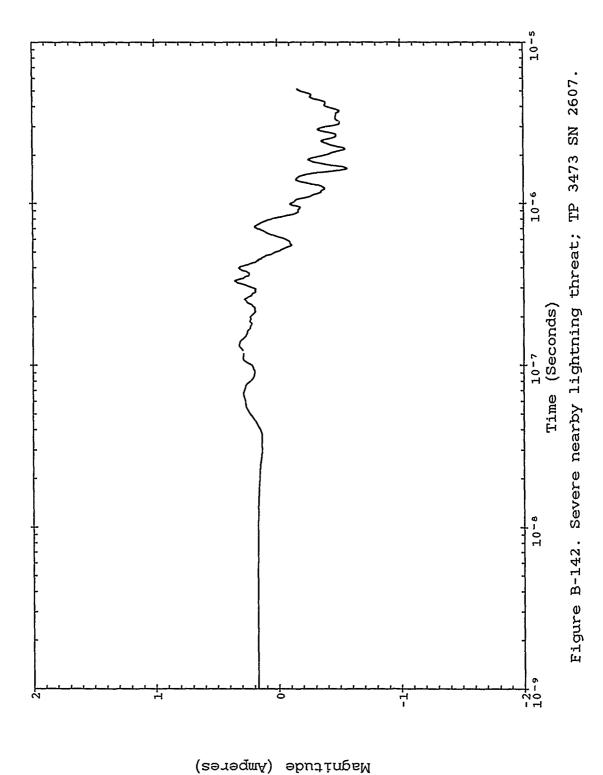


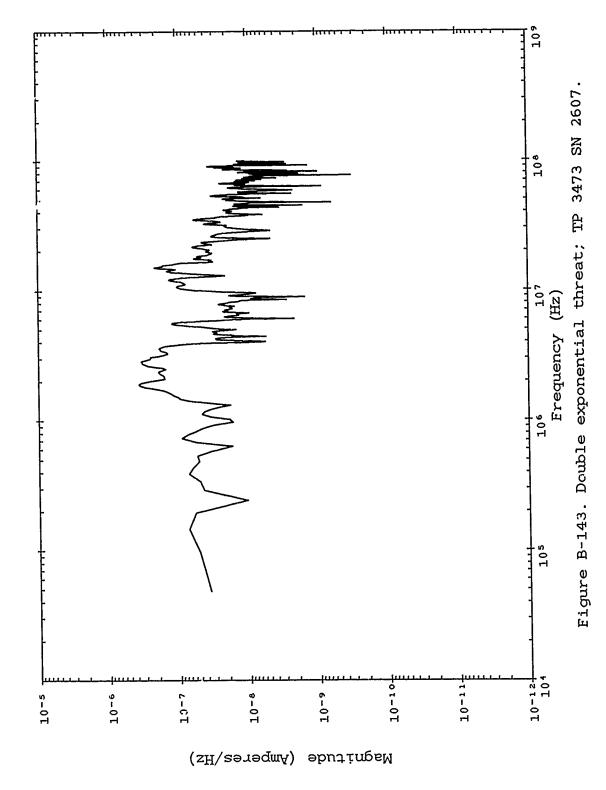


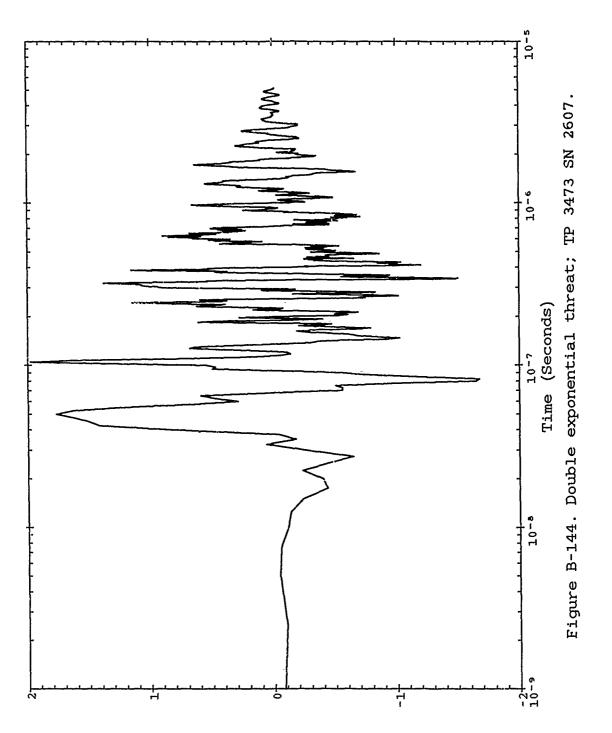




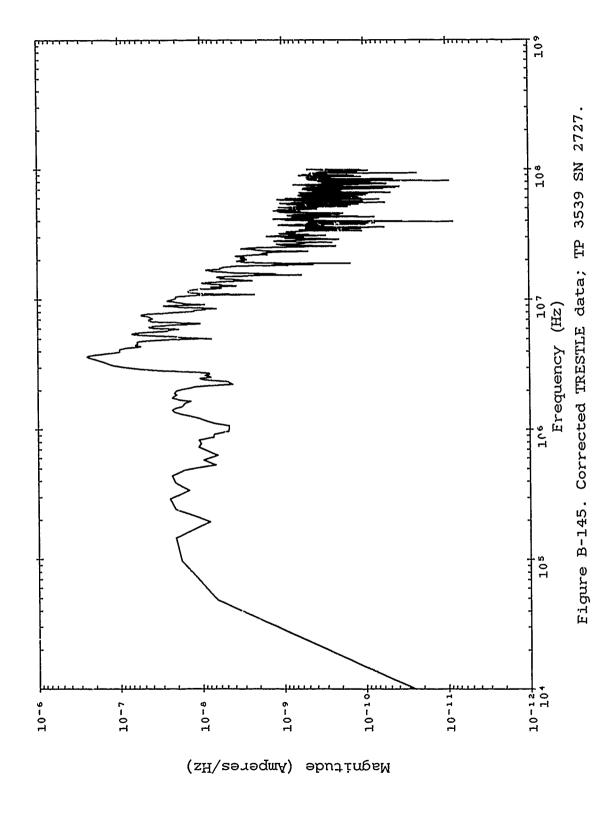


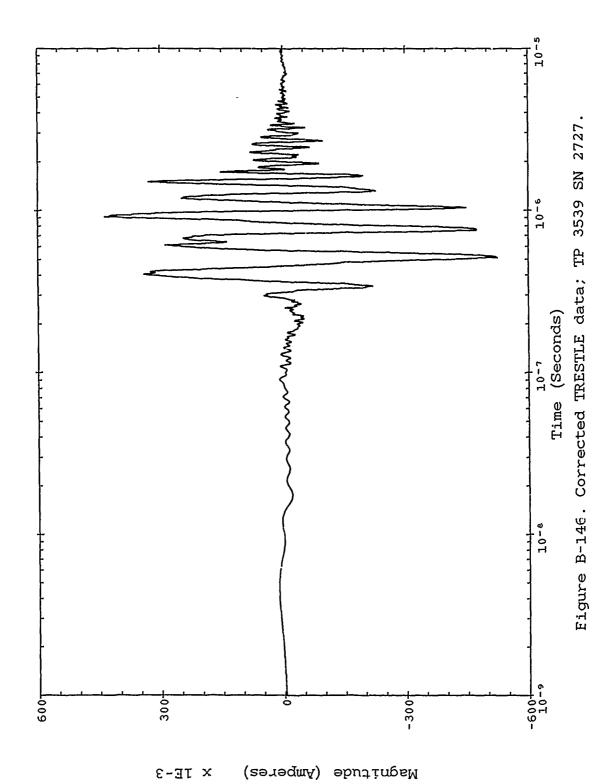


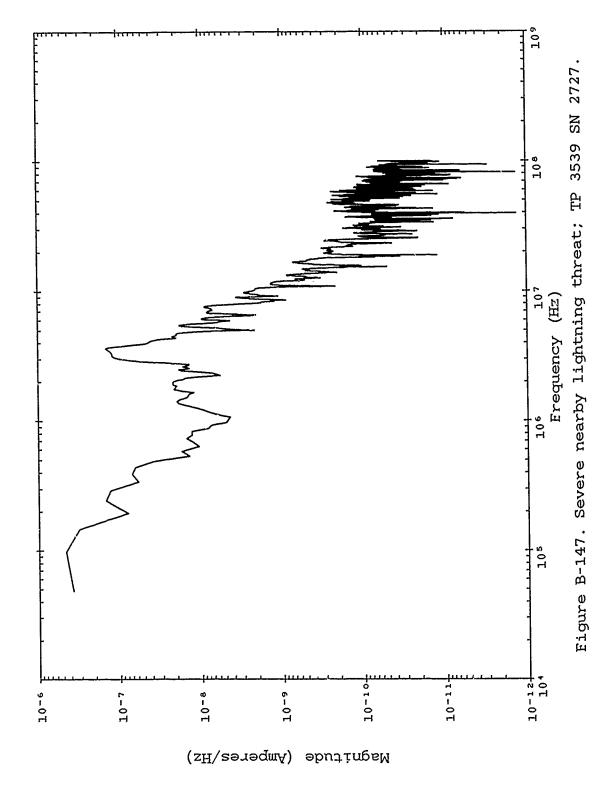


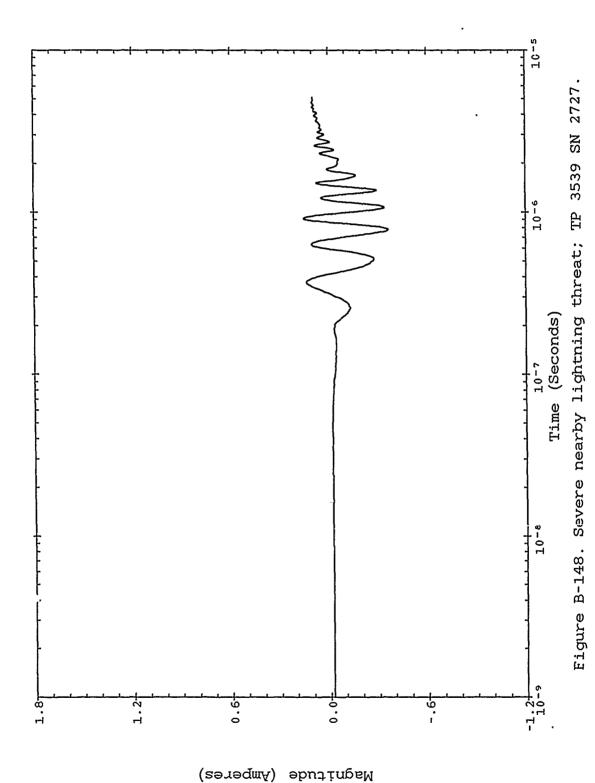


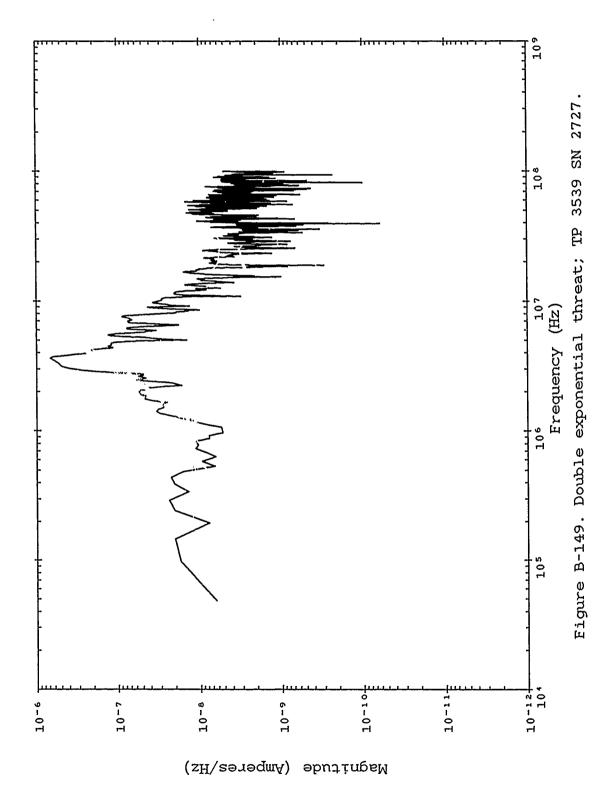
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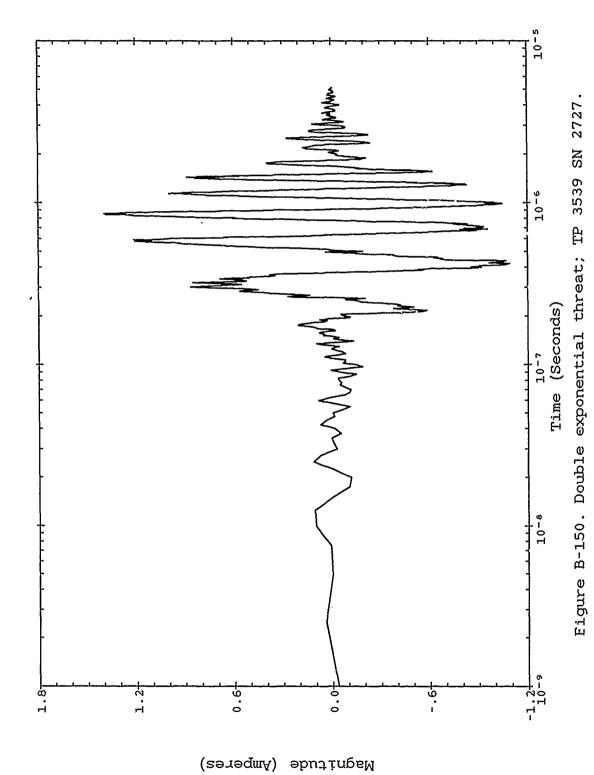


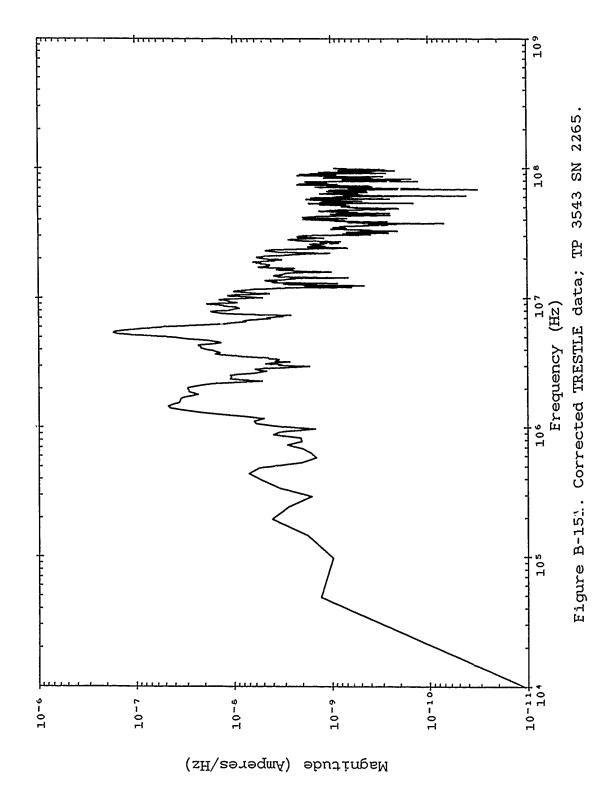


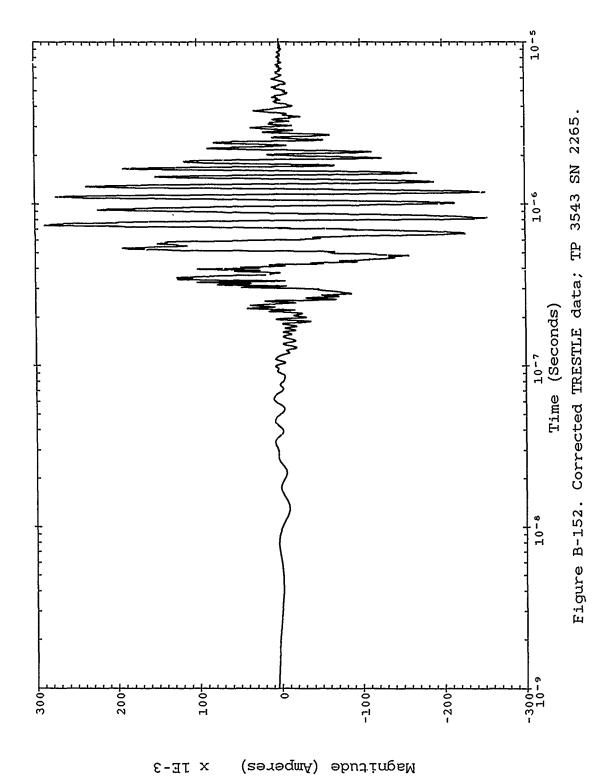


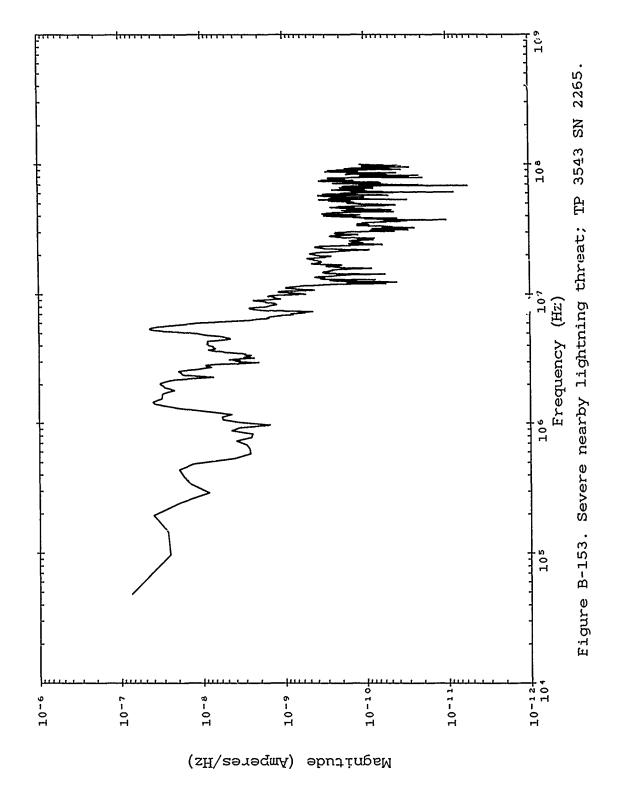


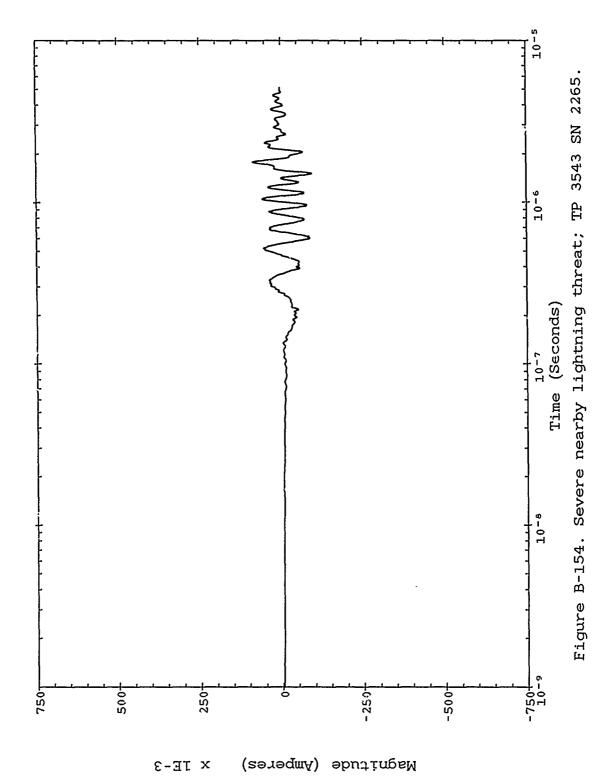


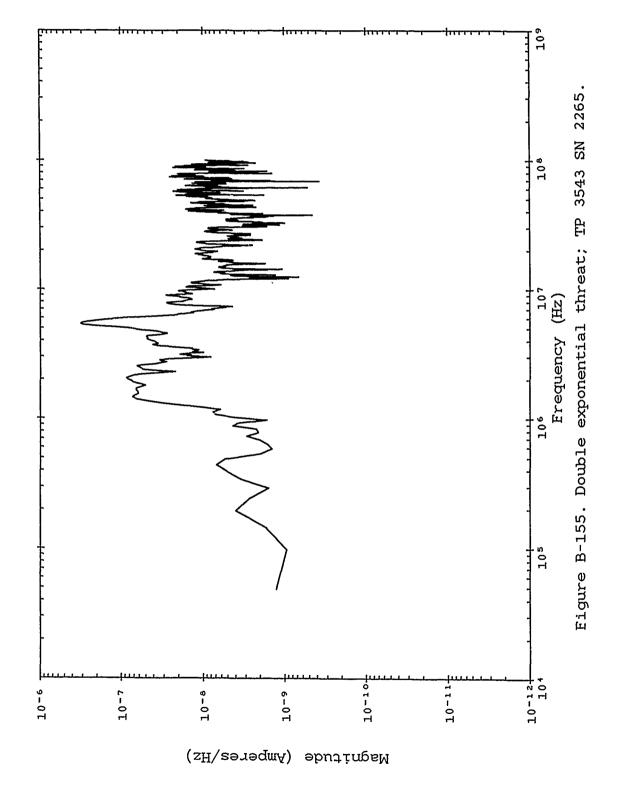


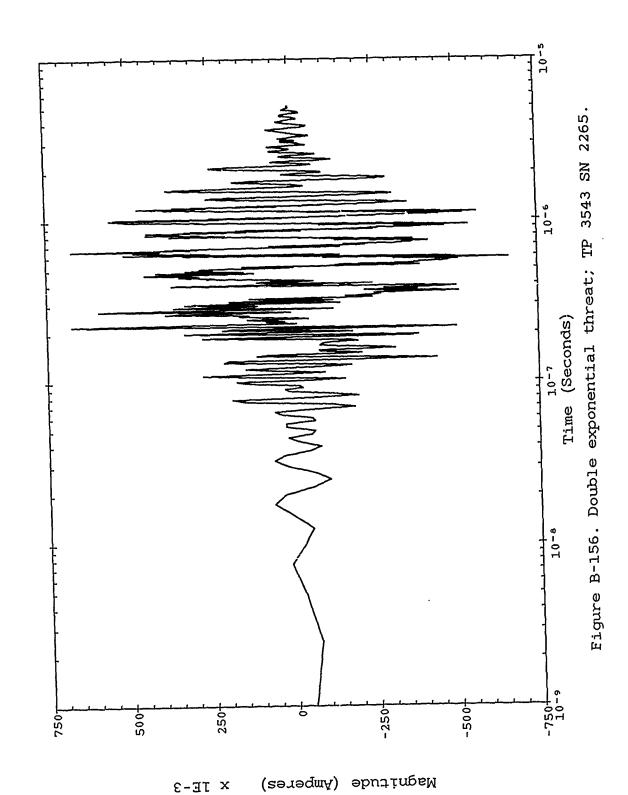


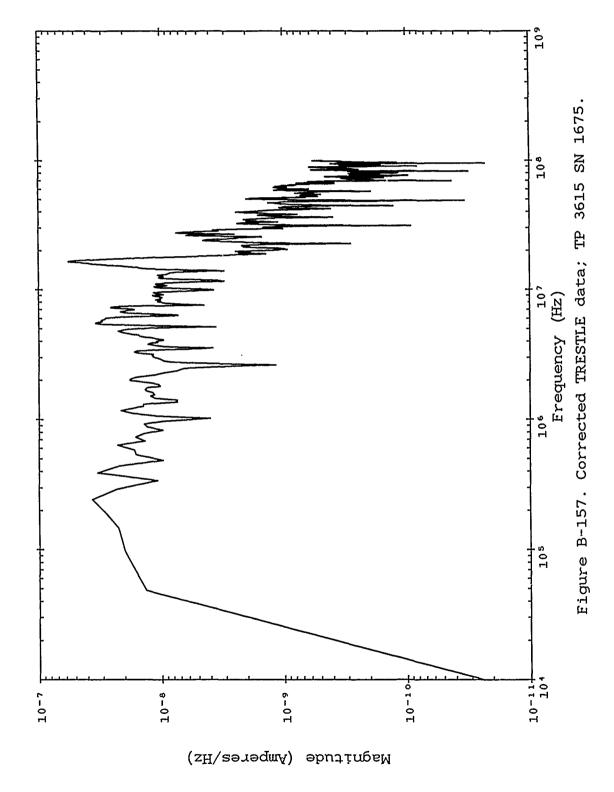


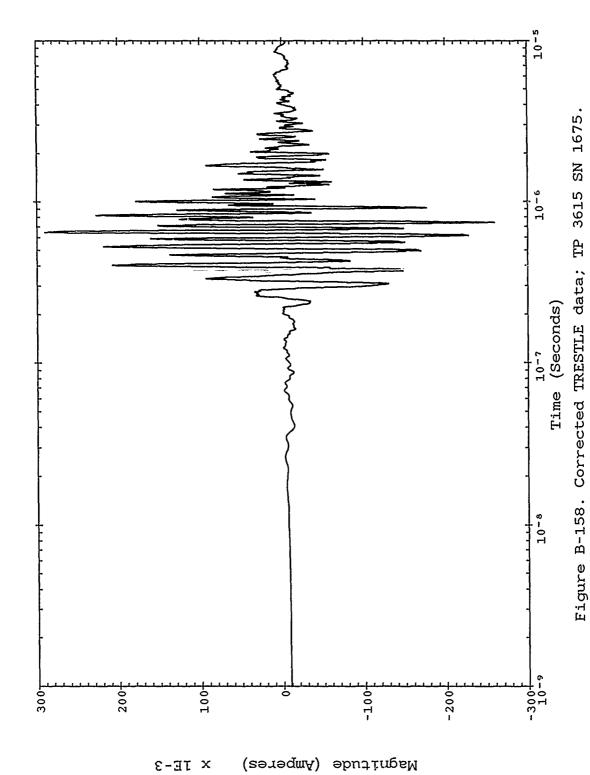




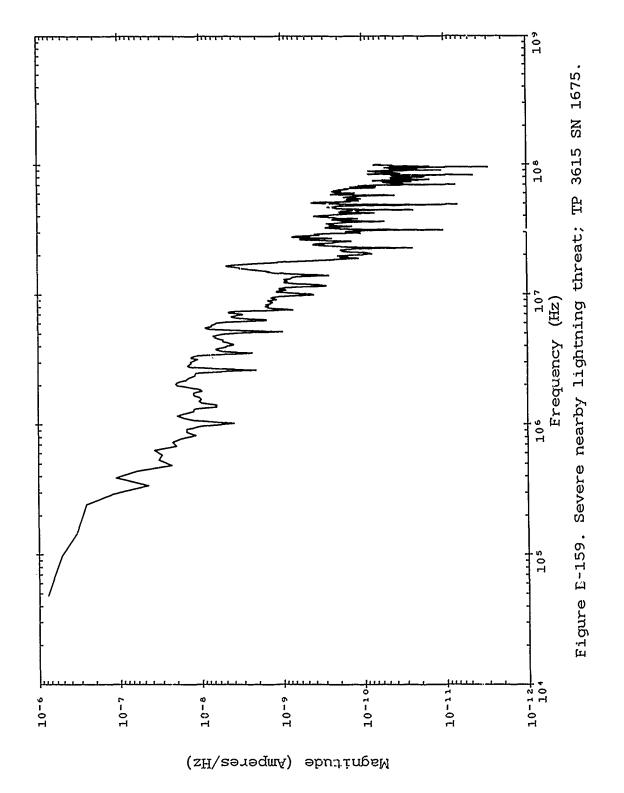


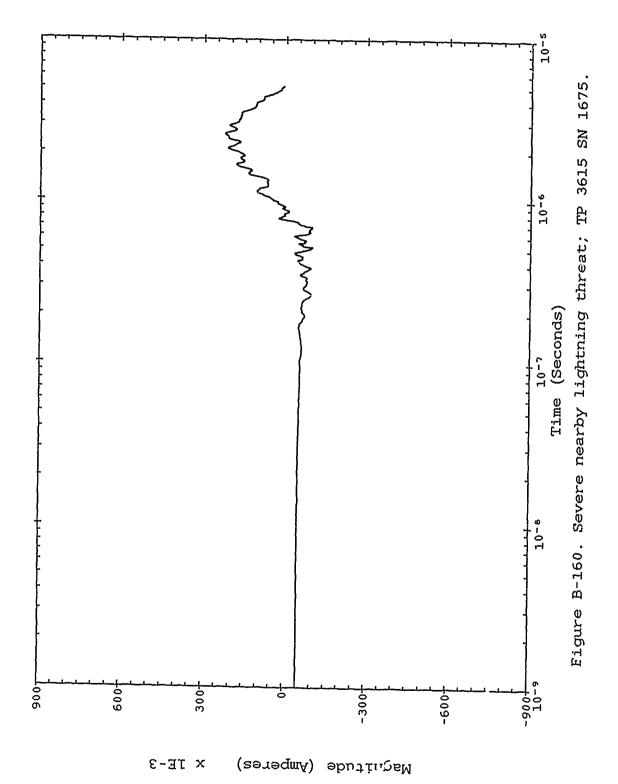


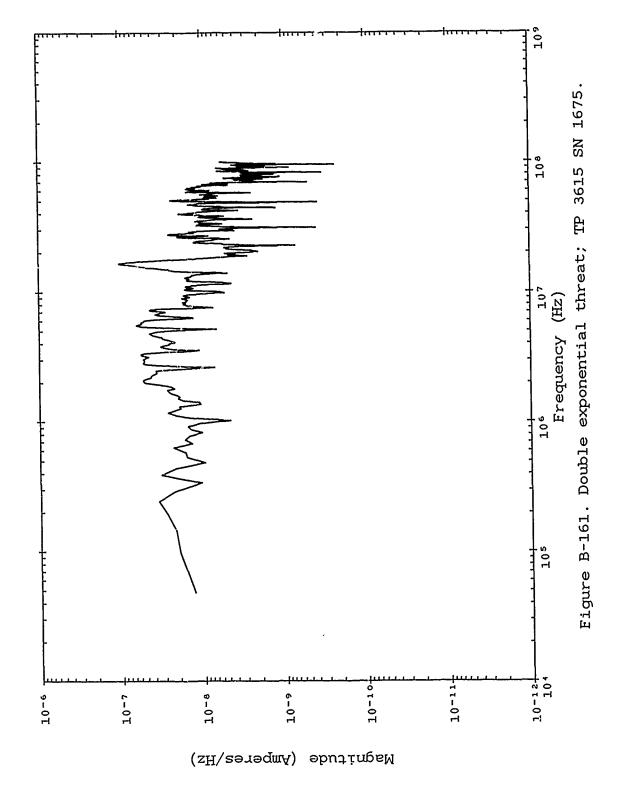


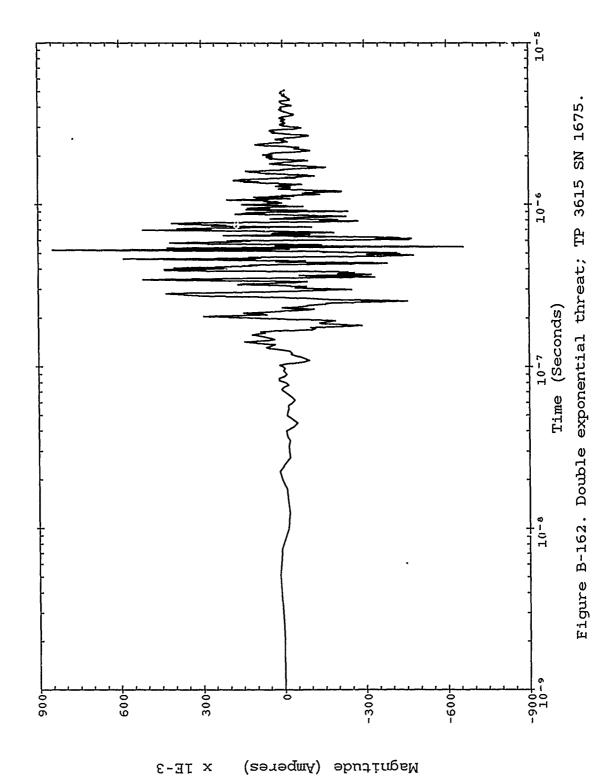


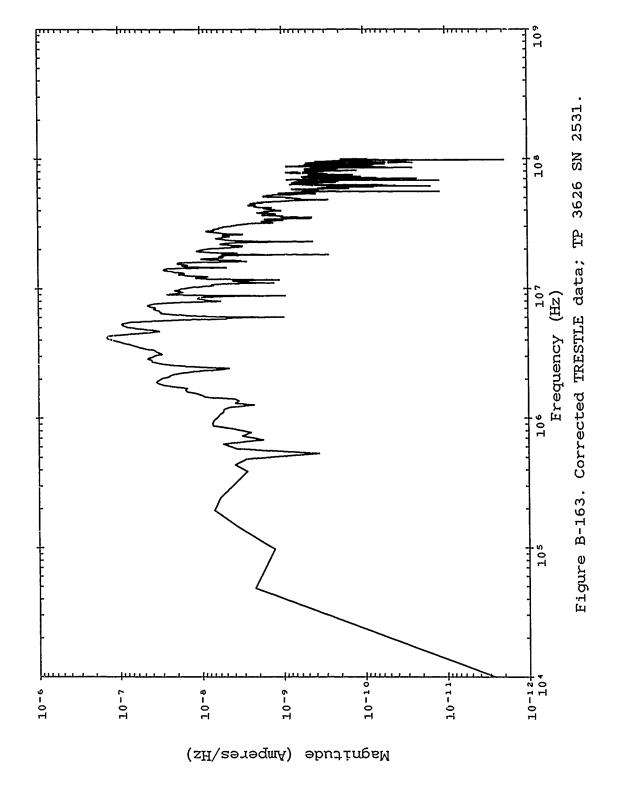
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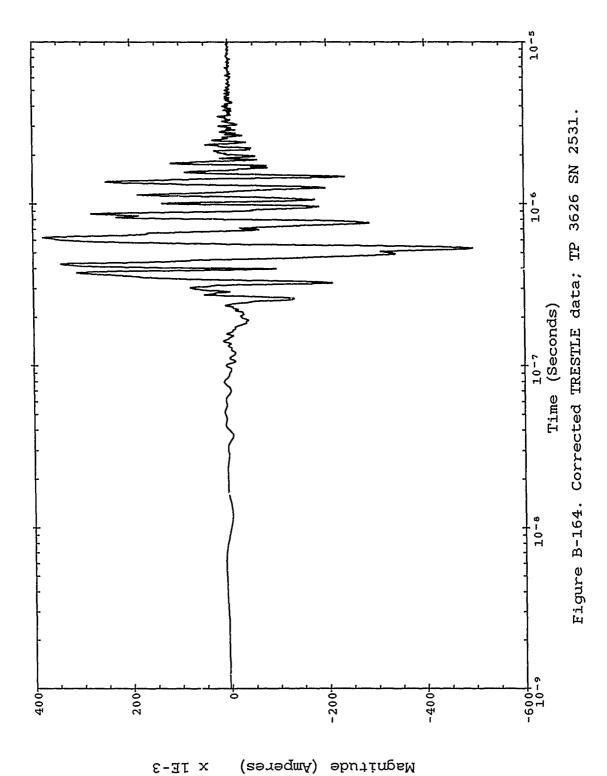


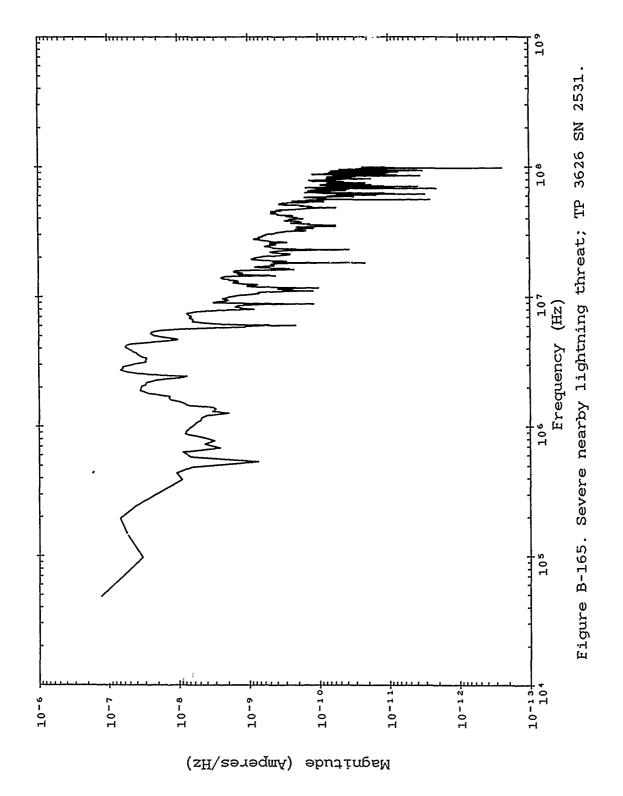


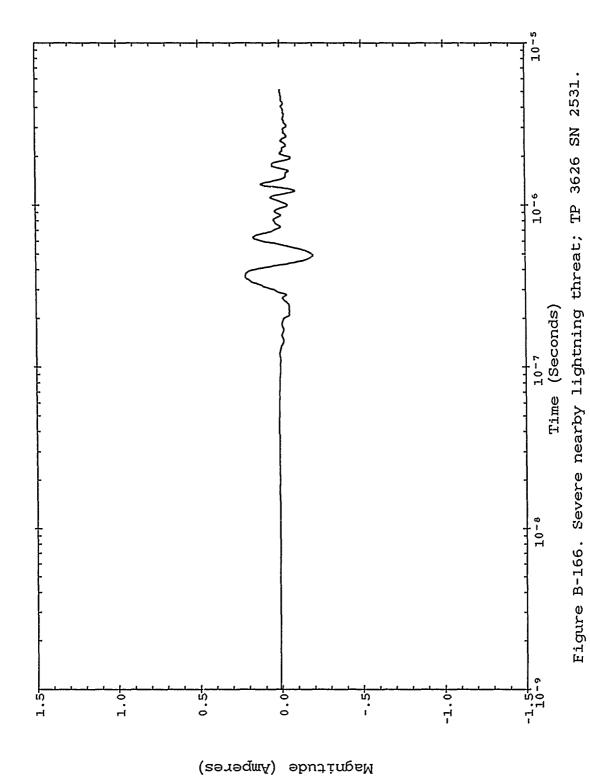






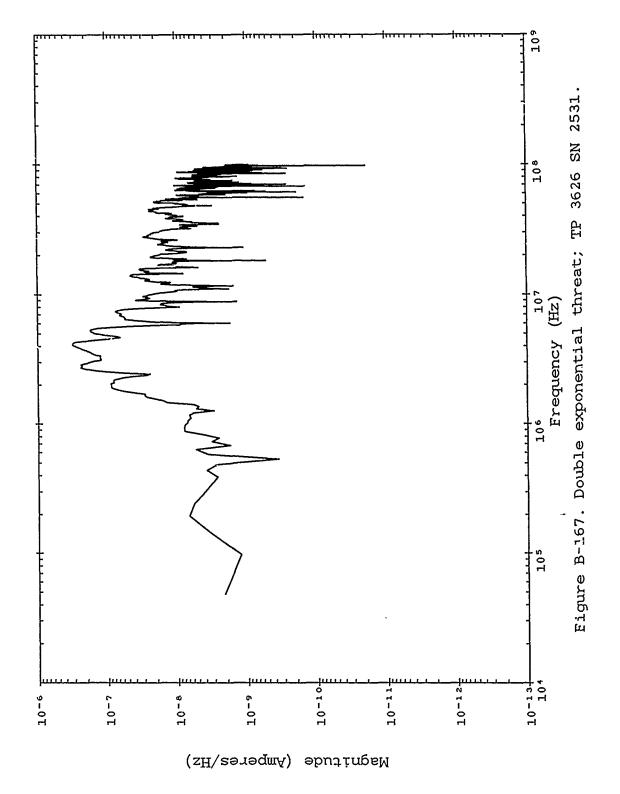


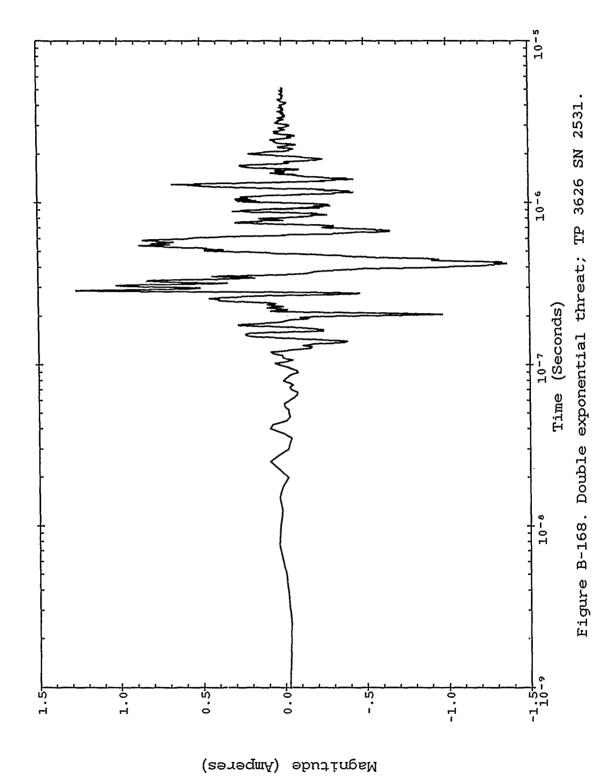


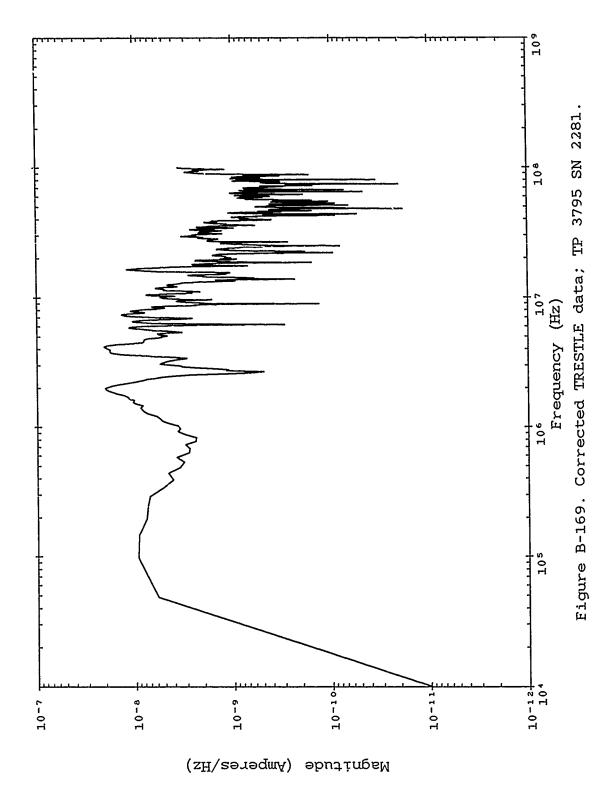


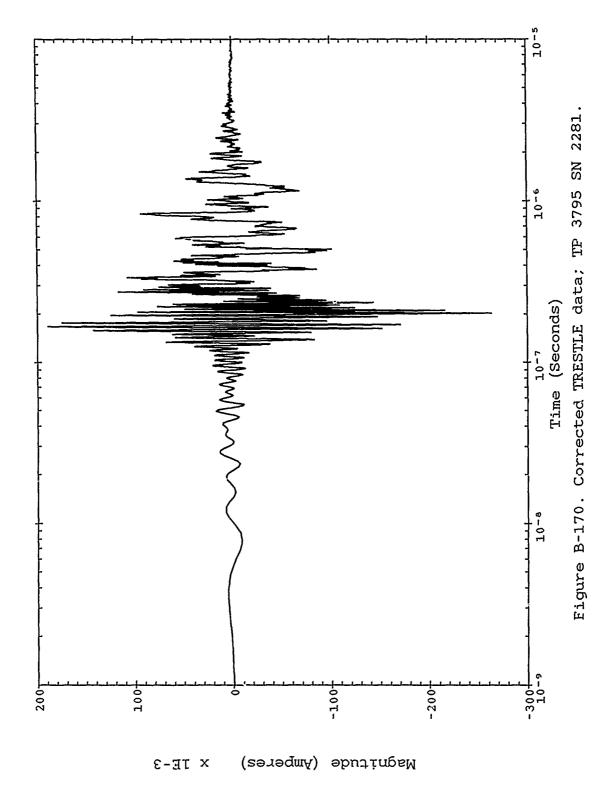
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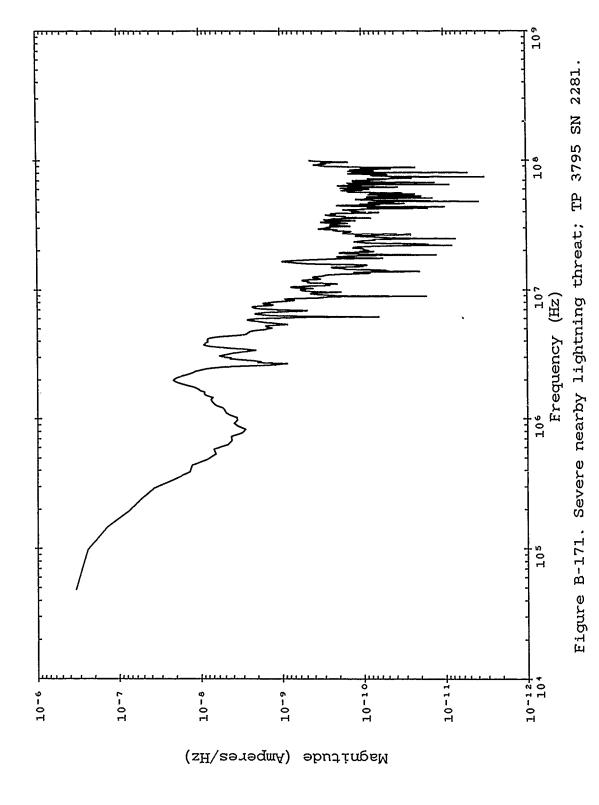
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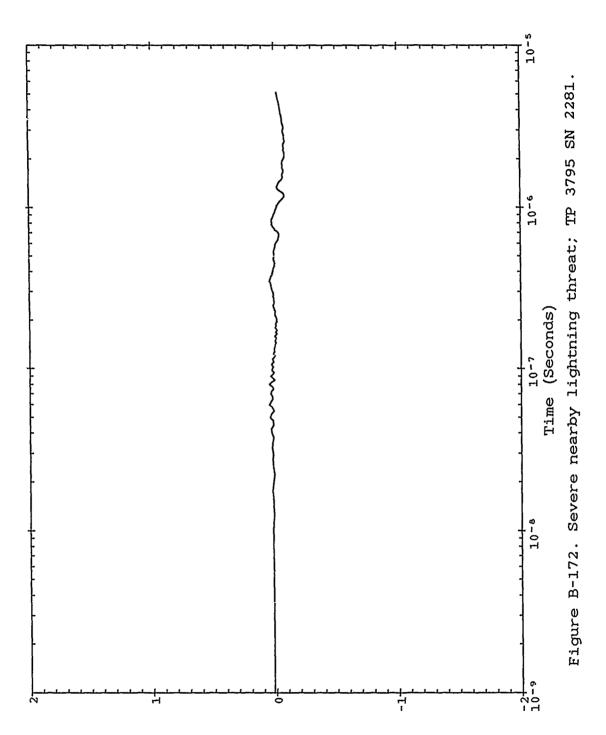




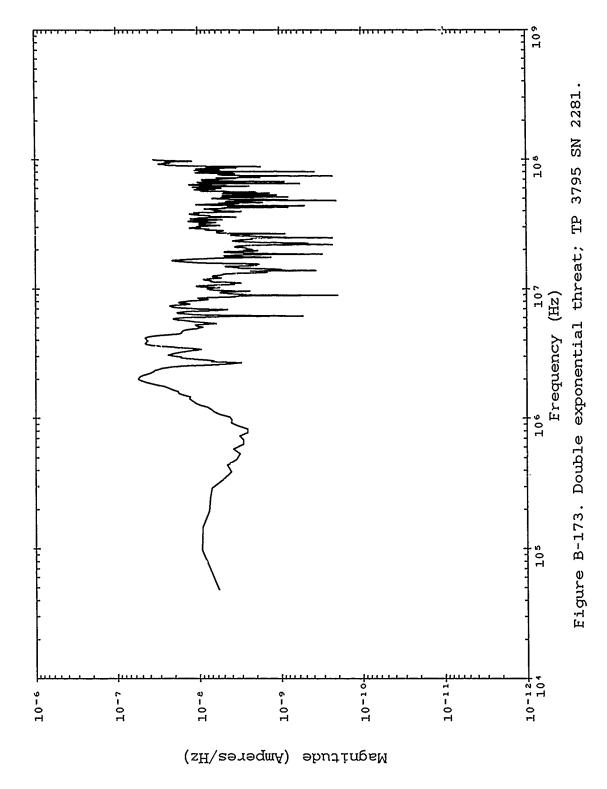


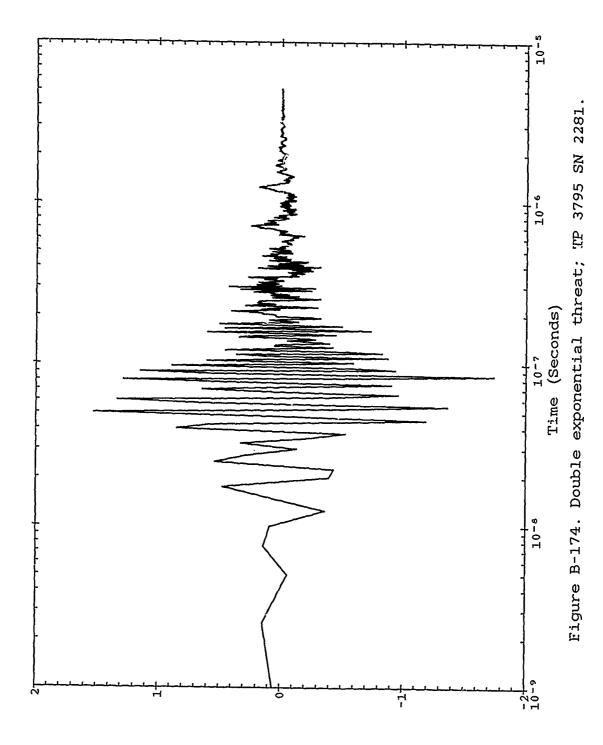




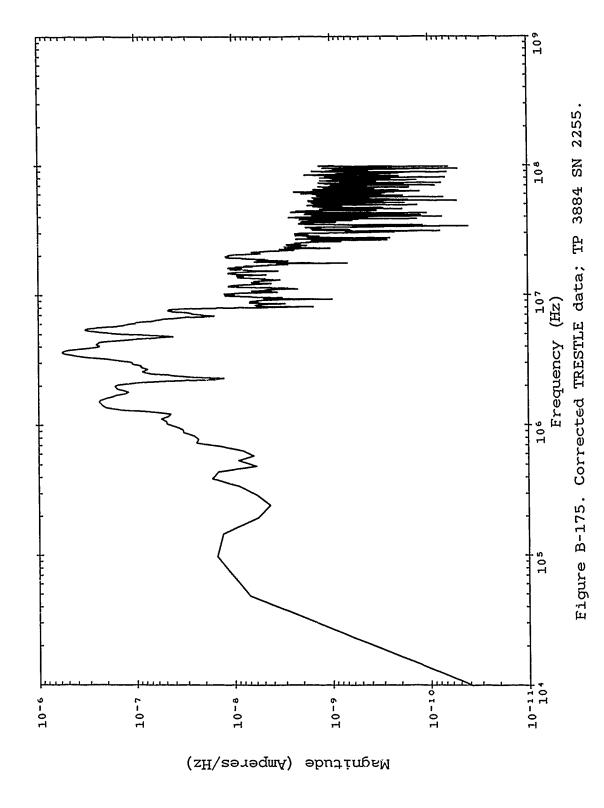


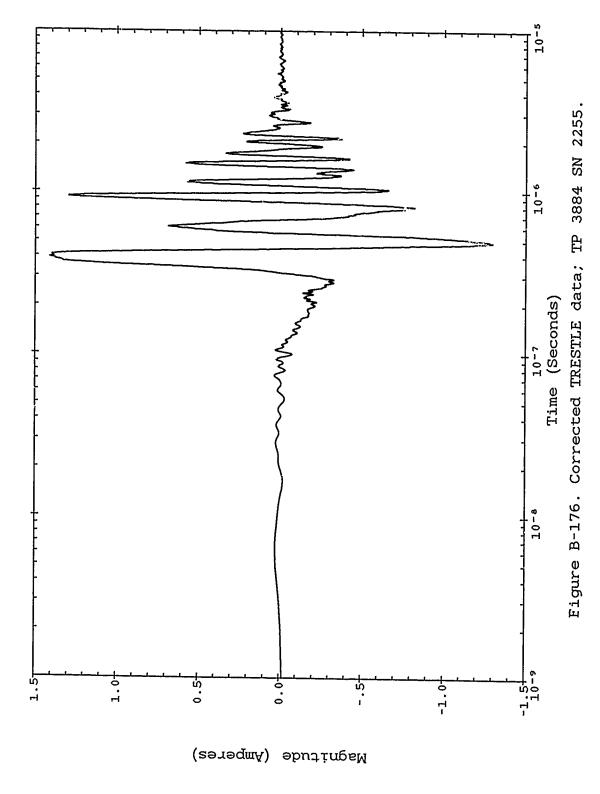
Magnitude (Amperes)

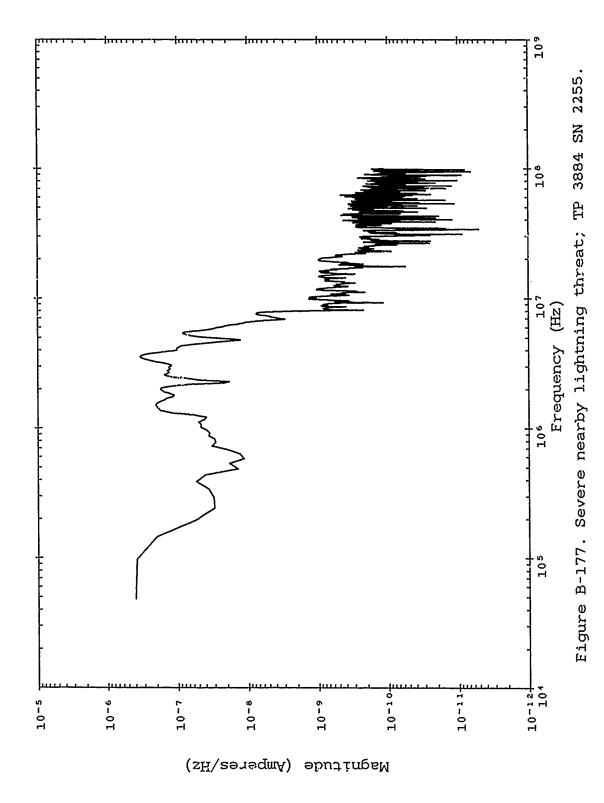


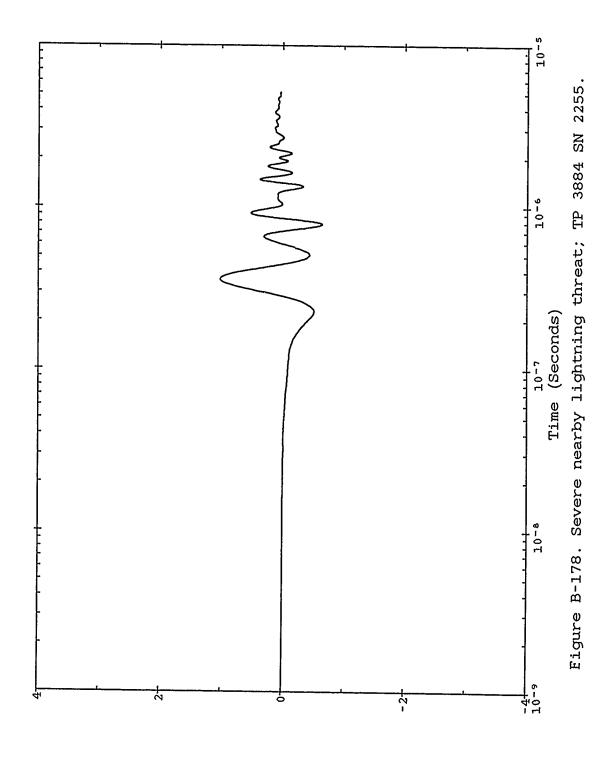


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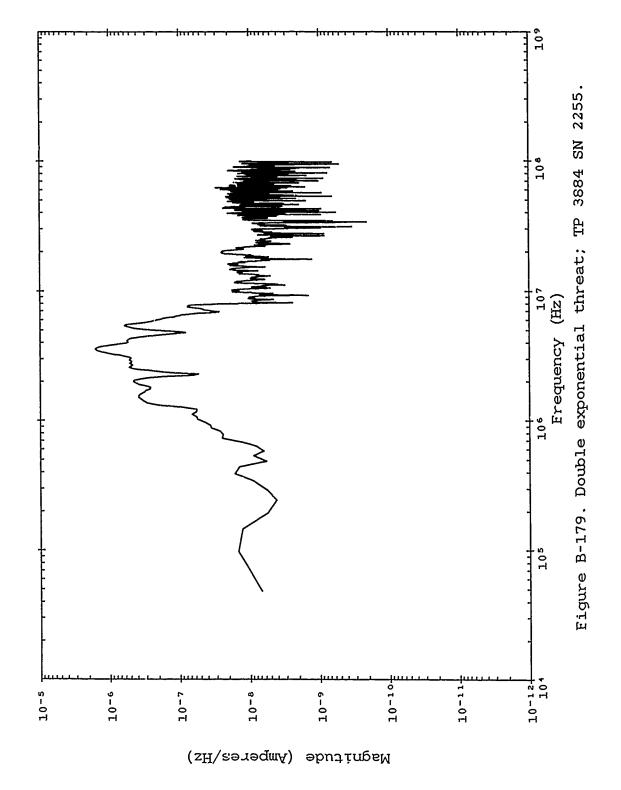








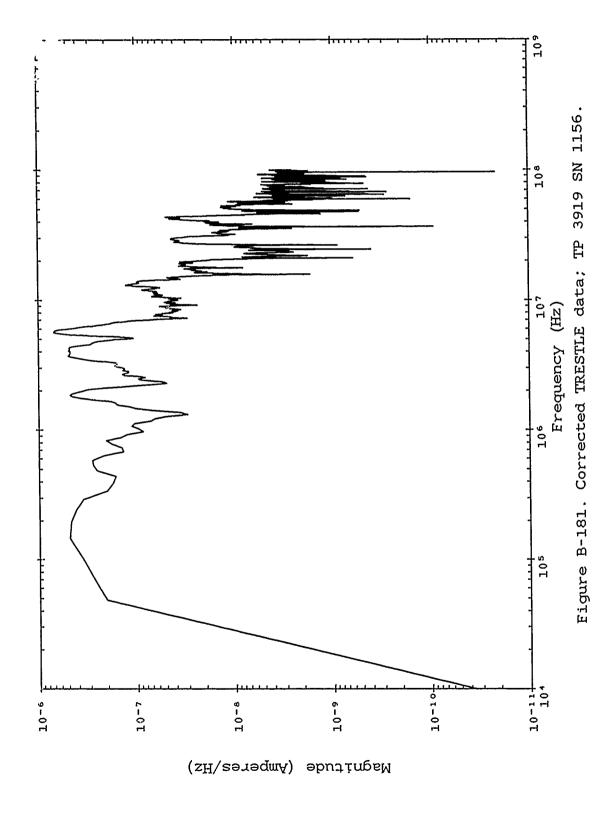
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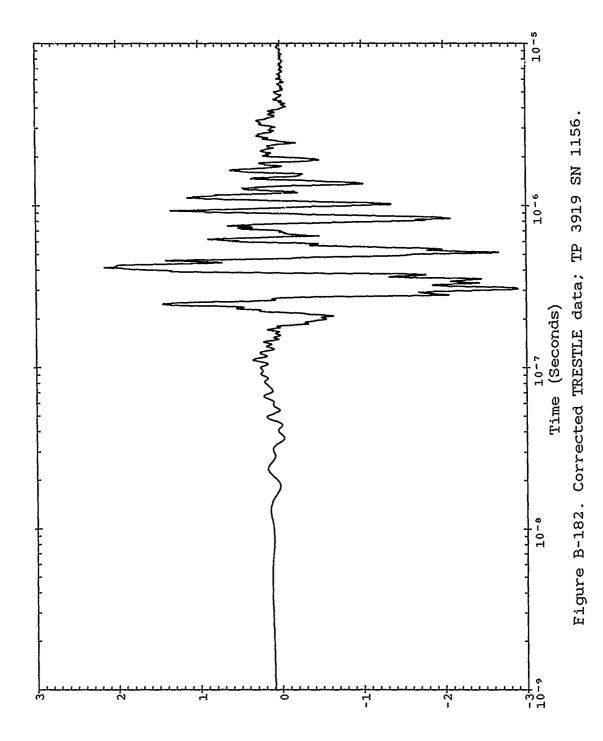


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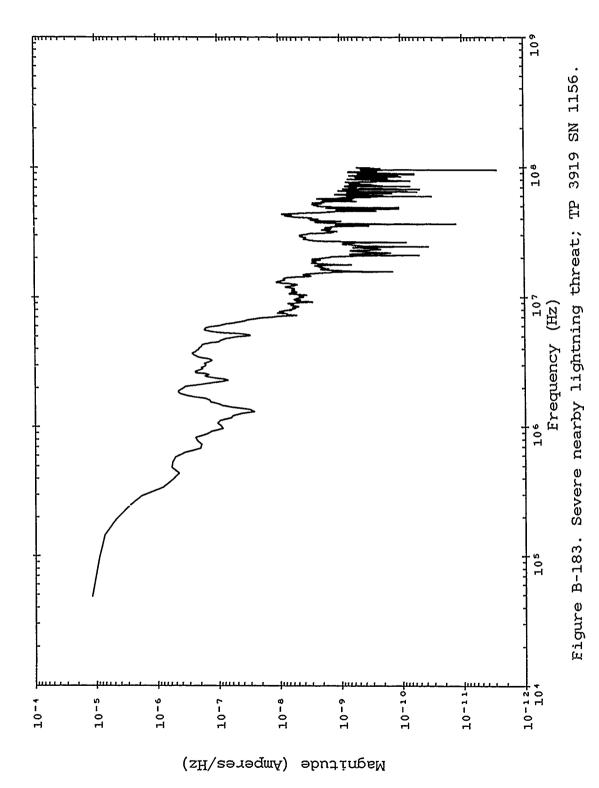
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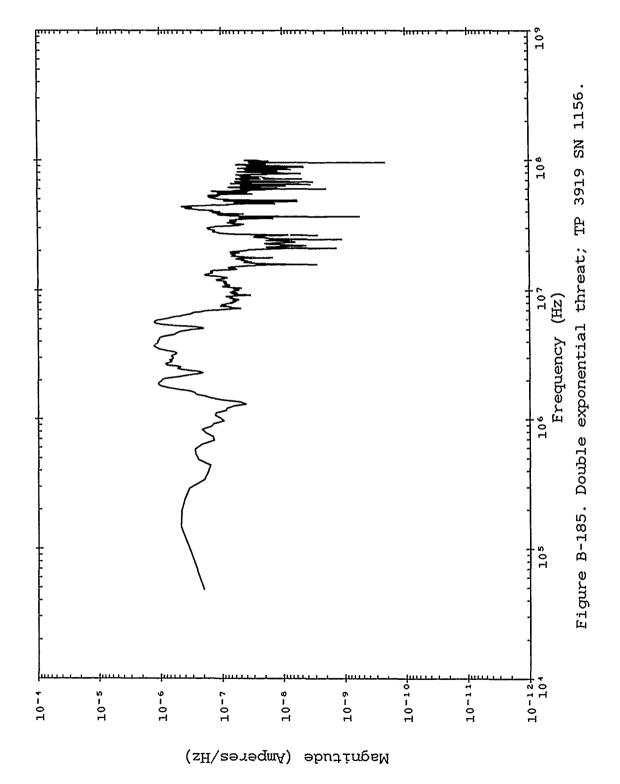


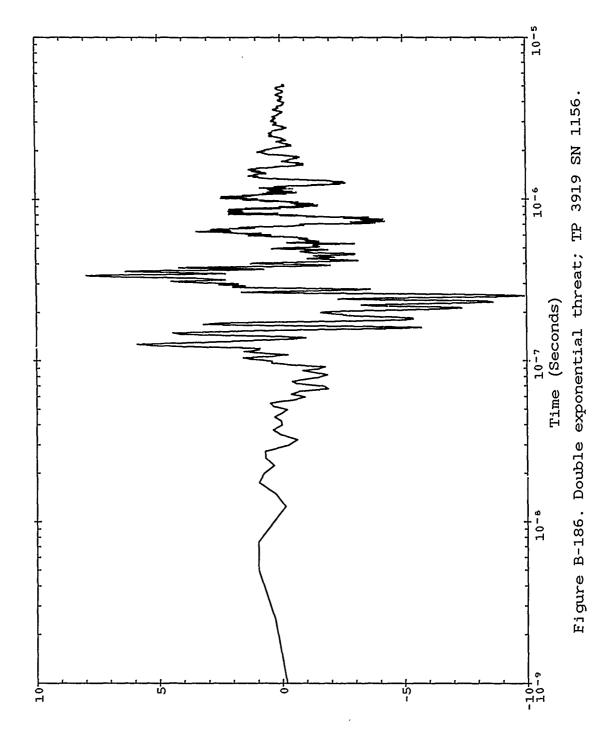


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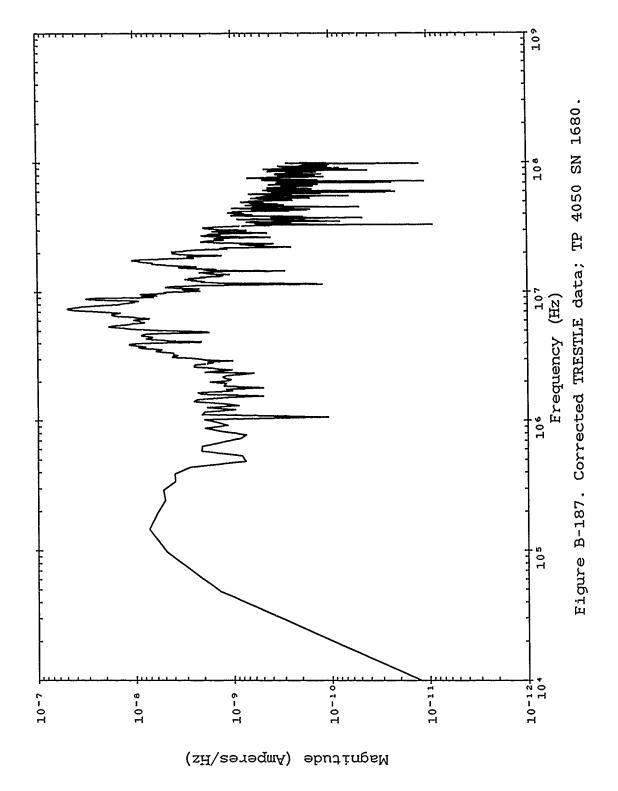
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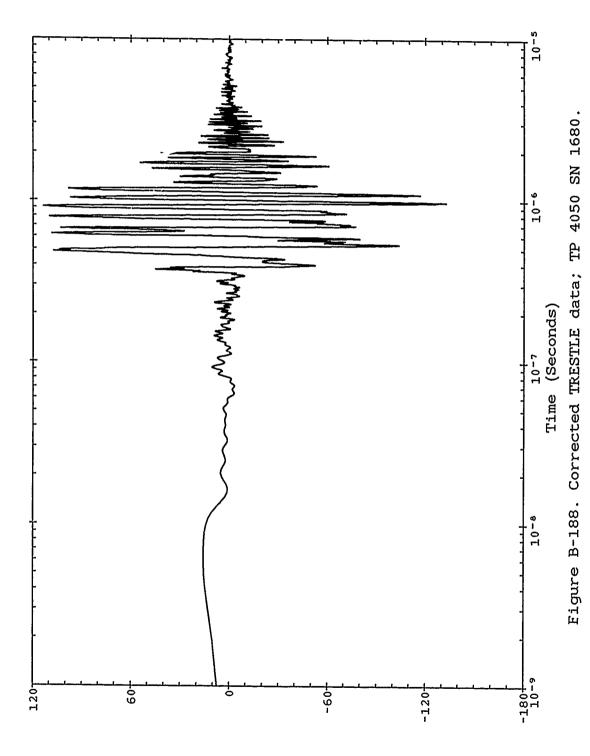




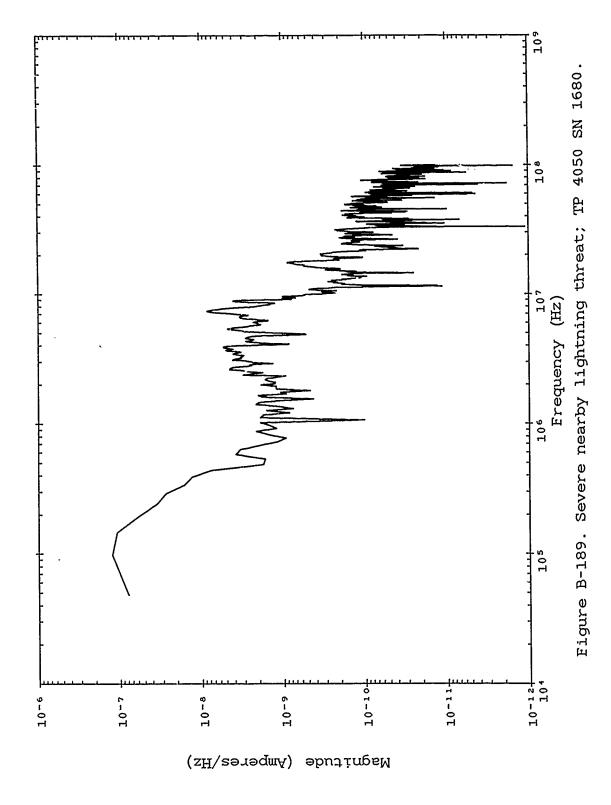


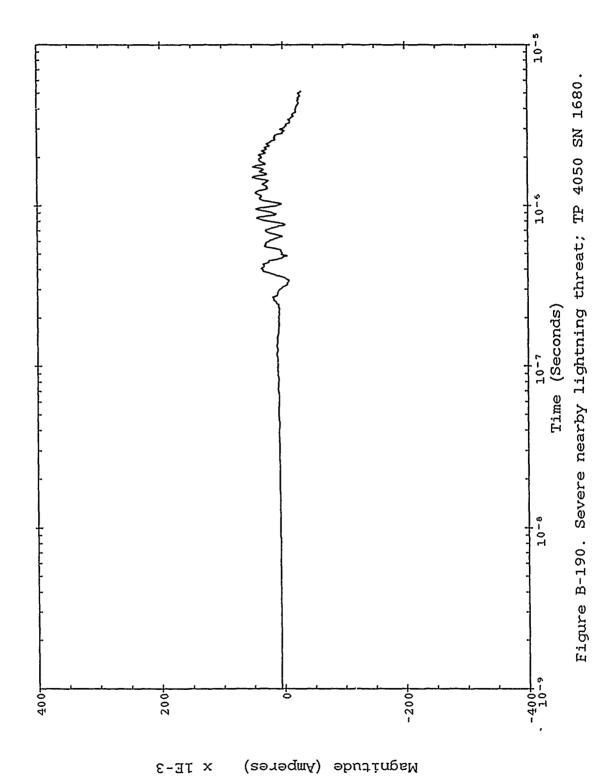
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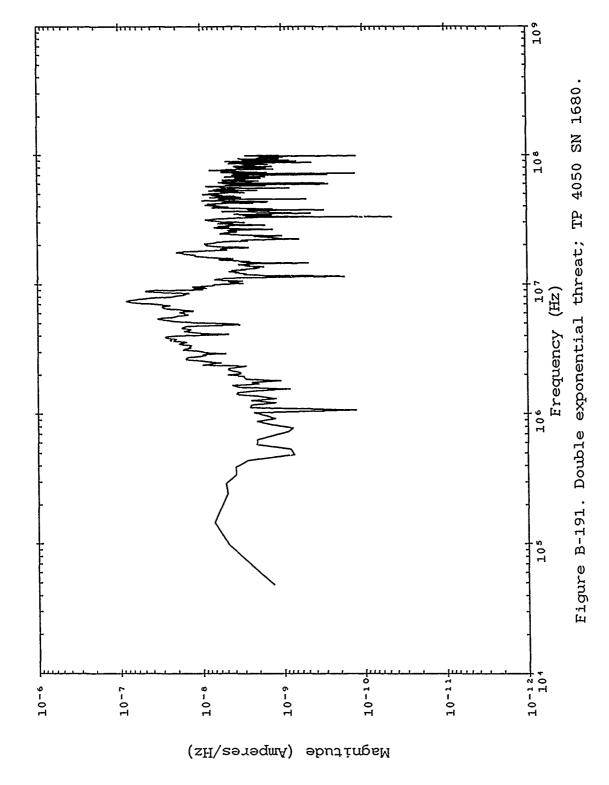


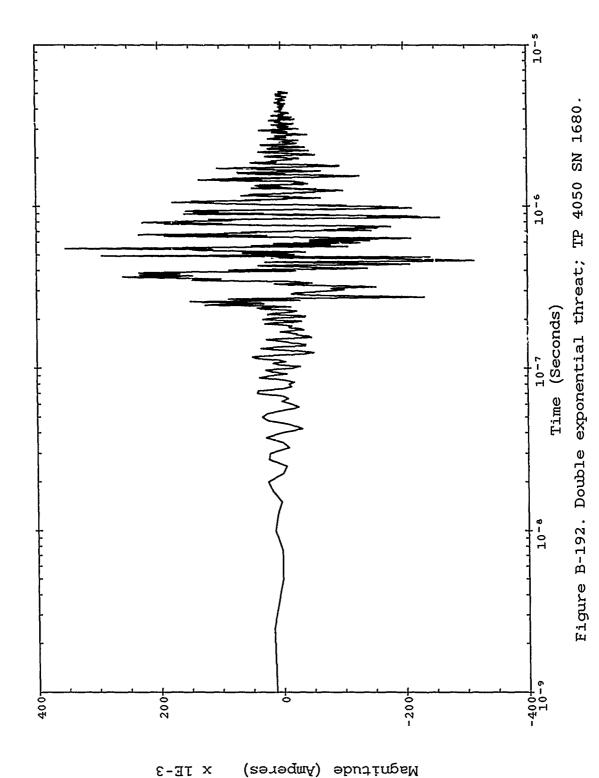


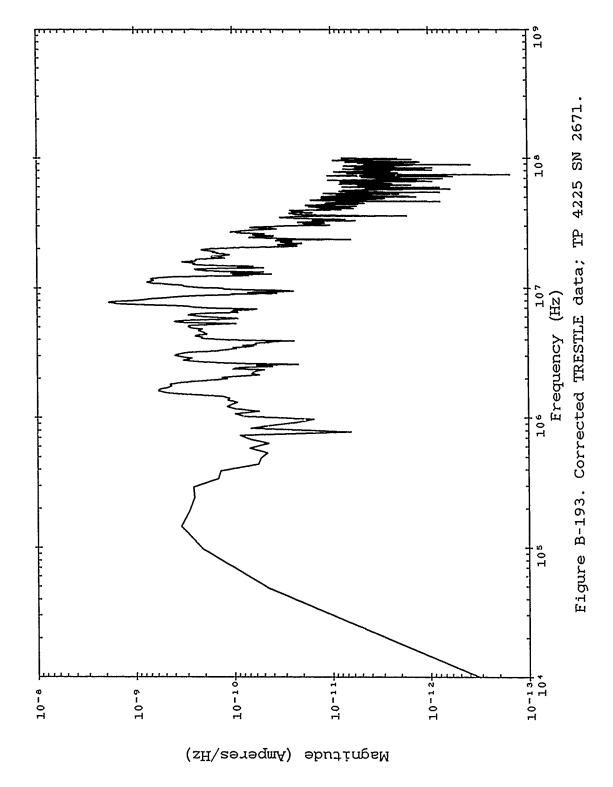
Wagnitude (Amperes) \times 1E-3

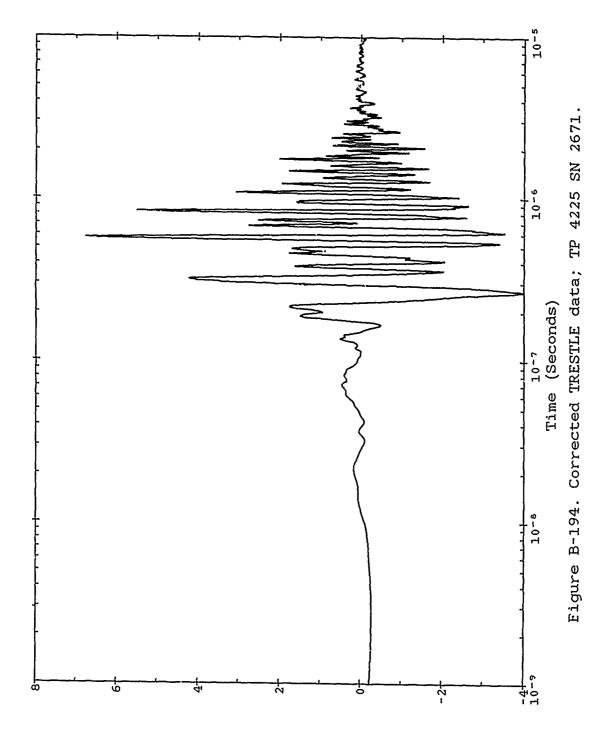


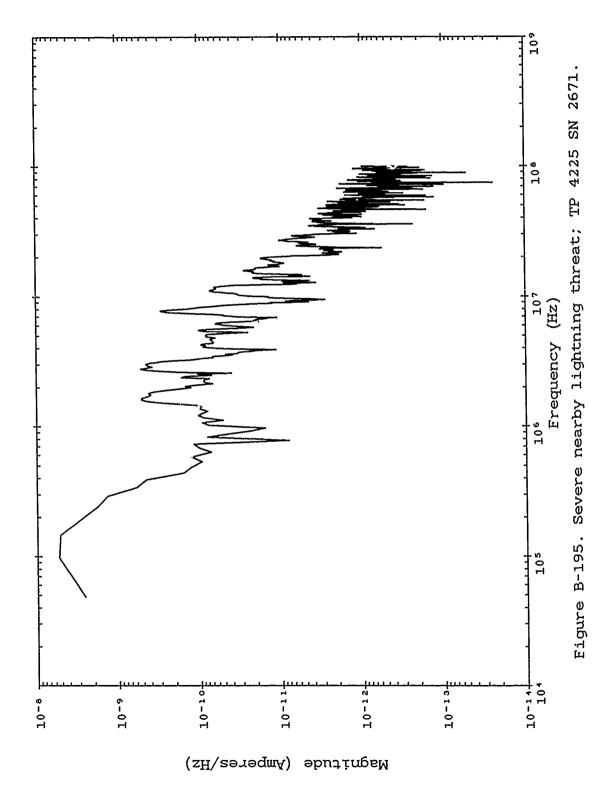


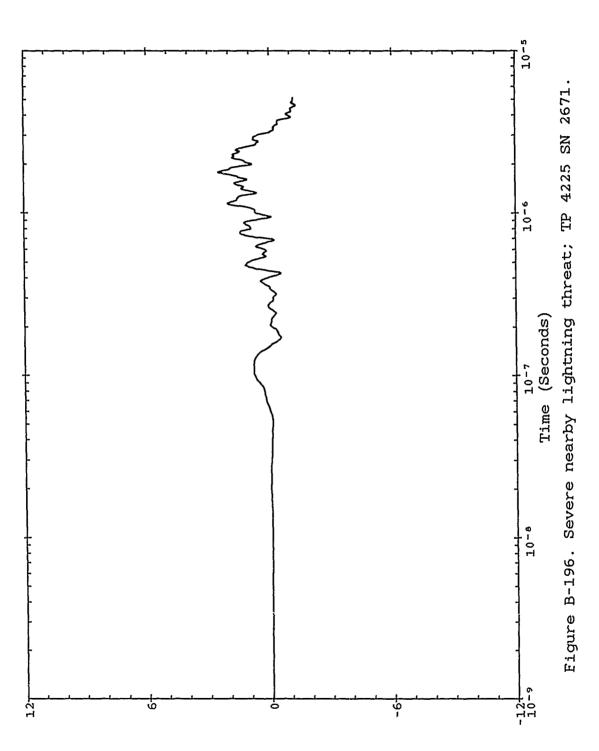




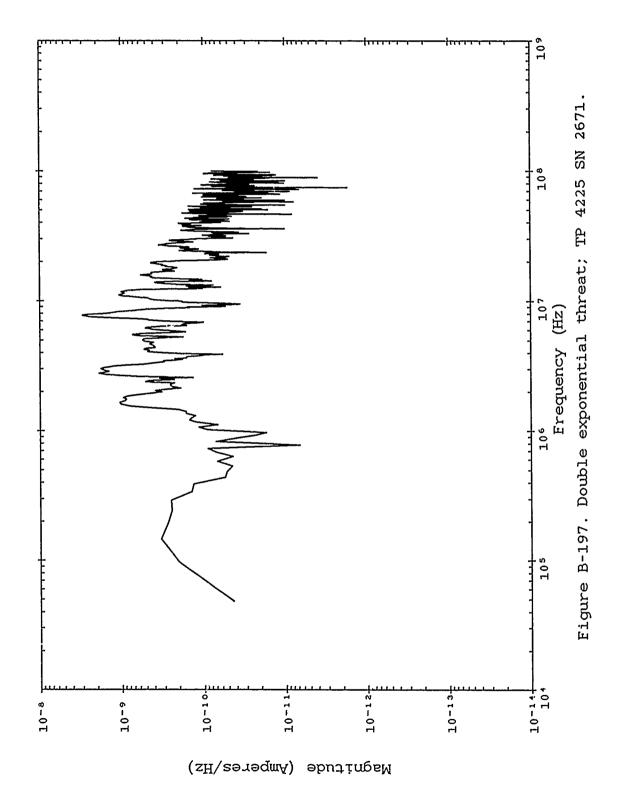


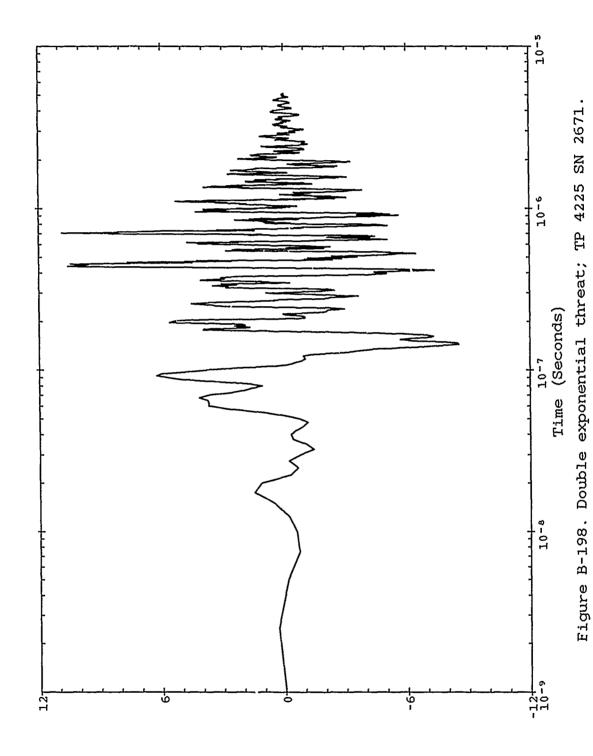






Magnitude (Amperes) x 1E-3

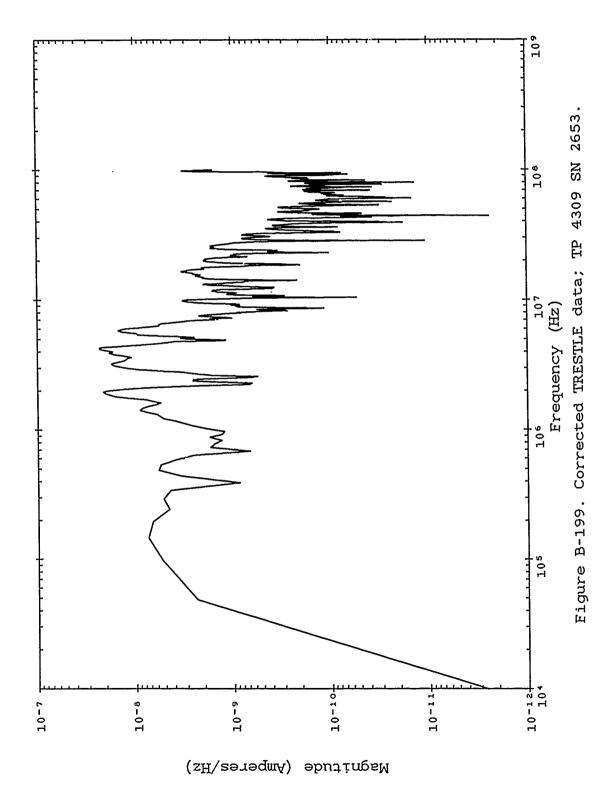


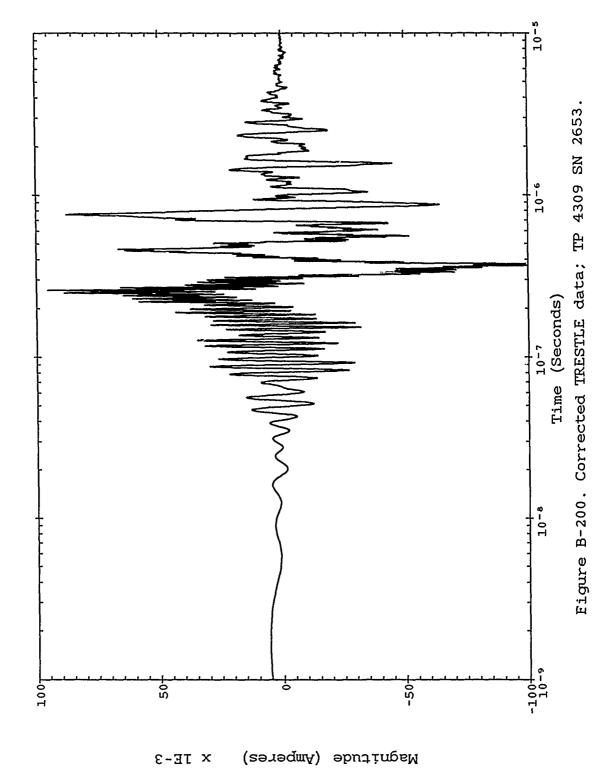


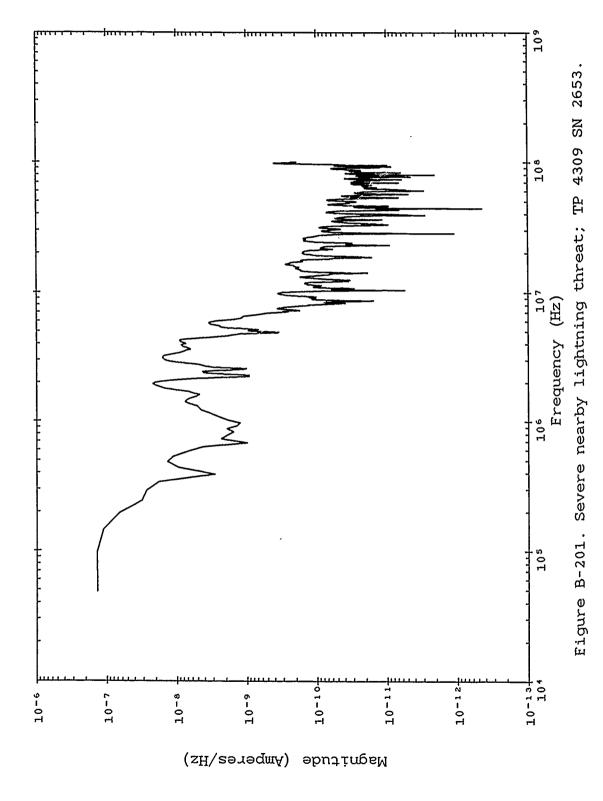
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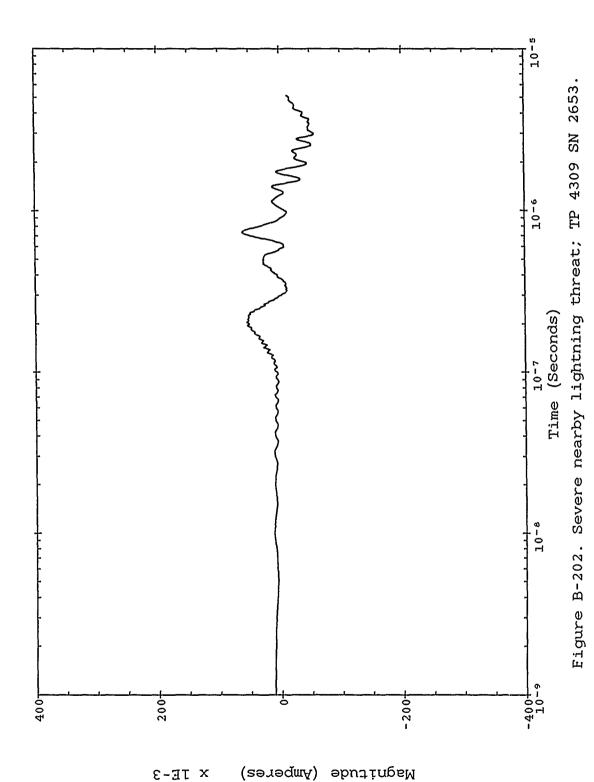
Magnitude (Amperes)

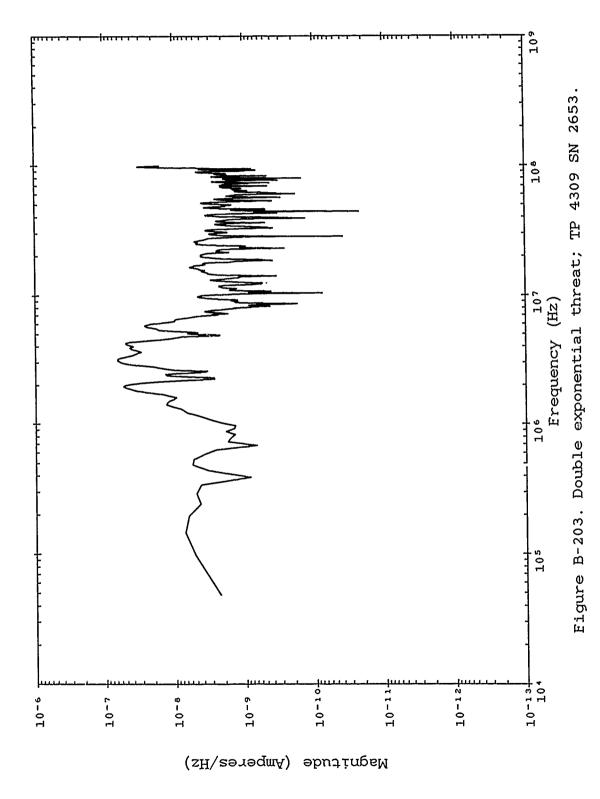
x JE-3

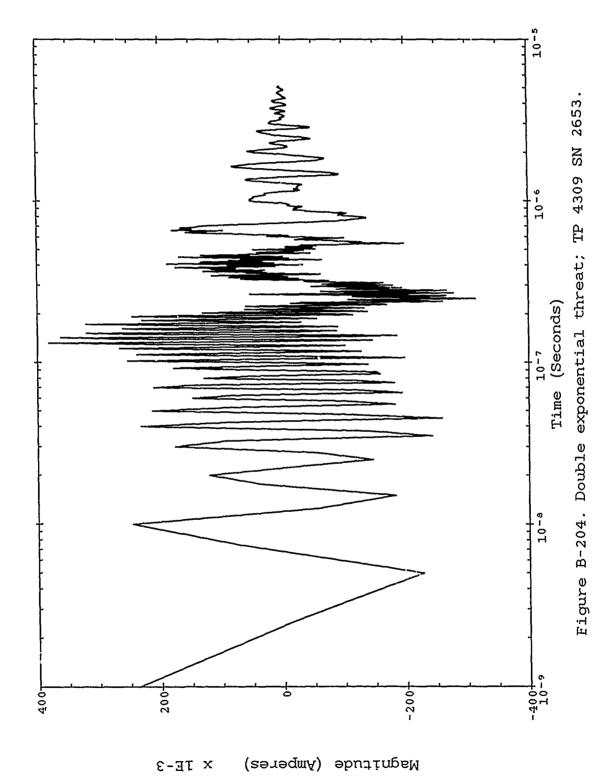




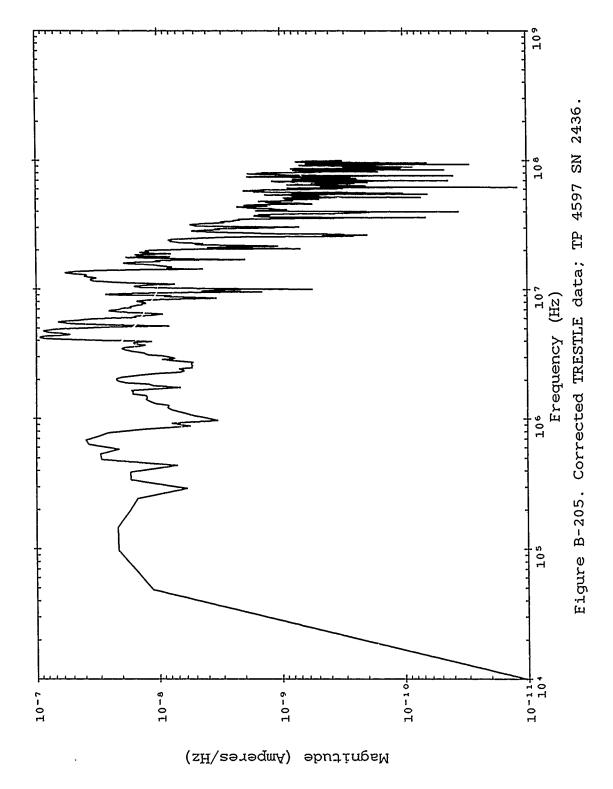


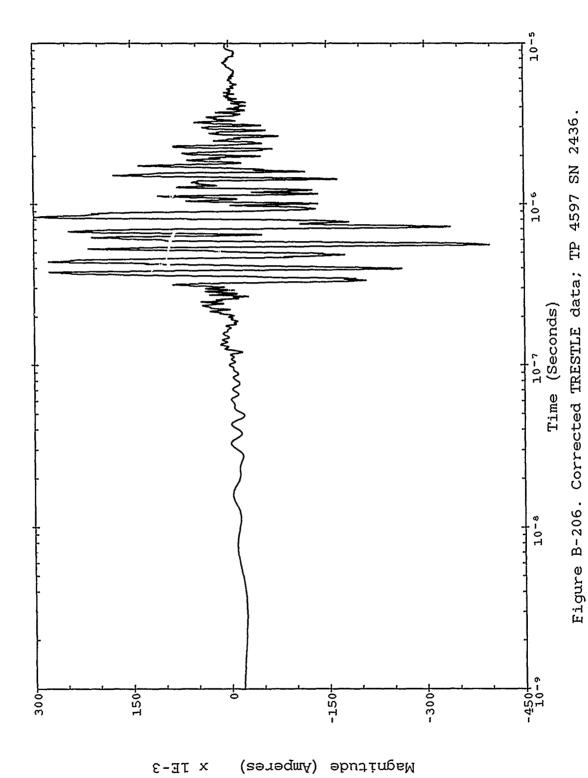


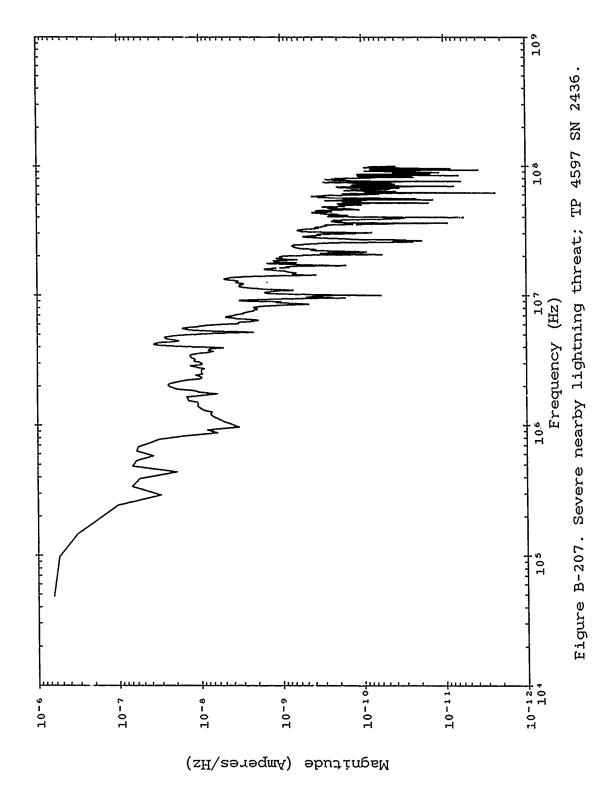


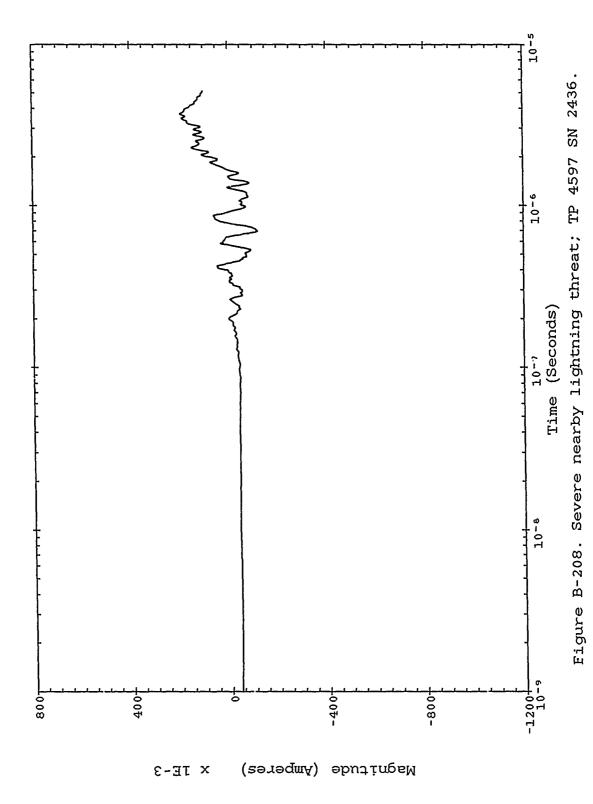


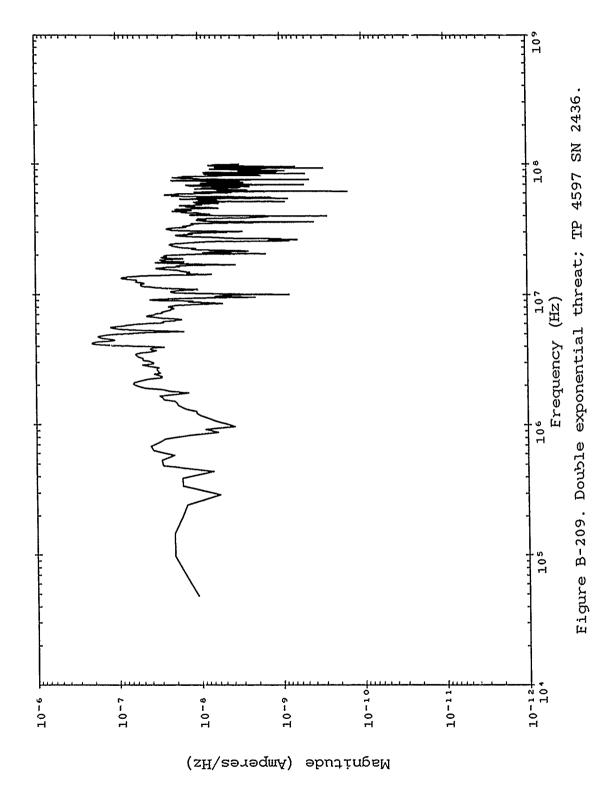
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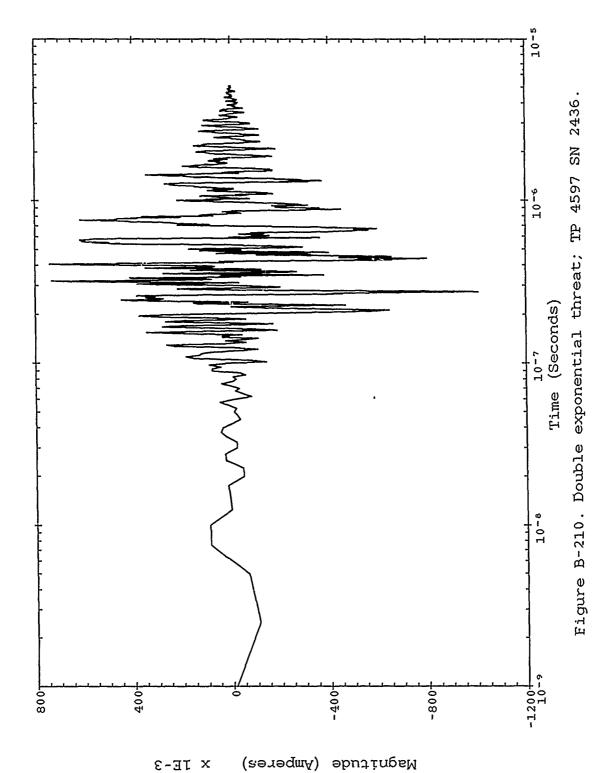


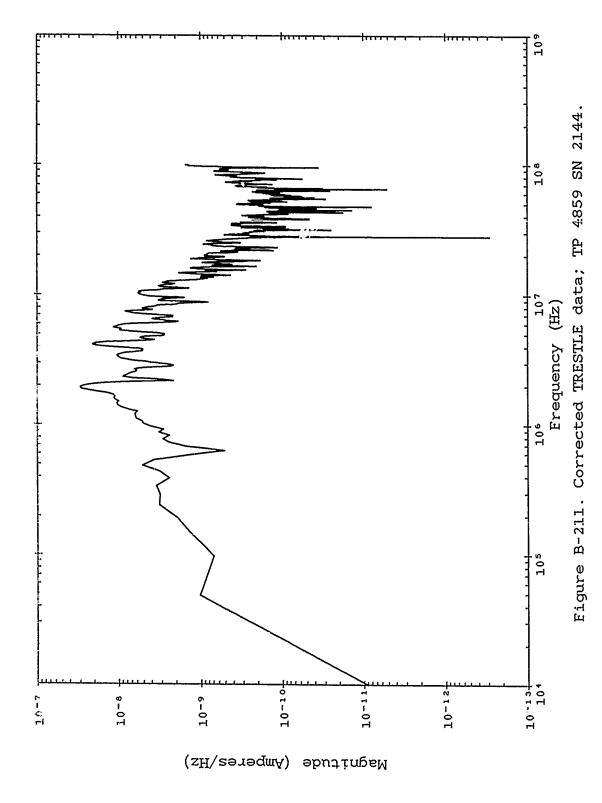


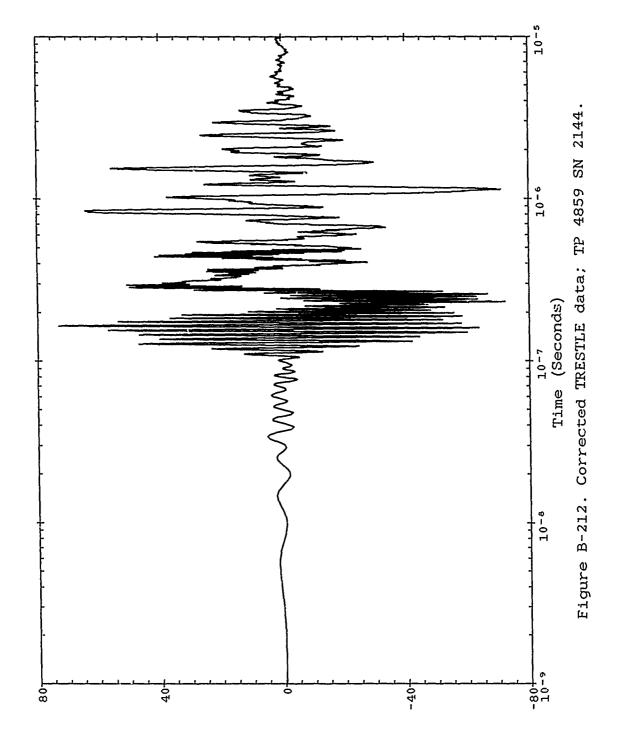




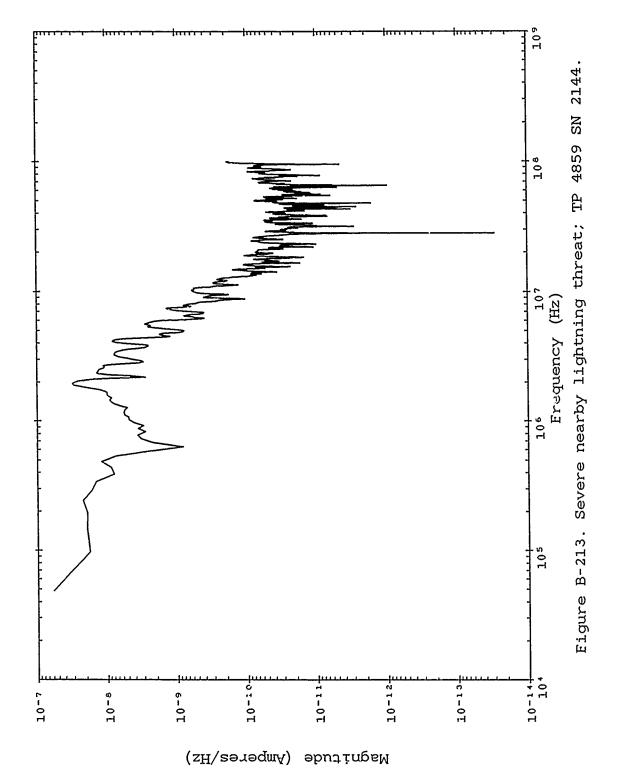


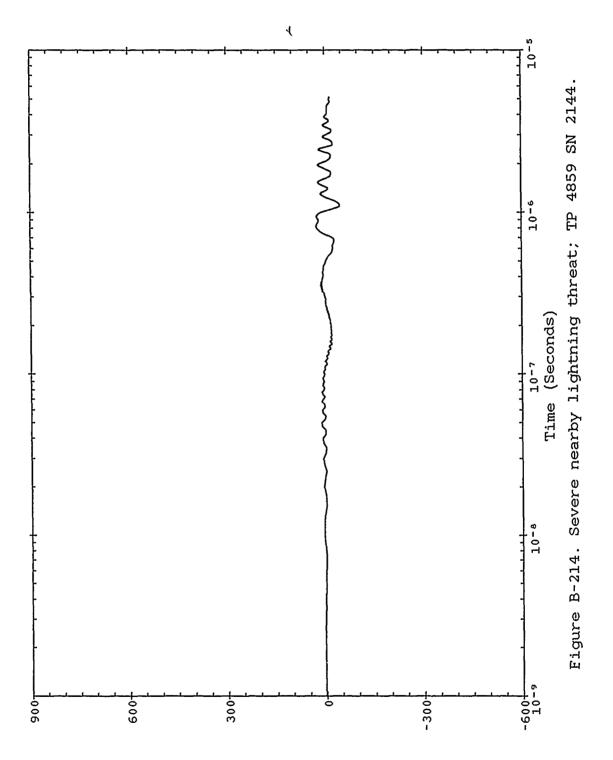






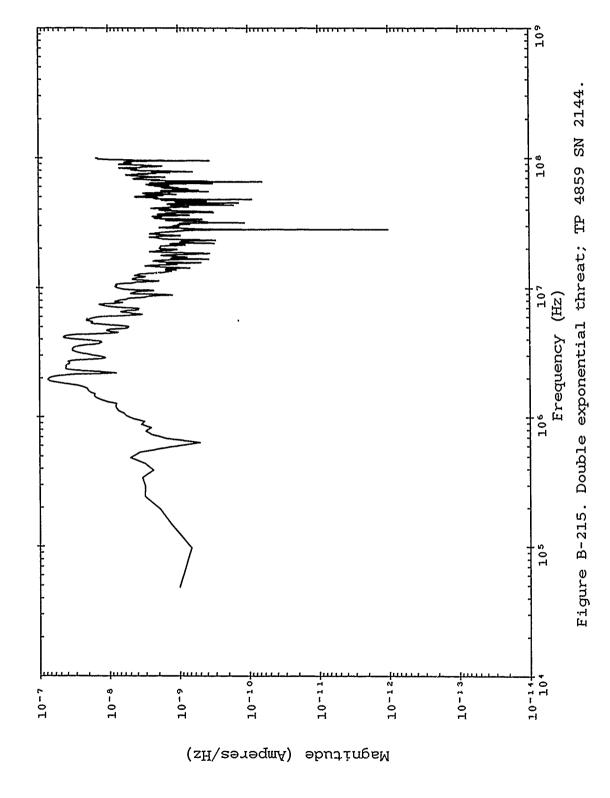
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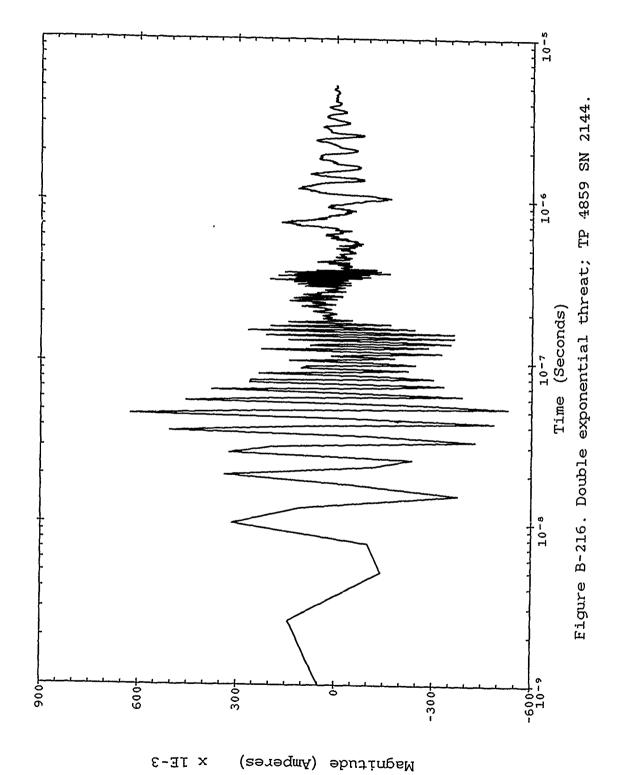


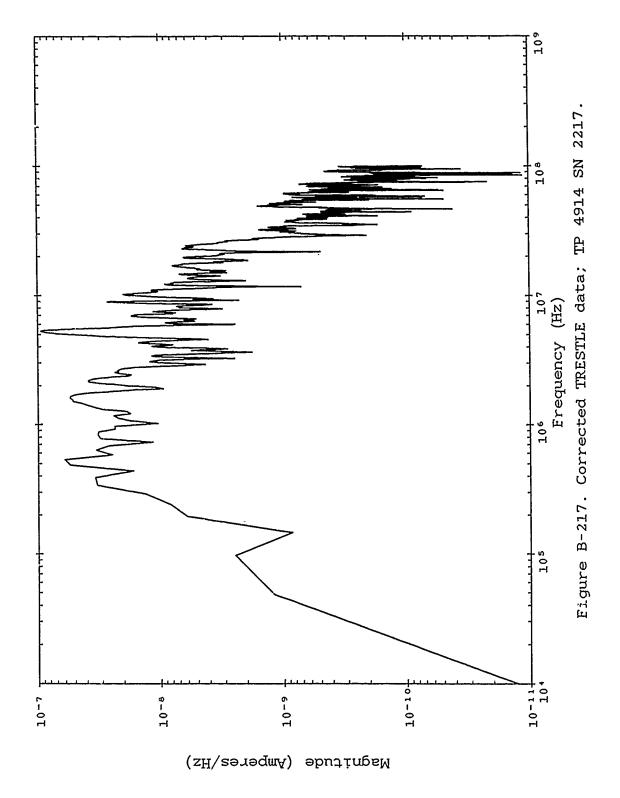


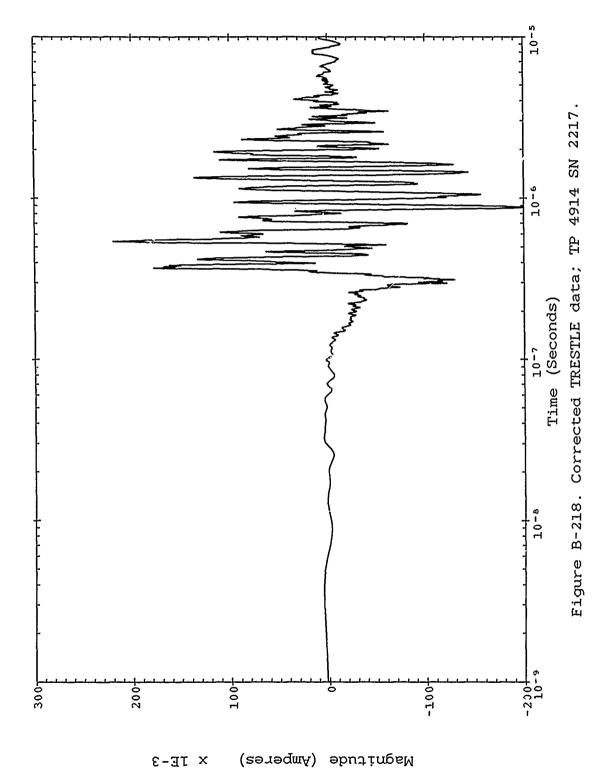
Magnitude (Amperes)

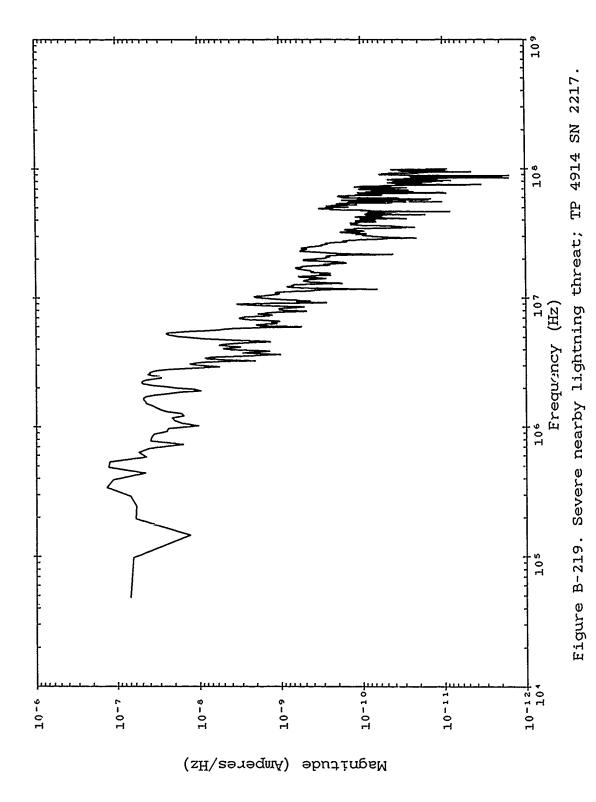
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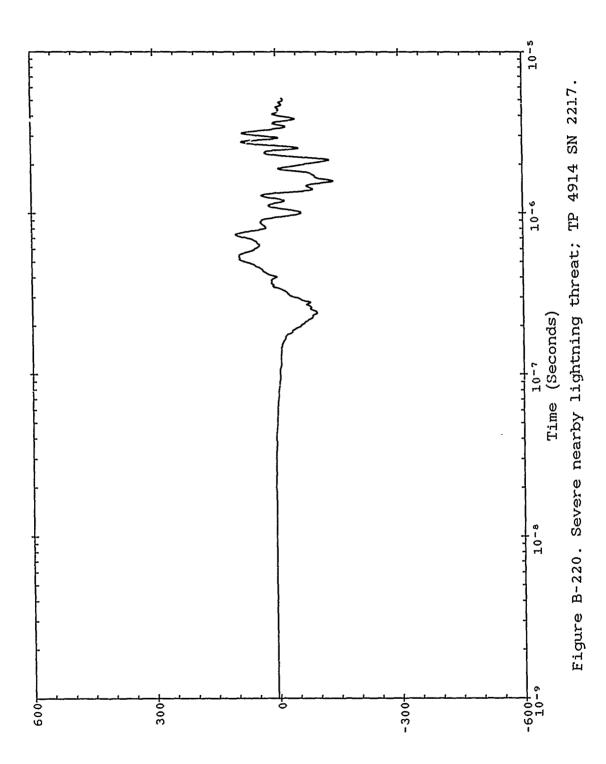






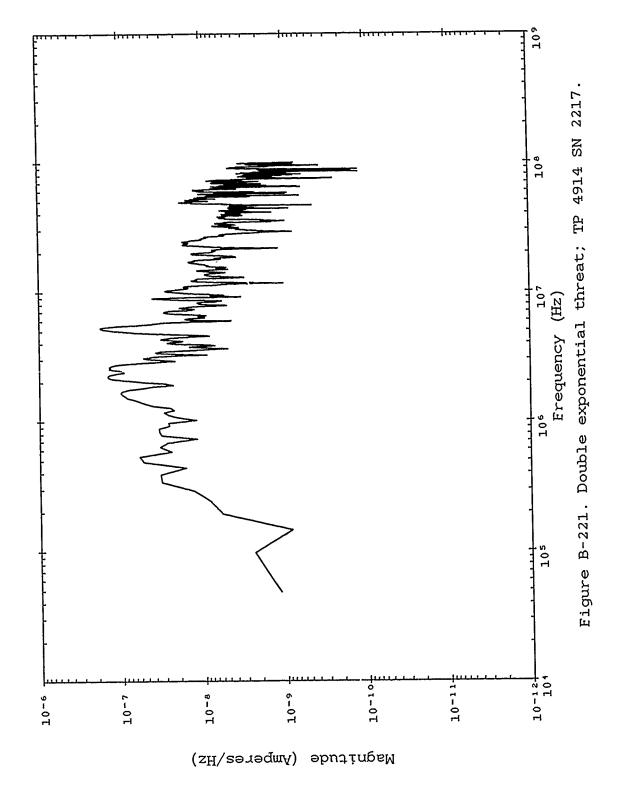


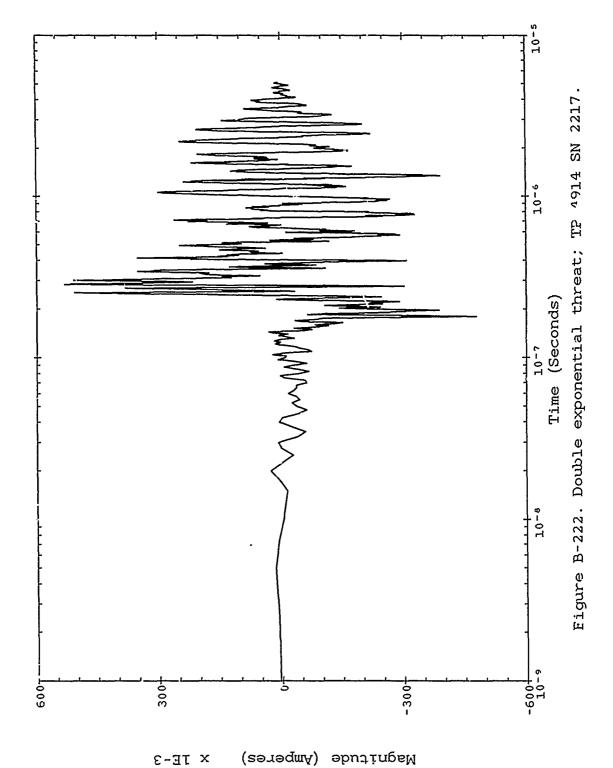


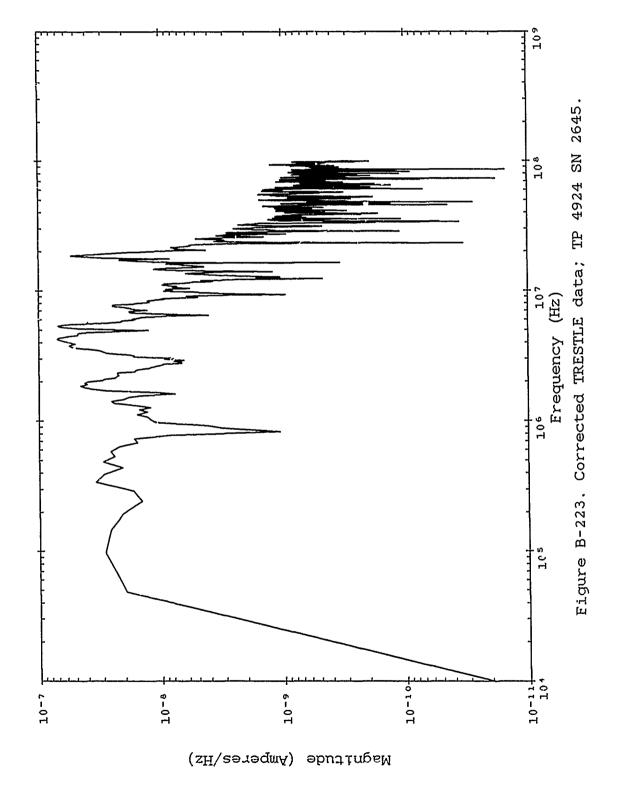


Magnitude (Amperes)

× IE-3



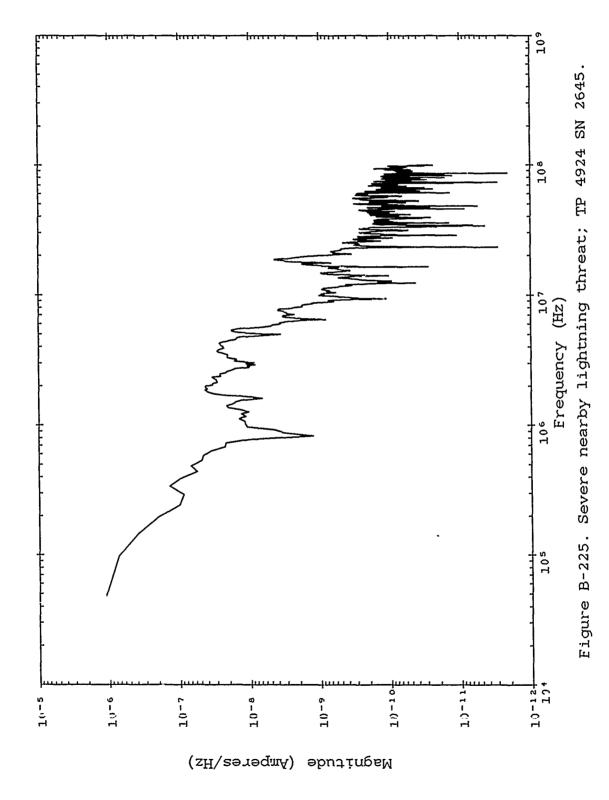




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Magnitude (Amperes)

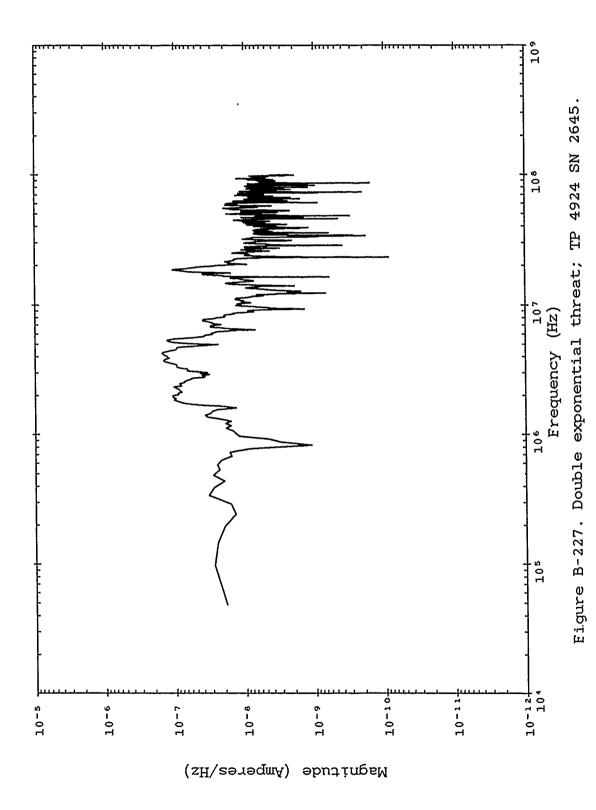
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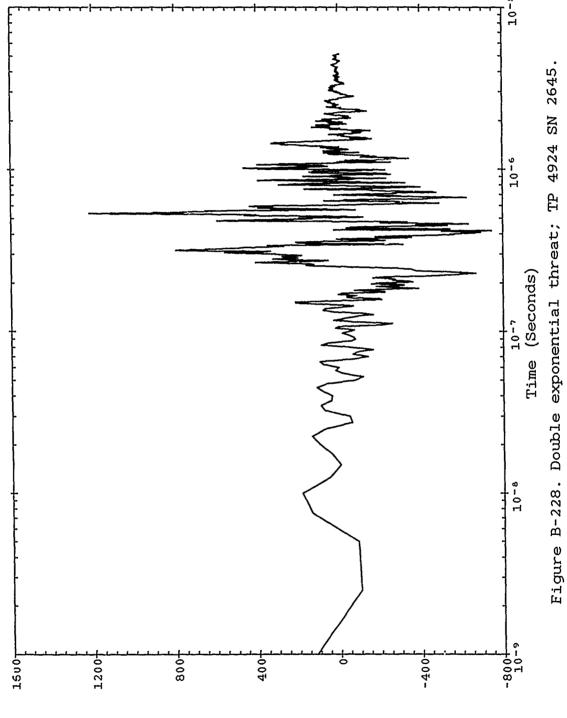


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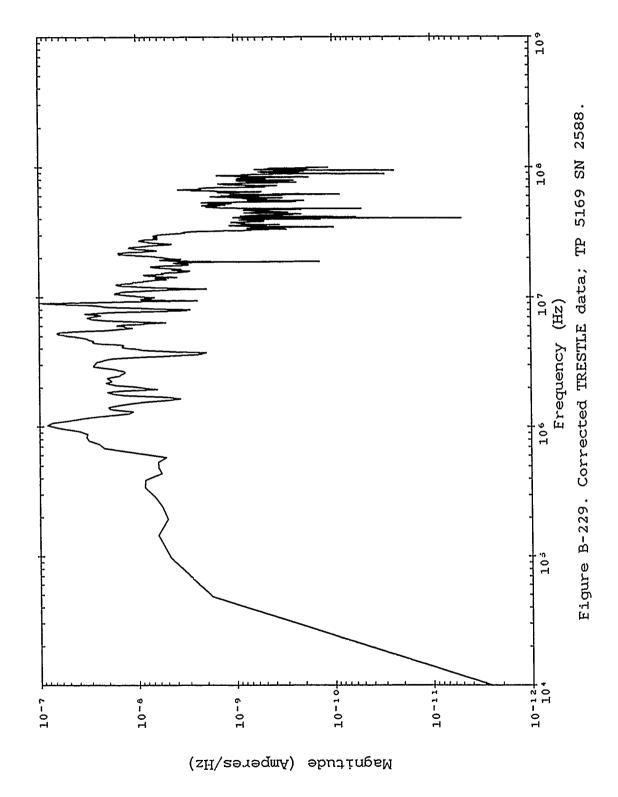
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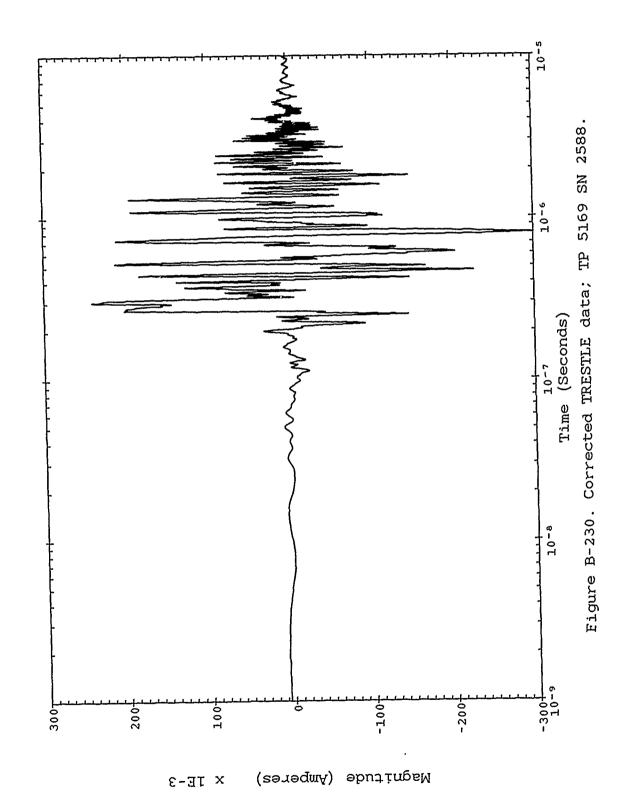
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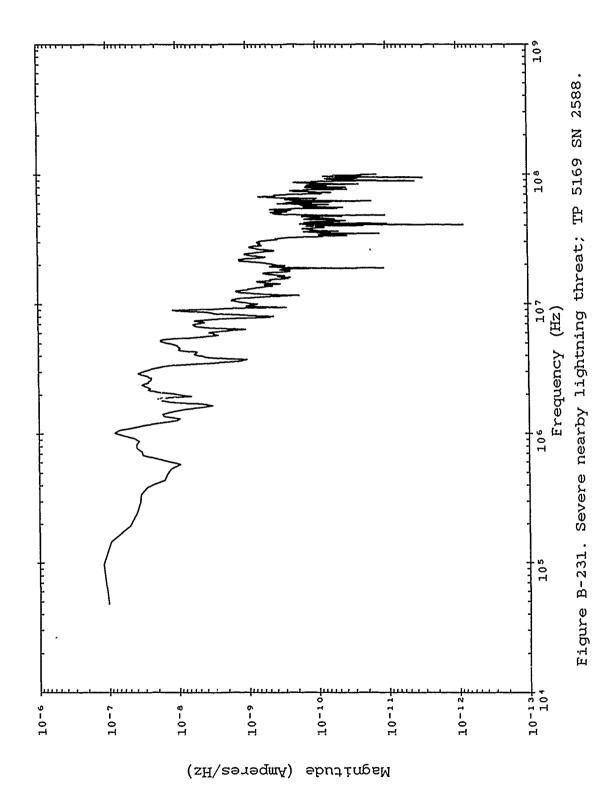


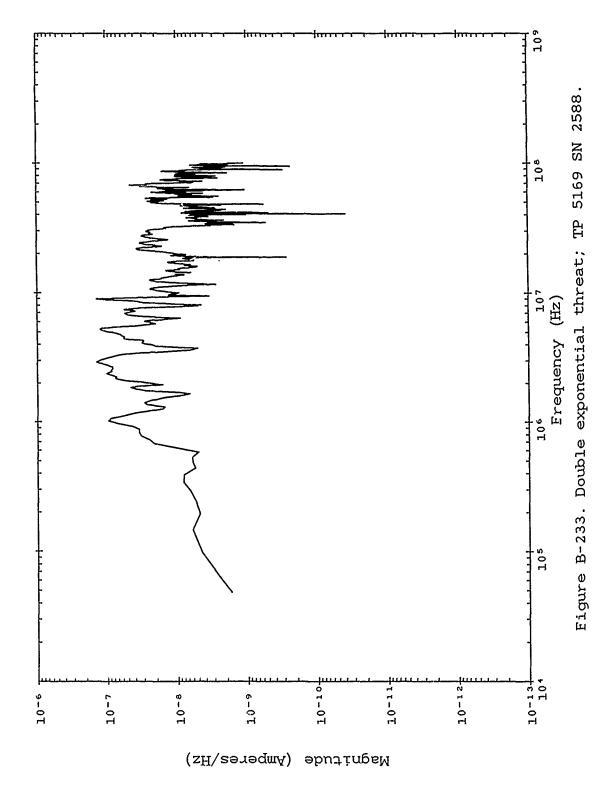


Magnitude (Amperes) x 1E-3

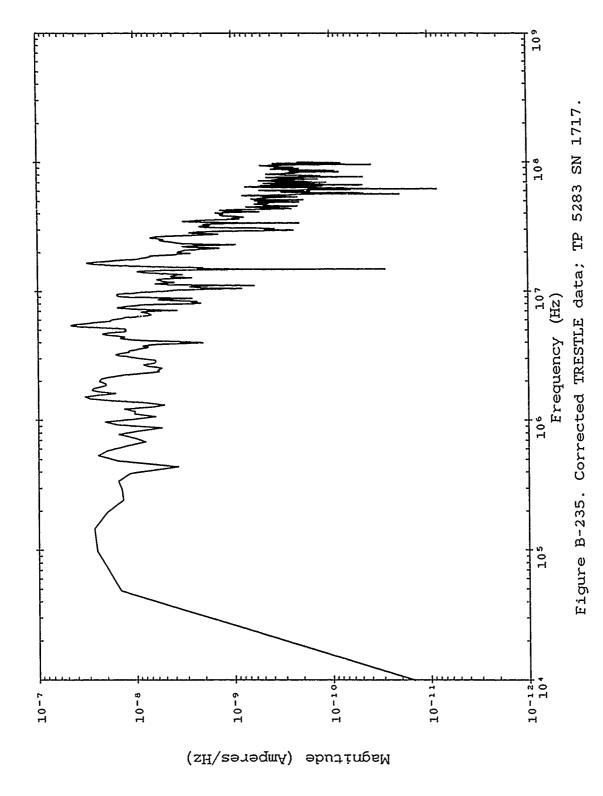


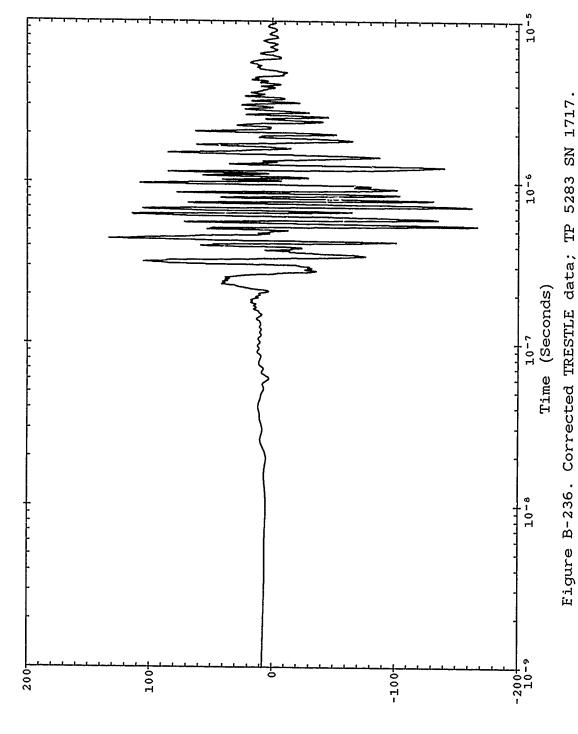




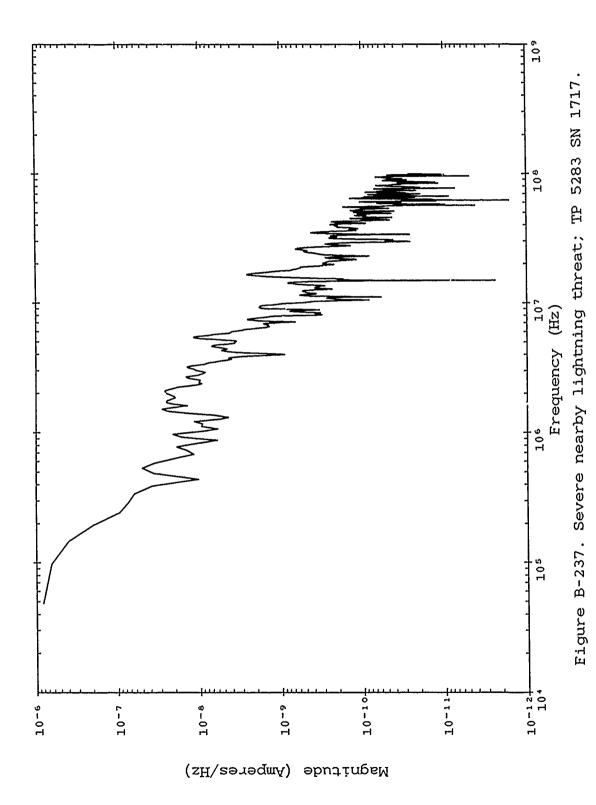


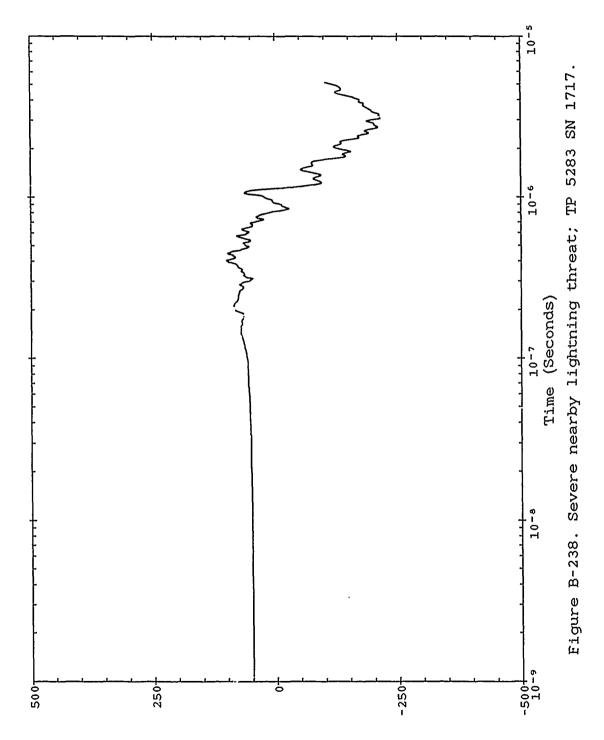
Magnitude (Amperes)





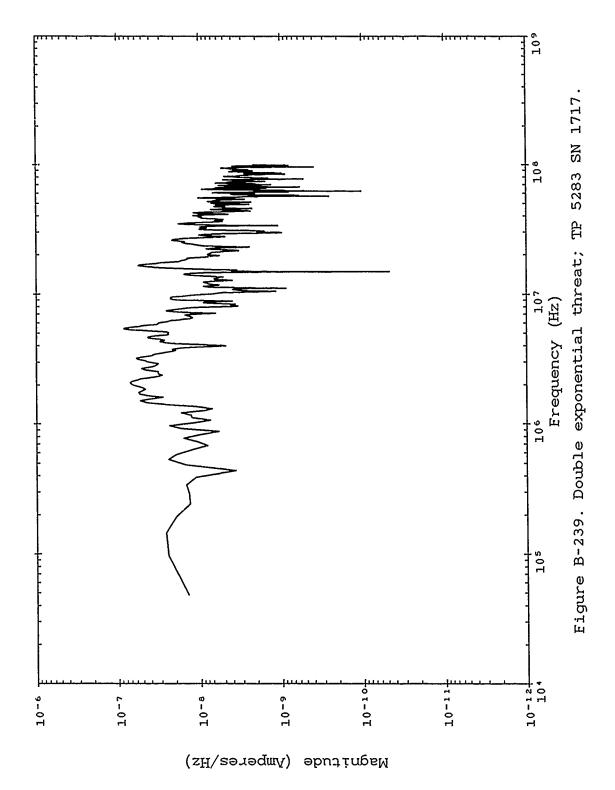
Wagnitude (Amperes) \times 1E-3

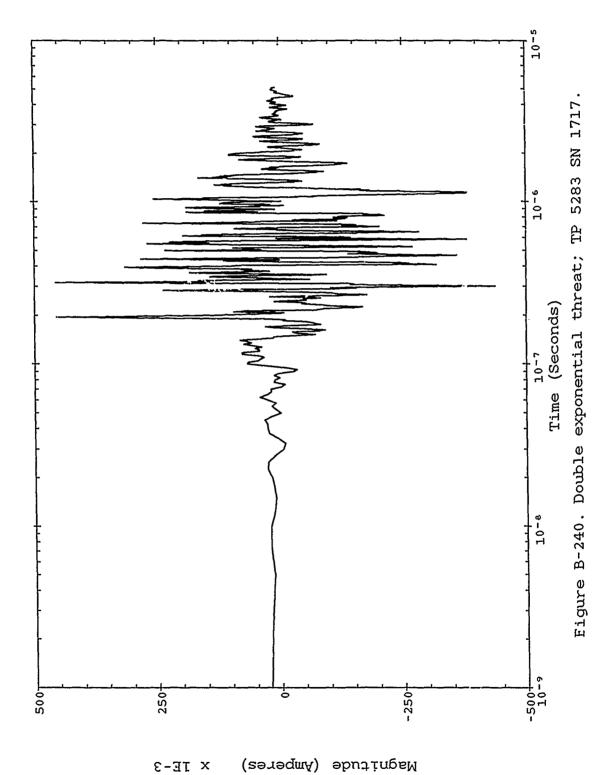


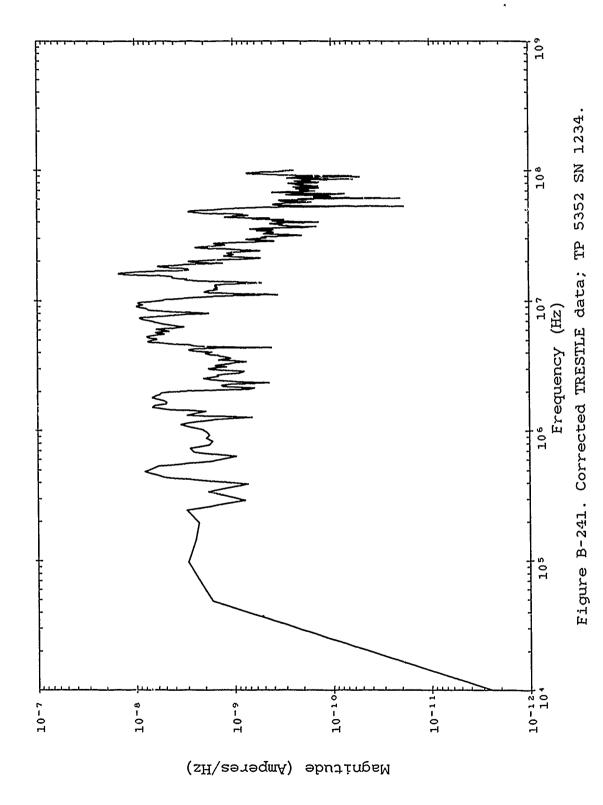


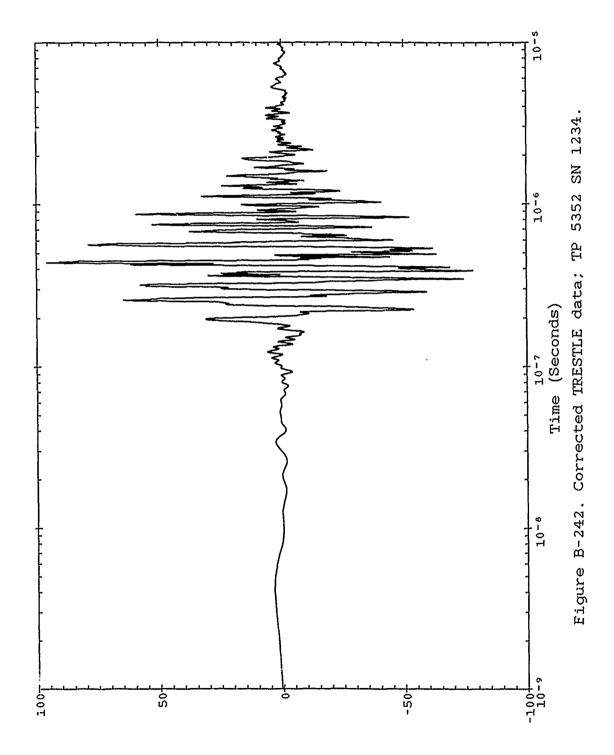
Magnitude (Amperes)

× JE-3





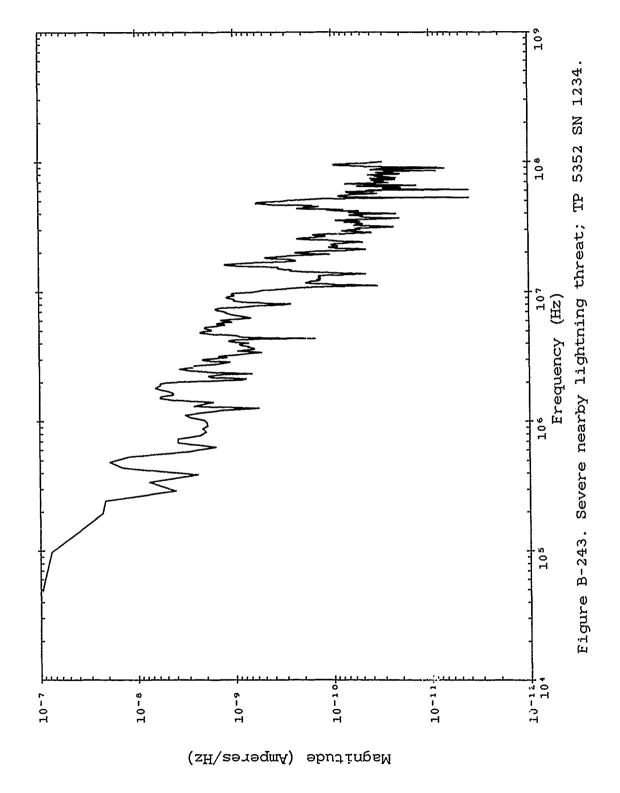


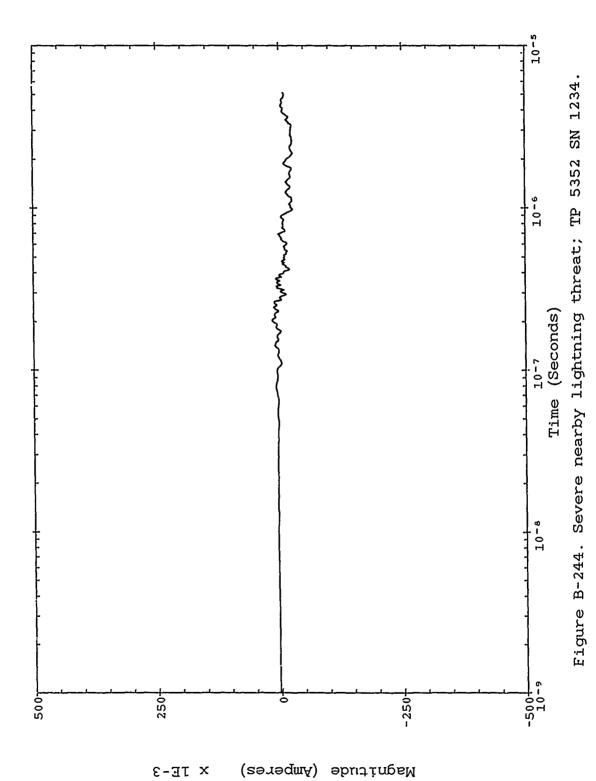


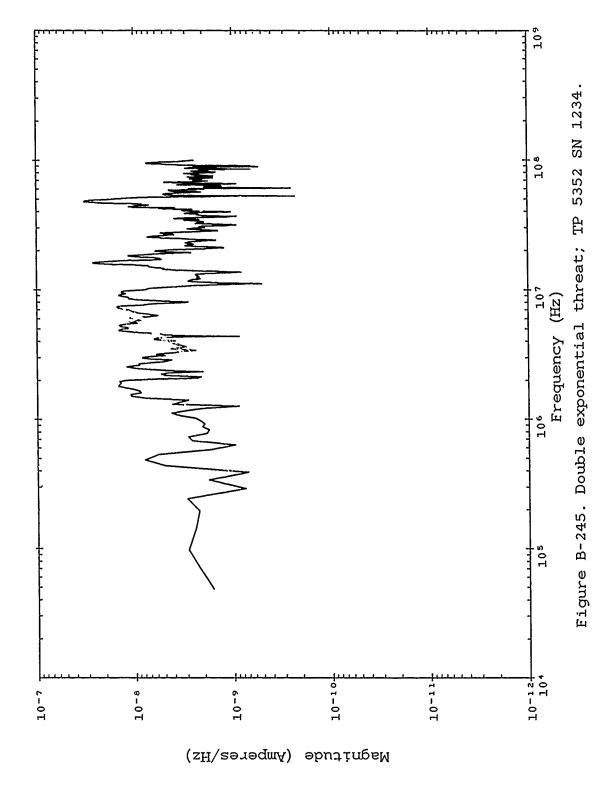
273

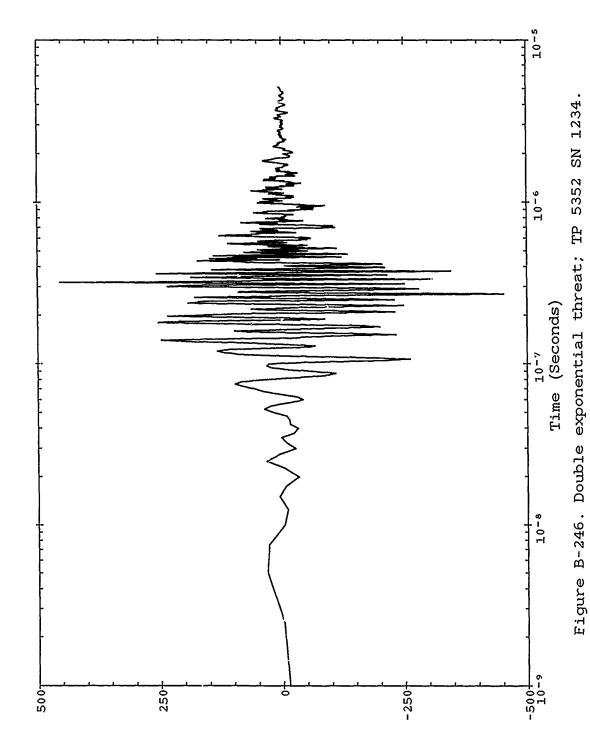
Magnitude (Amperes)

x IE-3

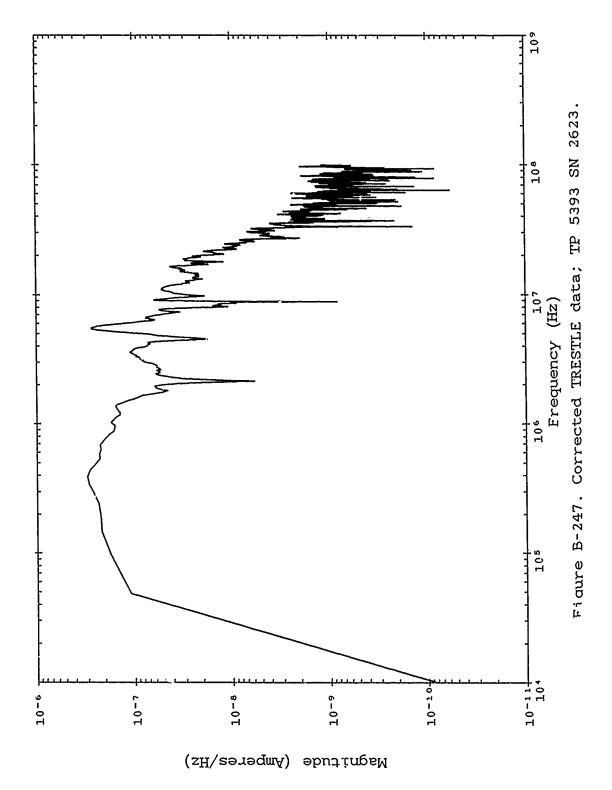


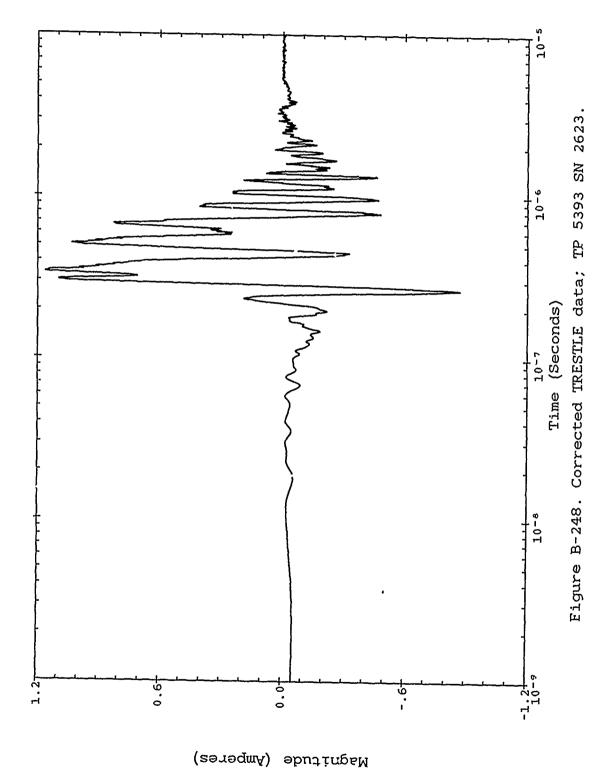


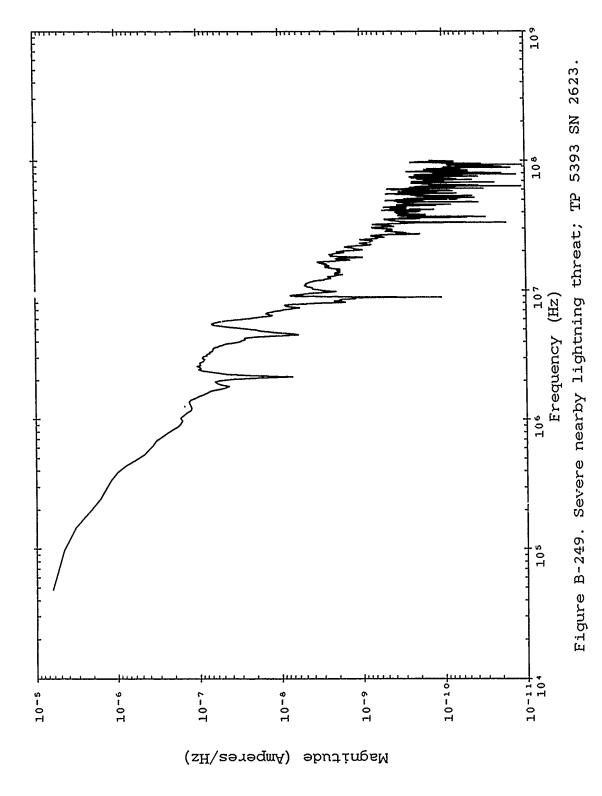


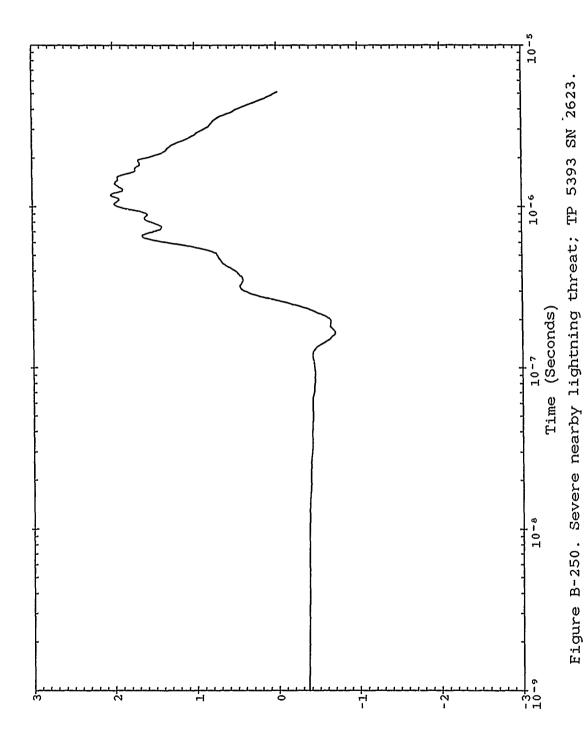


Magnitude (Amperes) x 1E-3



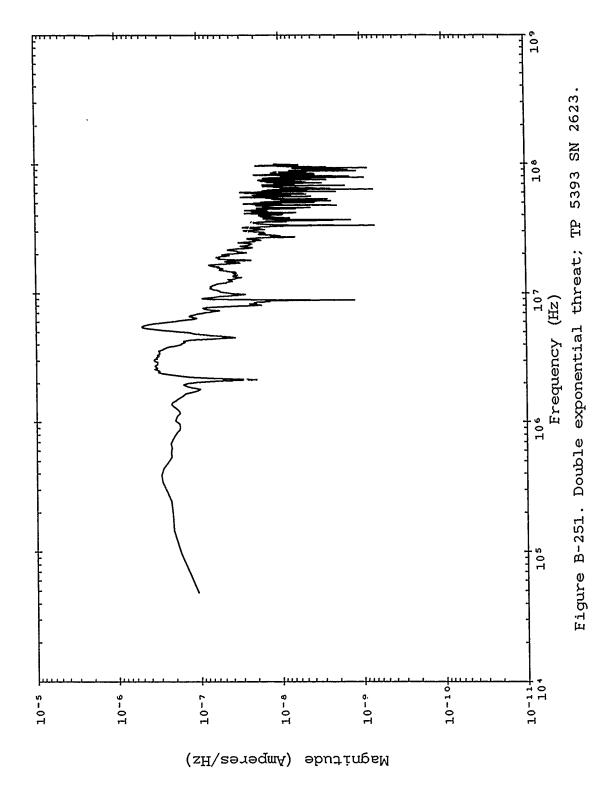


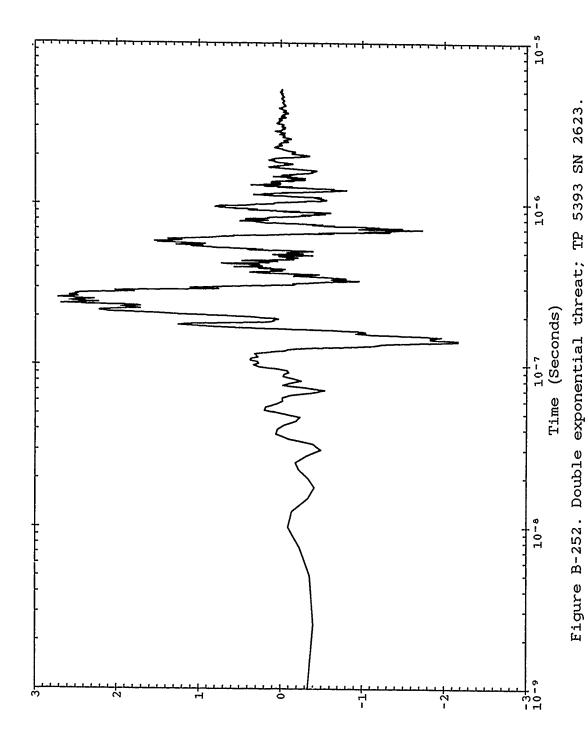




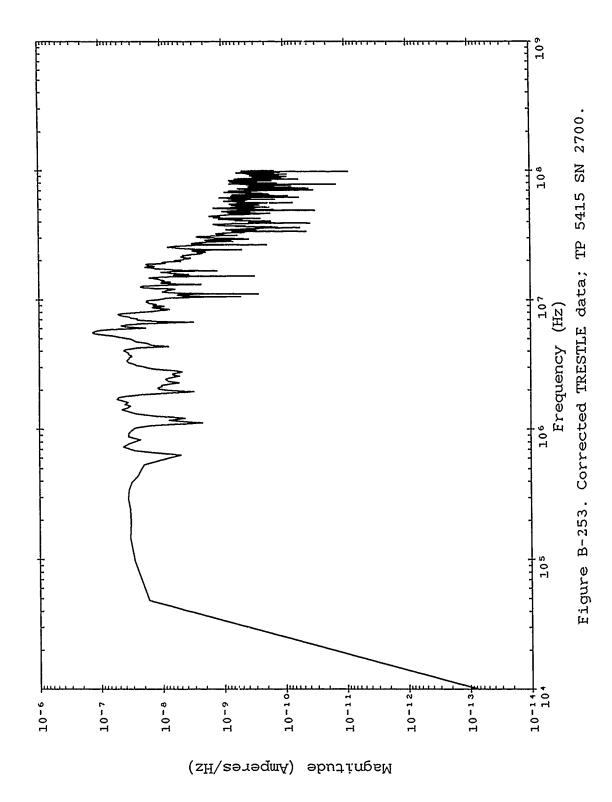
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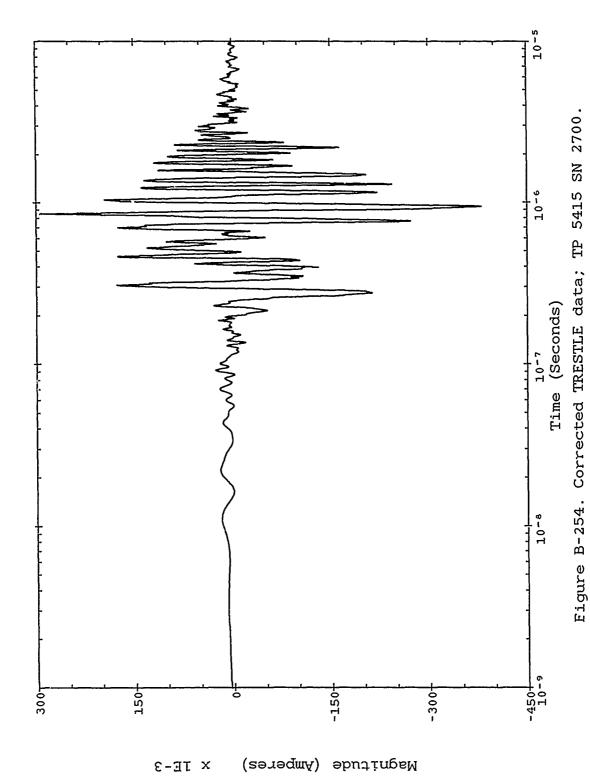
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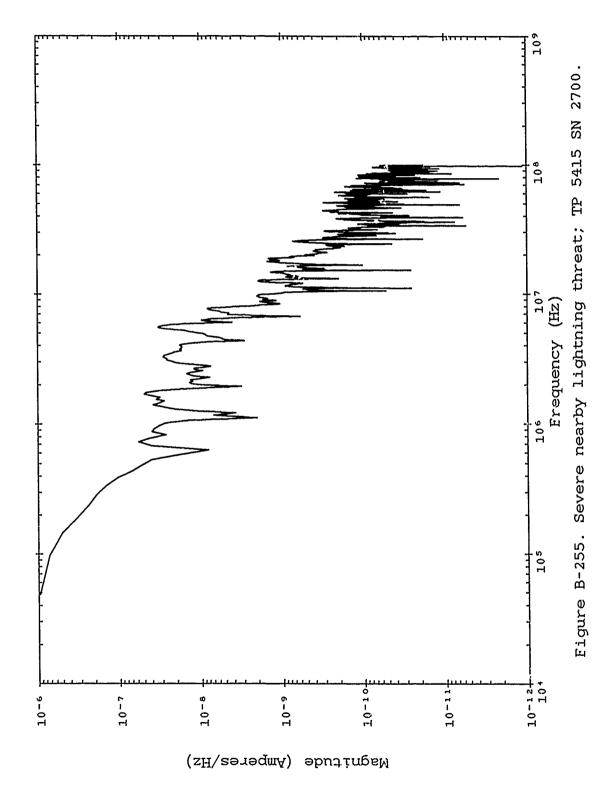


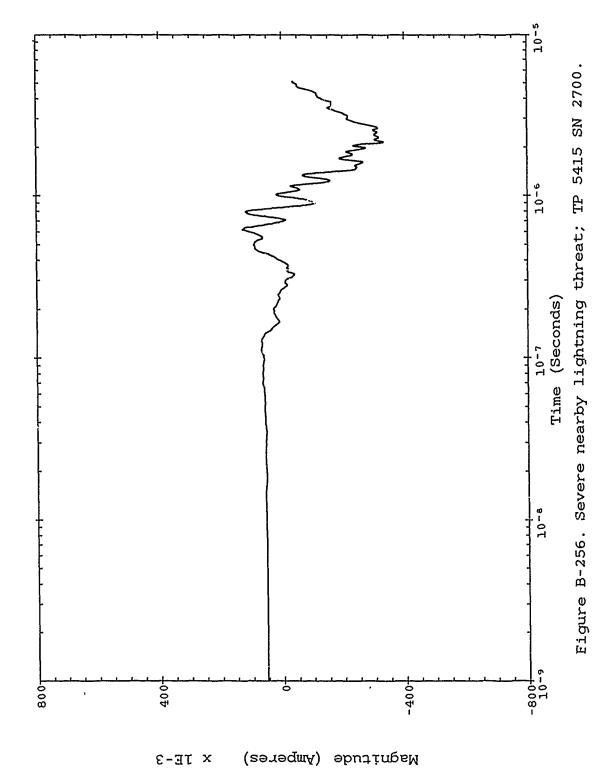


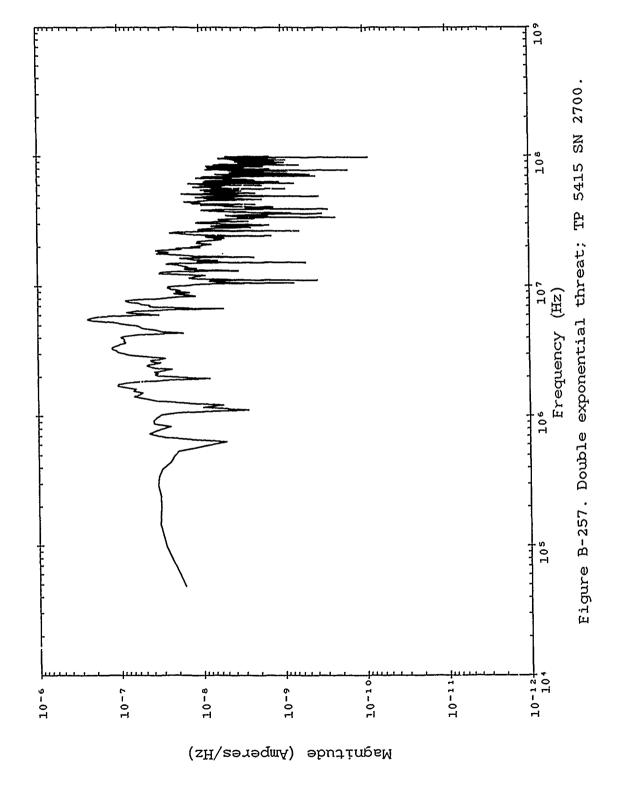
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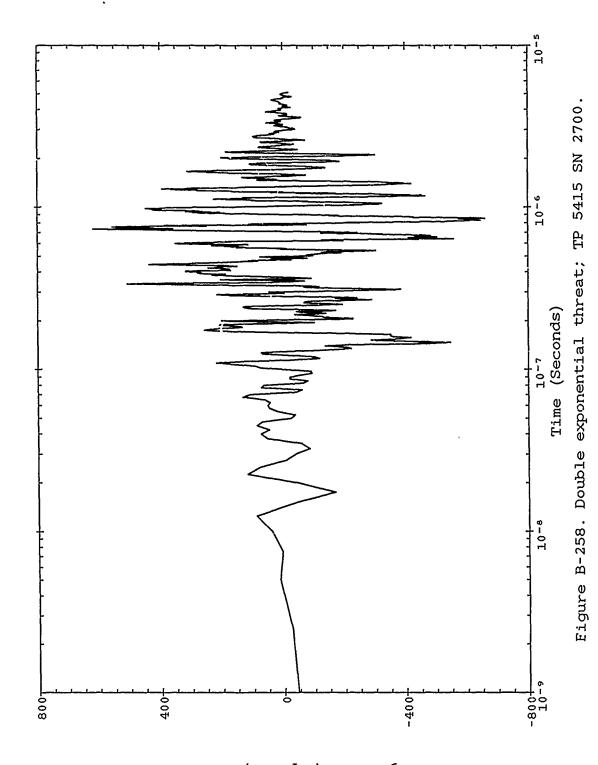




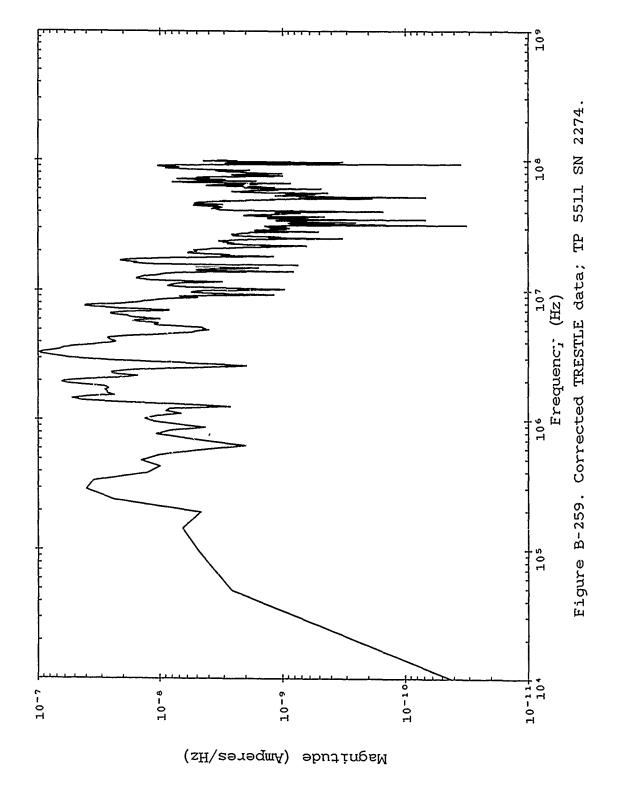


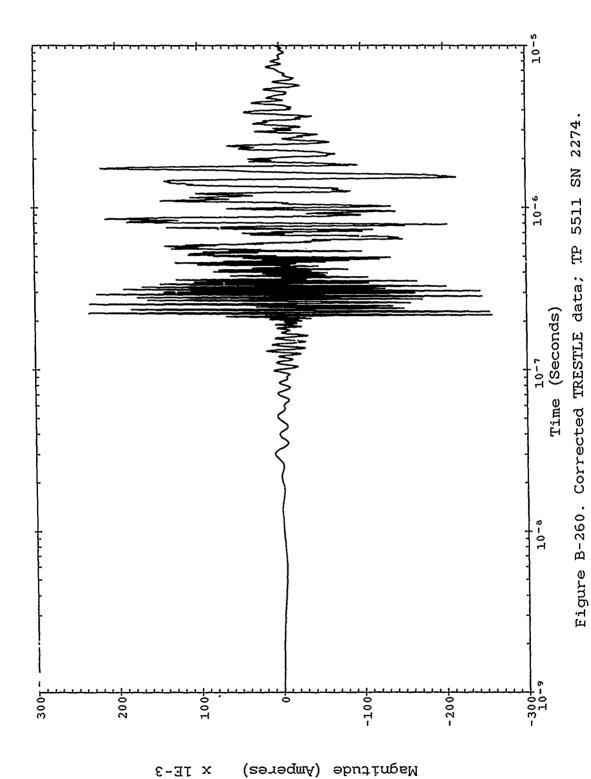


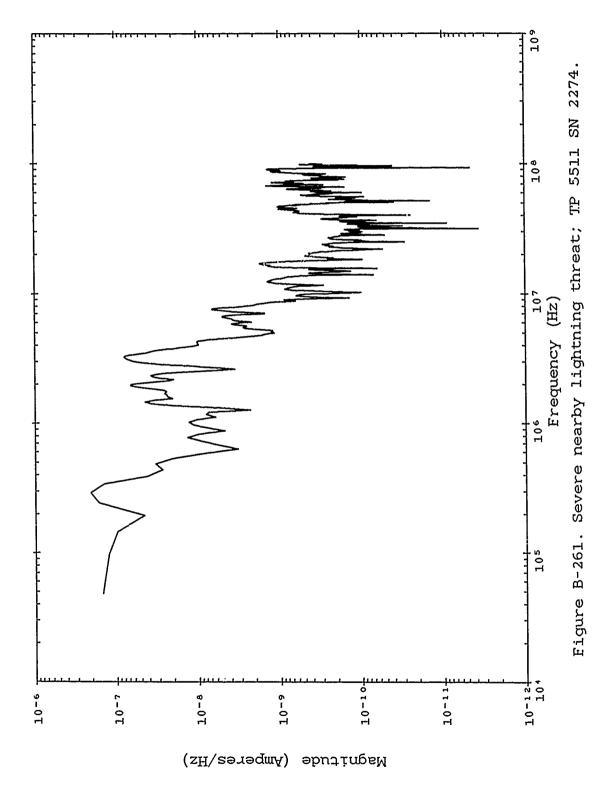


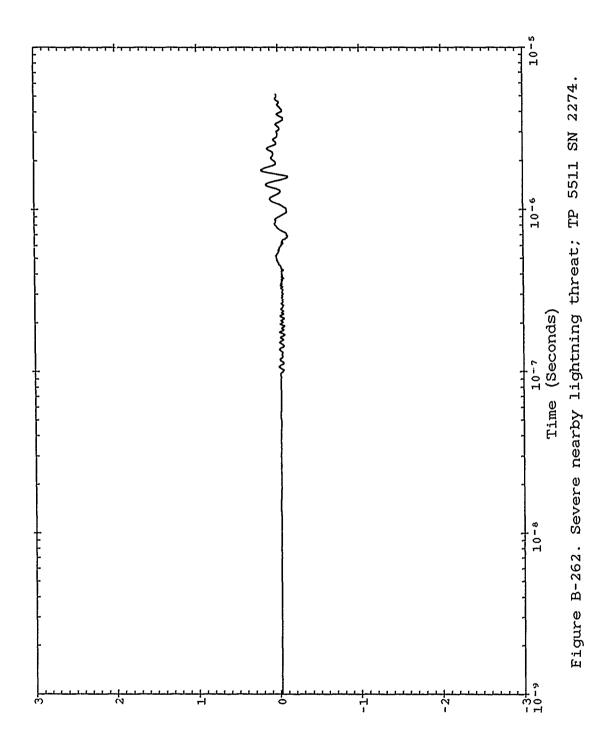


Magnitude (Amperes) x lE-3



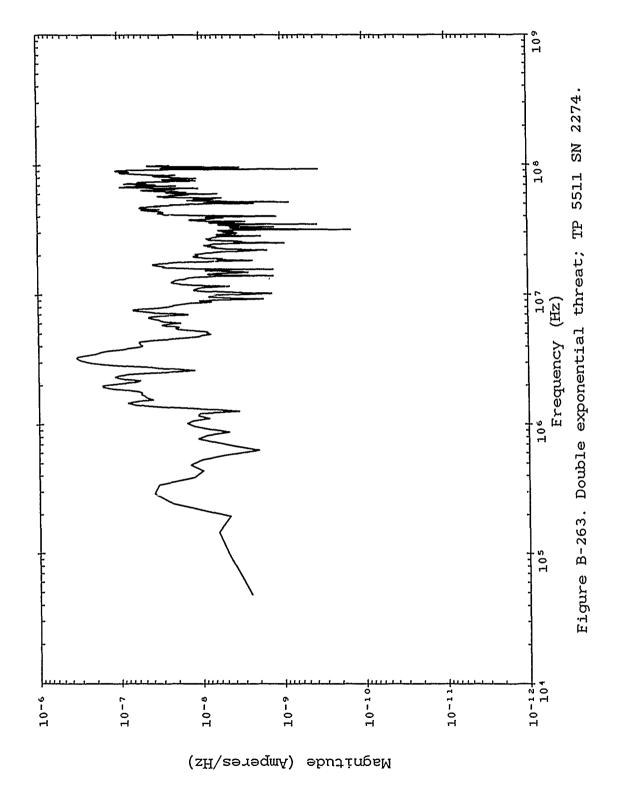


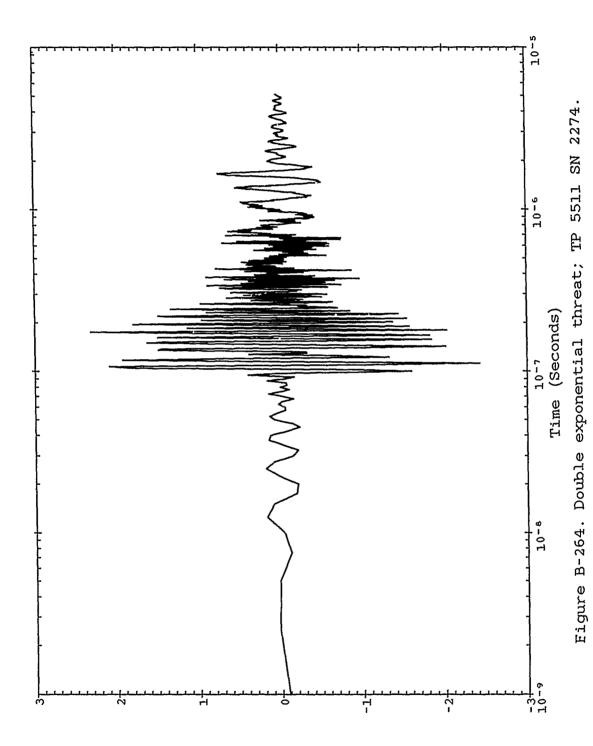




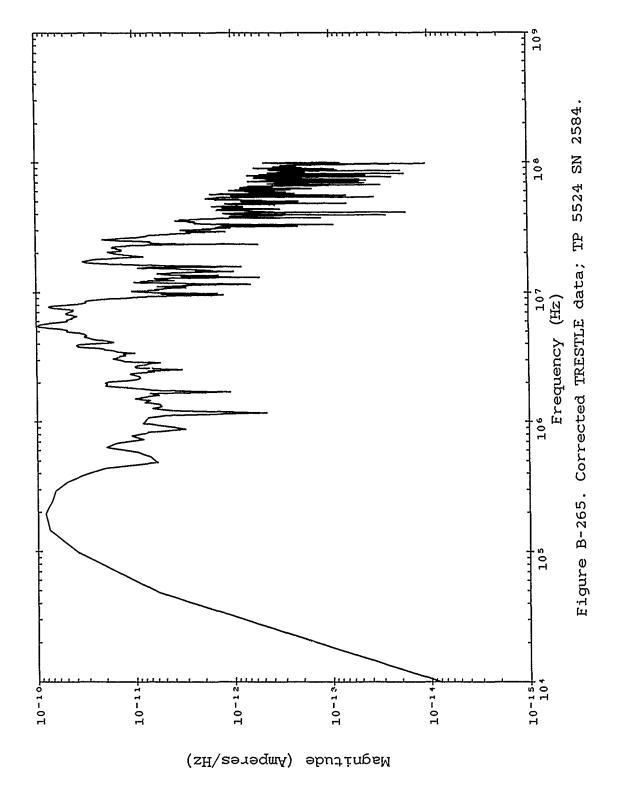
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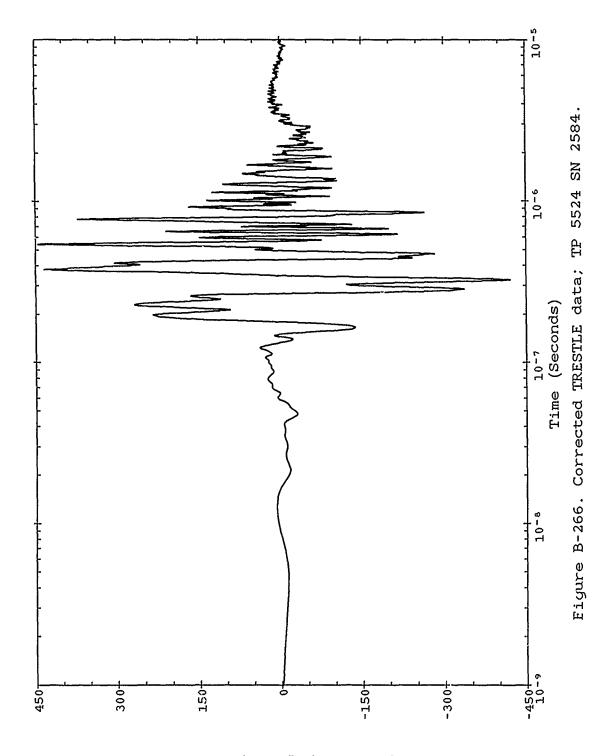
Magnitude (Amperes)



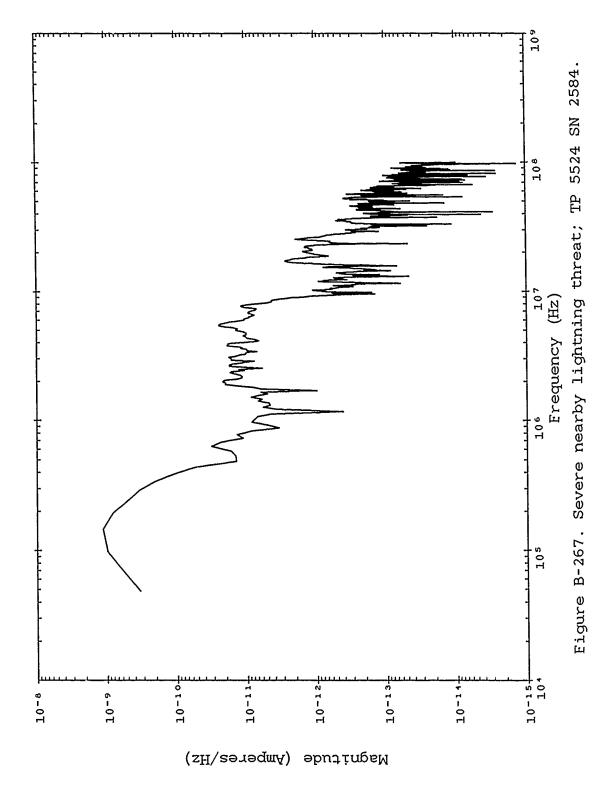


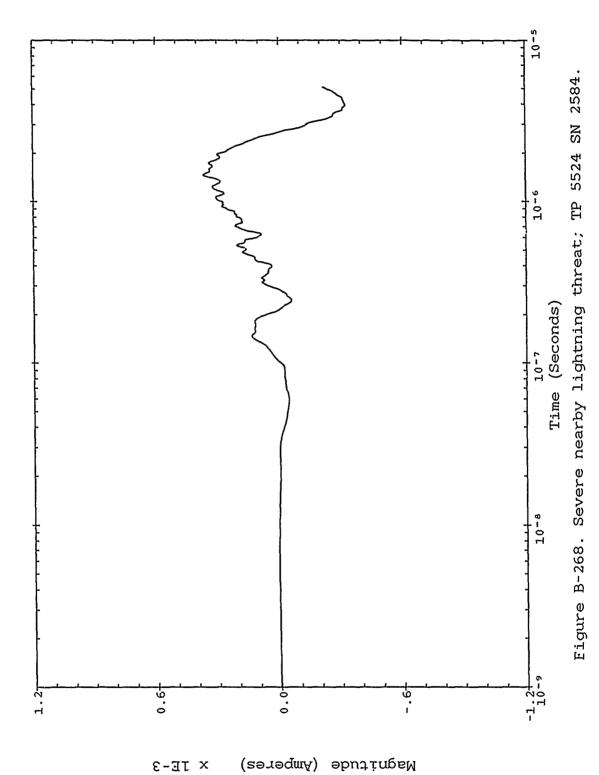
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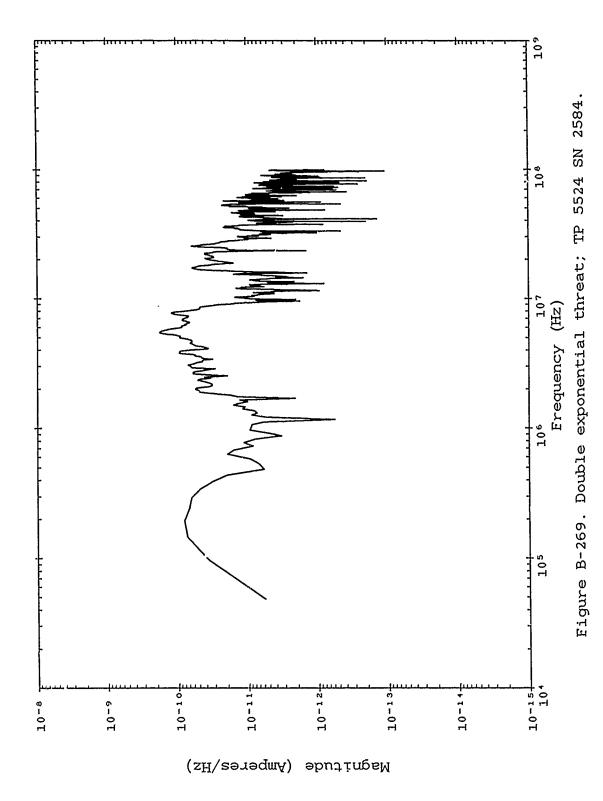


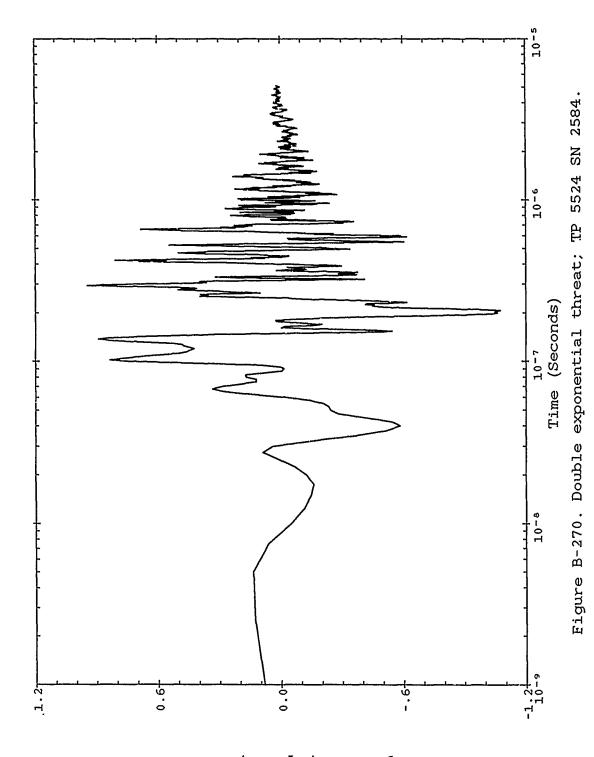


Magnitude (Amperes) x lE-6

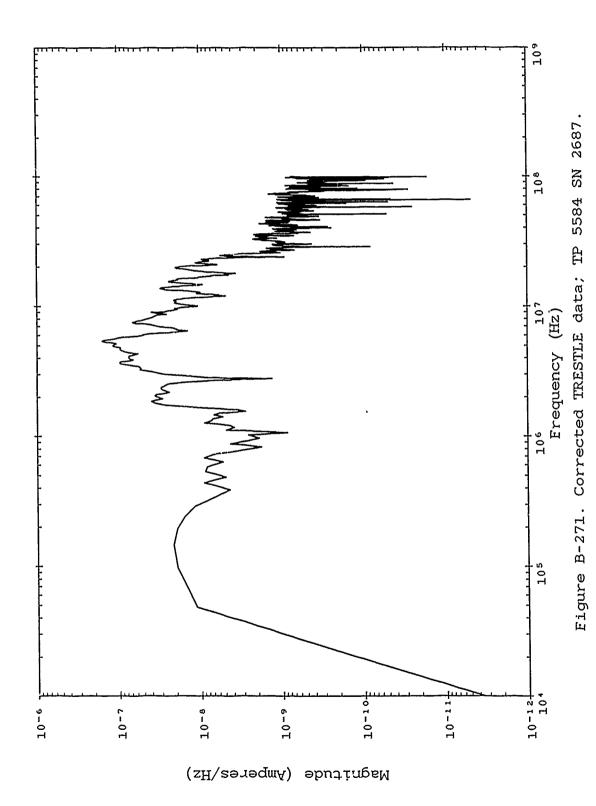


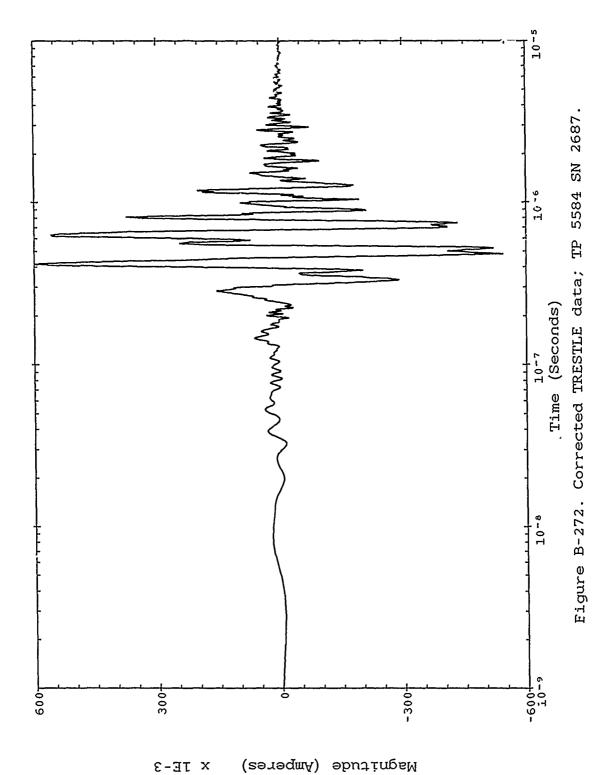


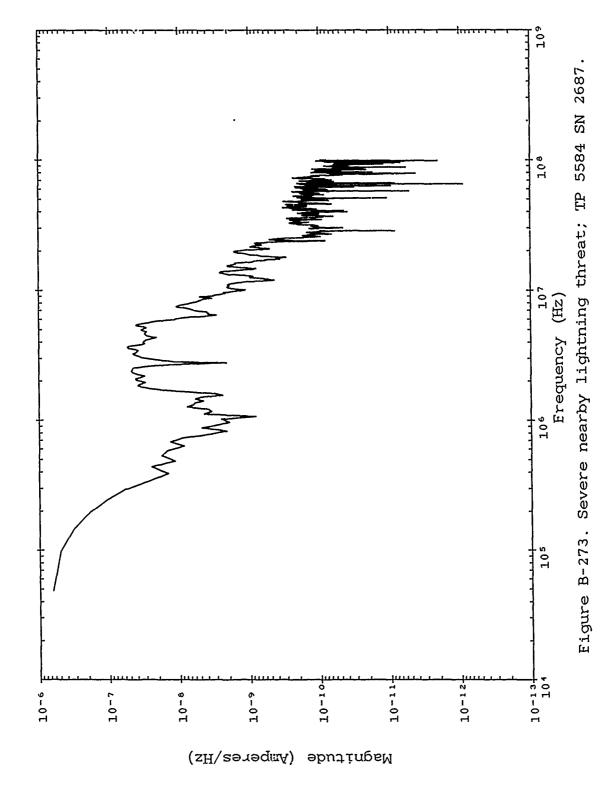


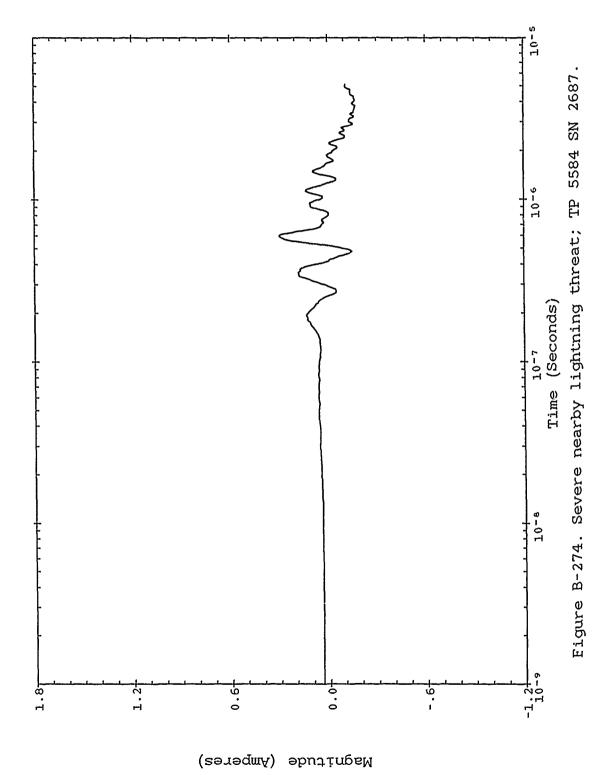


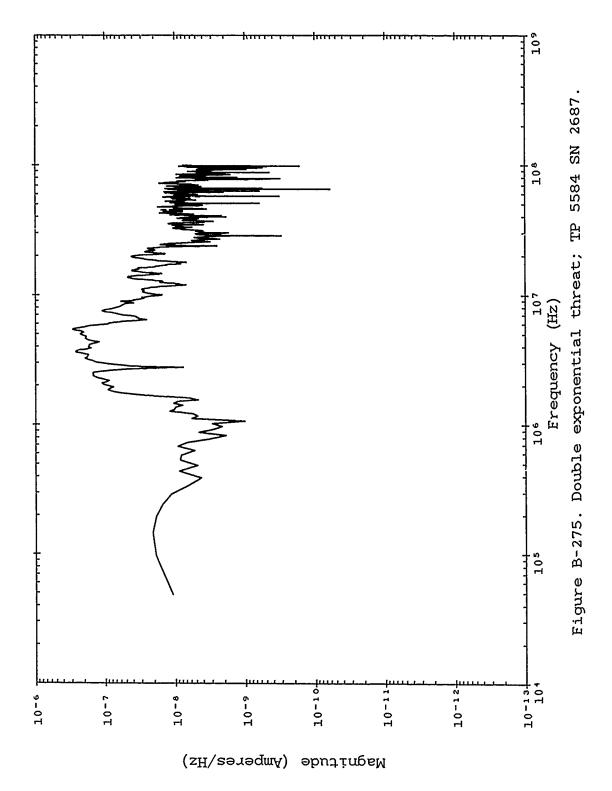
Magnitude (Amperes) \times 1E-3

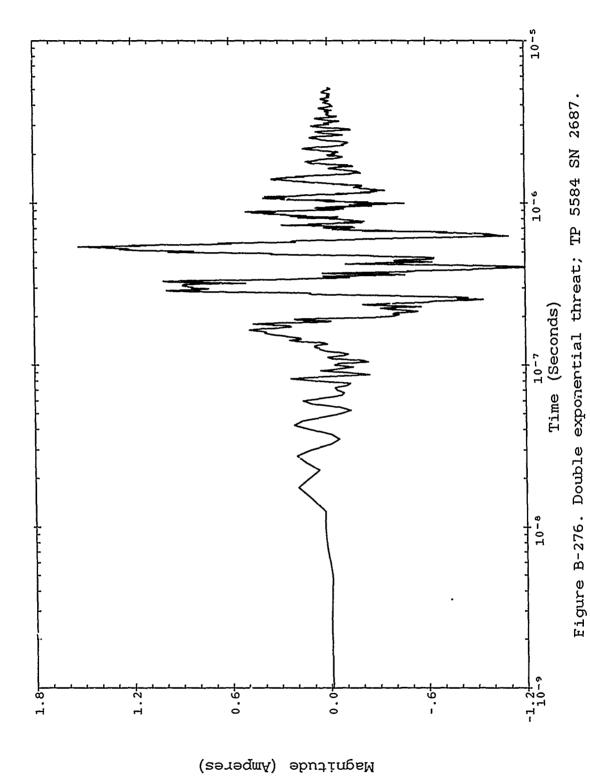


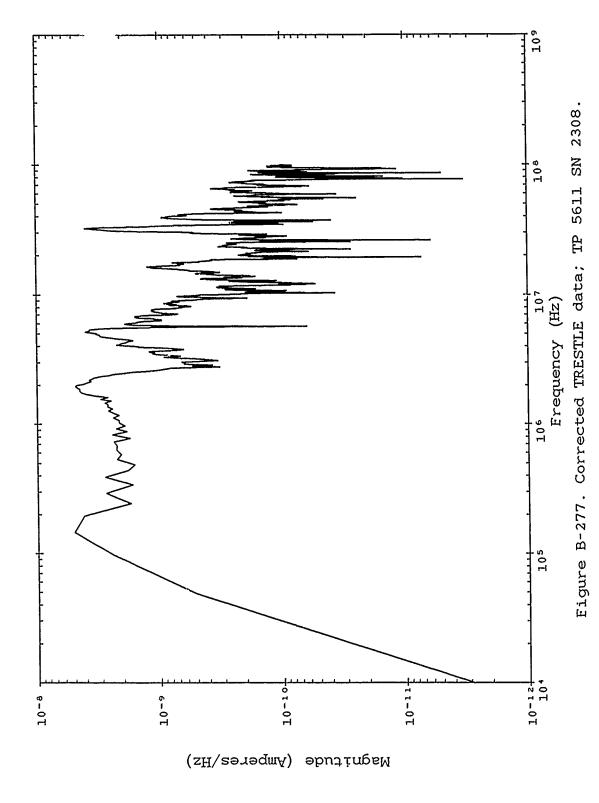


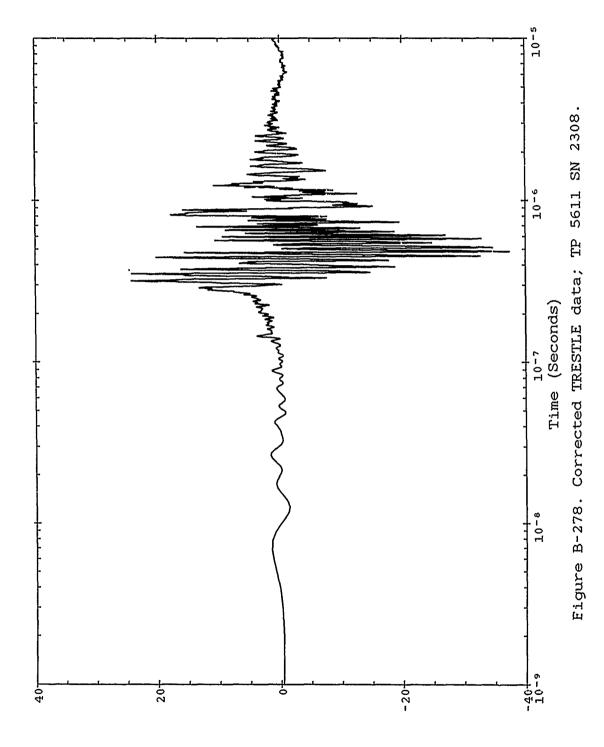






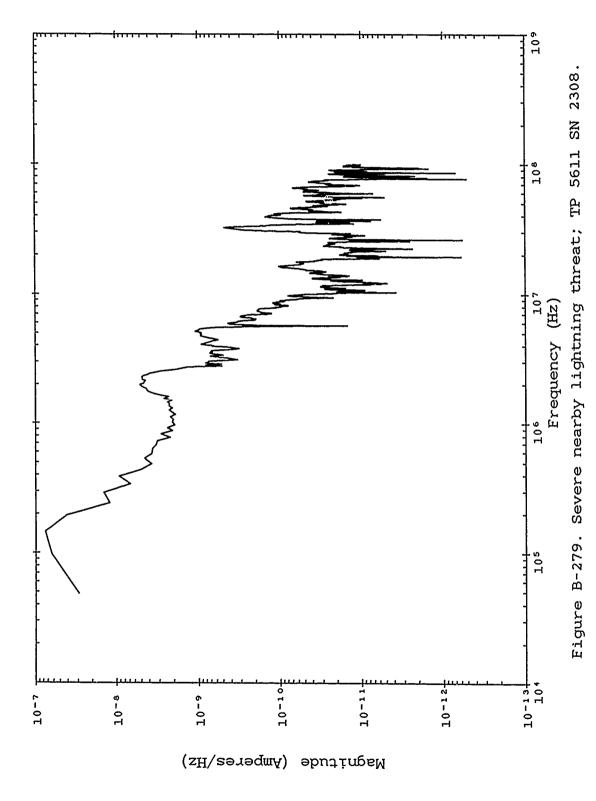


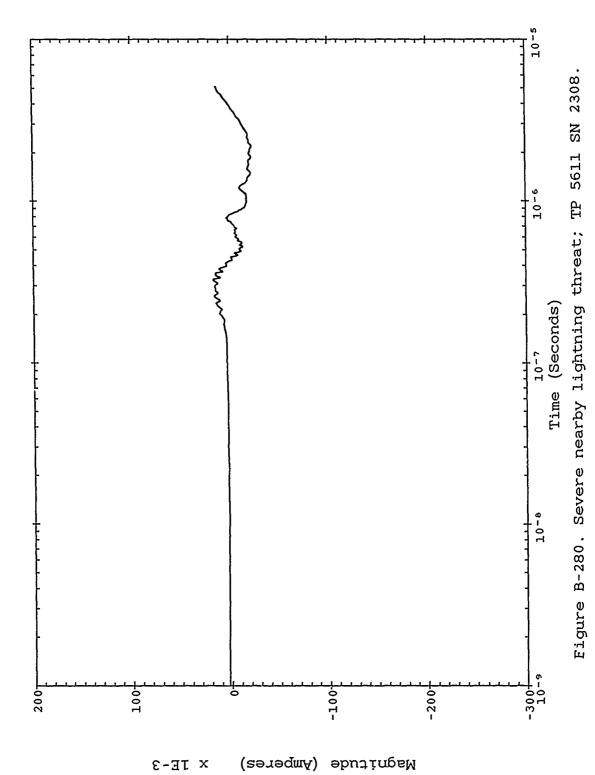


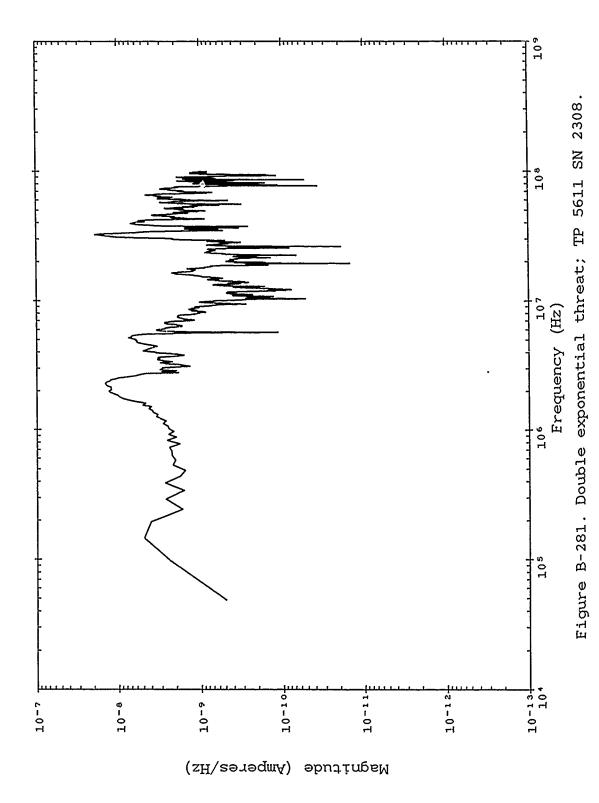


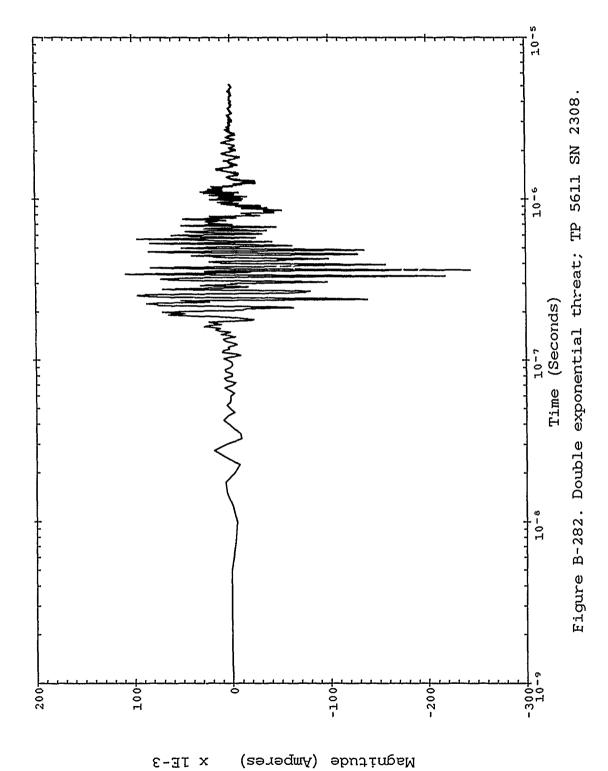
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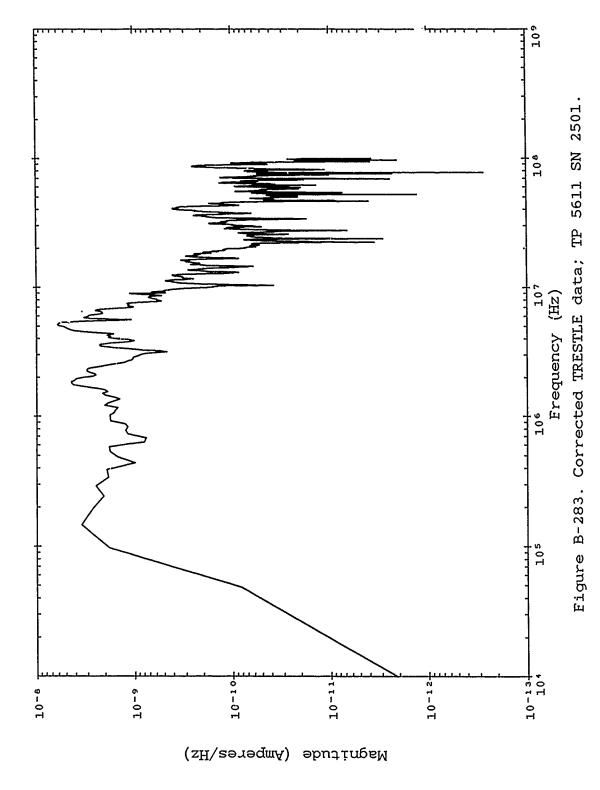
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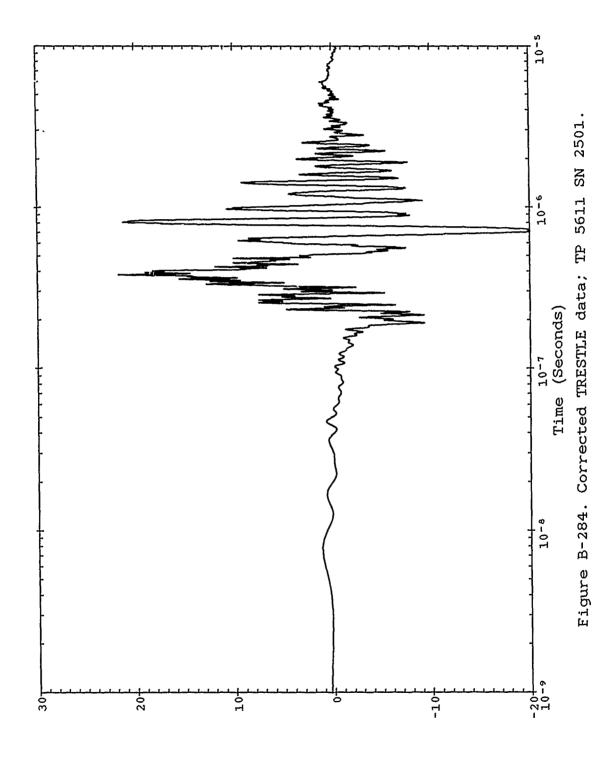




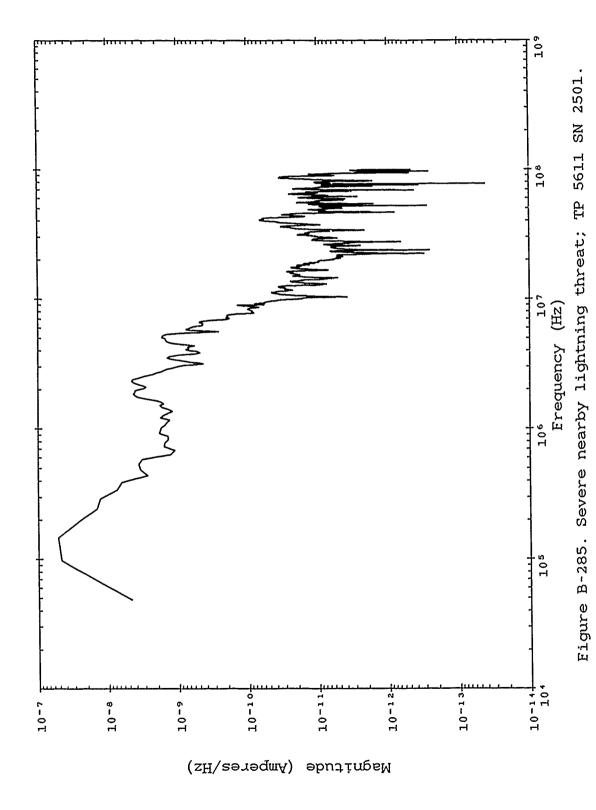


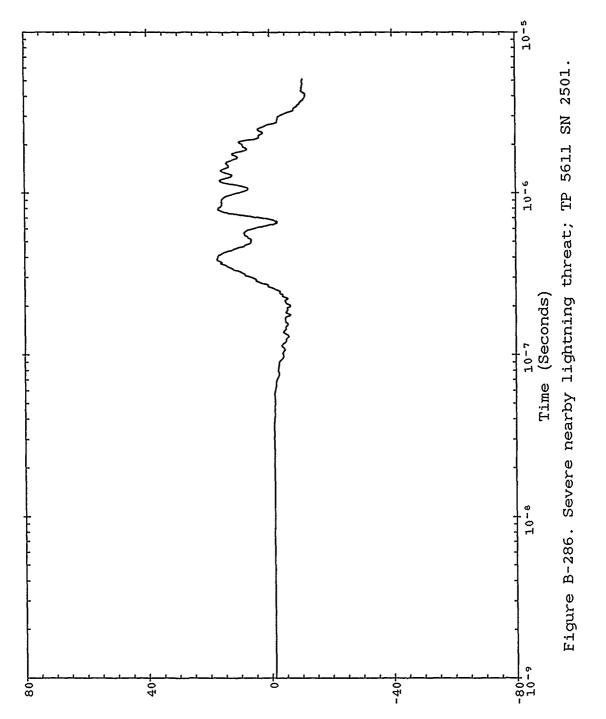






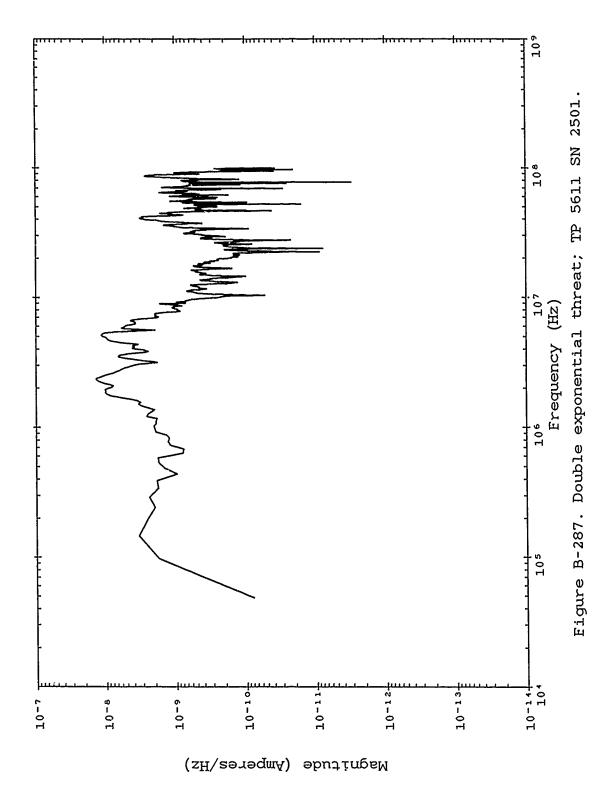
Wagnitude (Amperes) x 1E-3

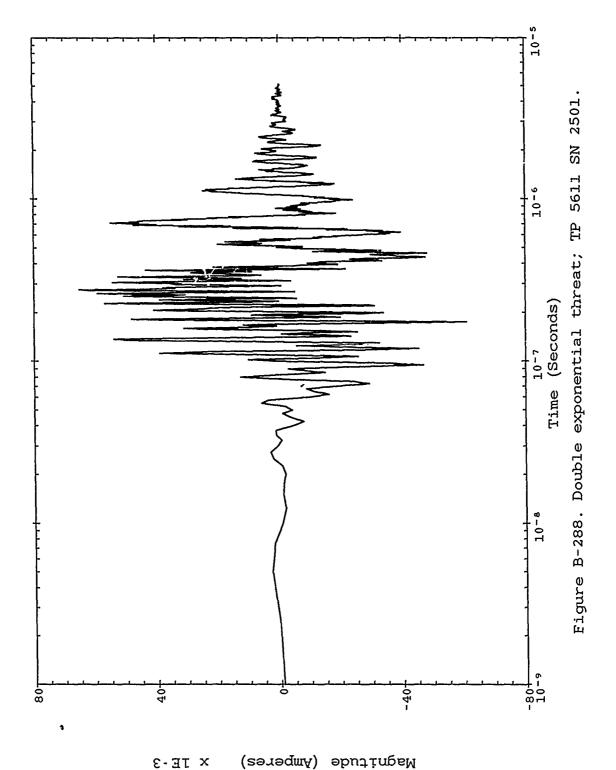


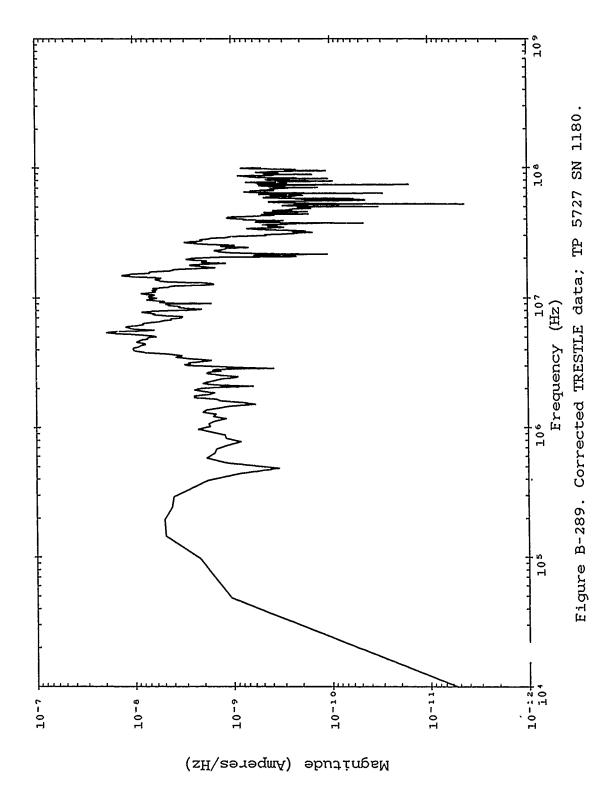


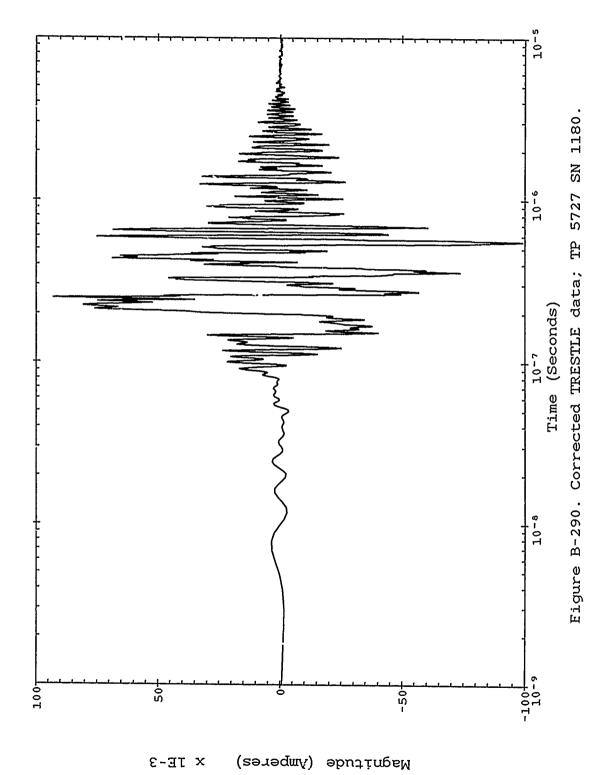
Magnitude (Amperes)

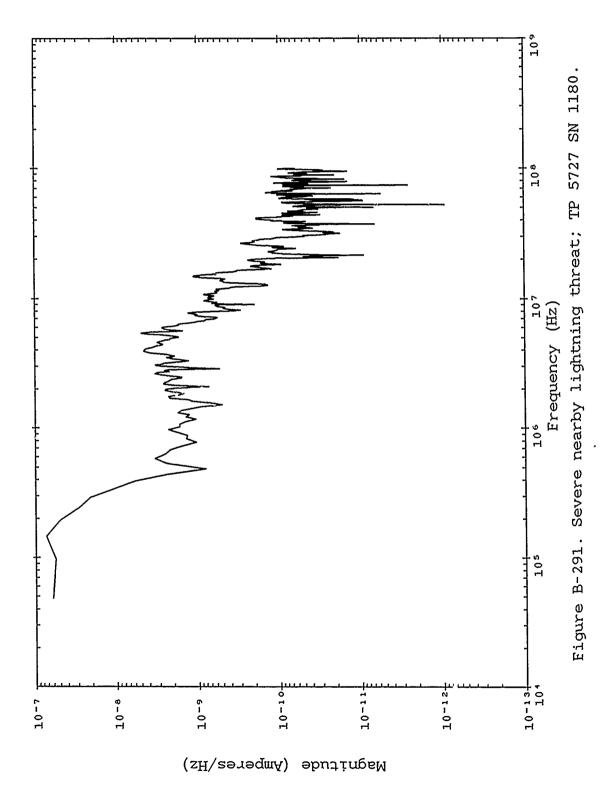
x TE-3

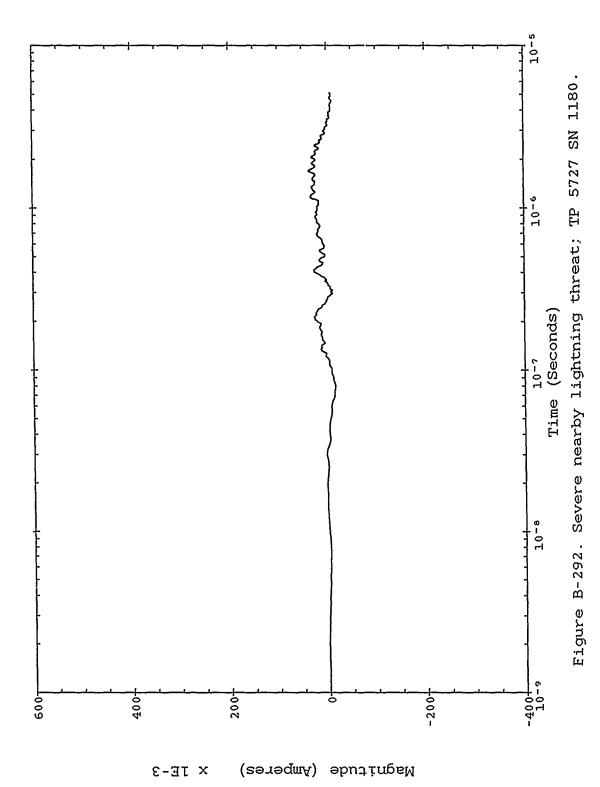


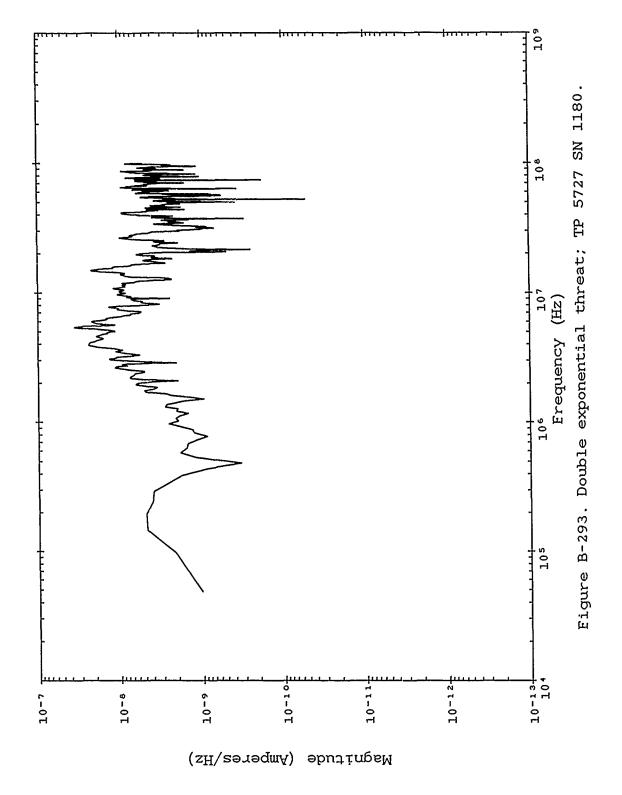


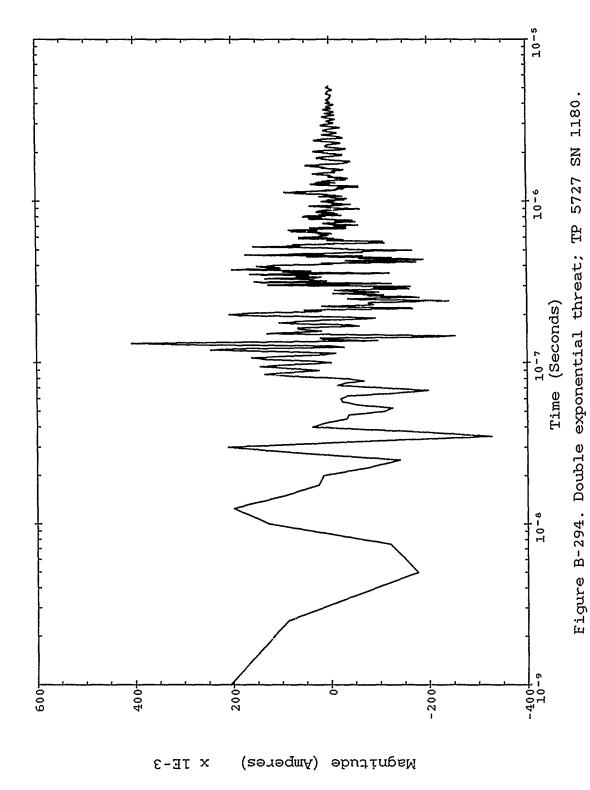


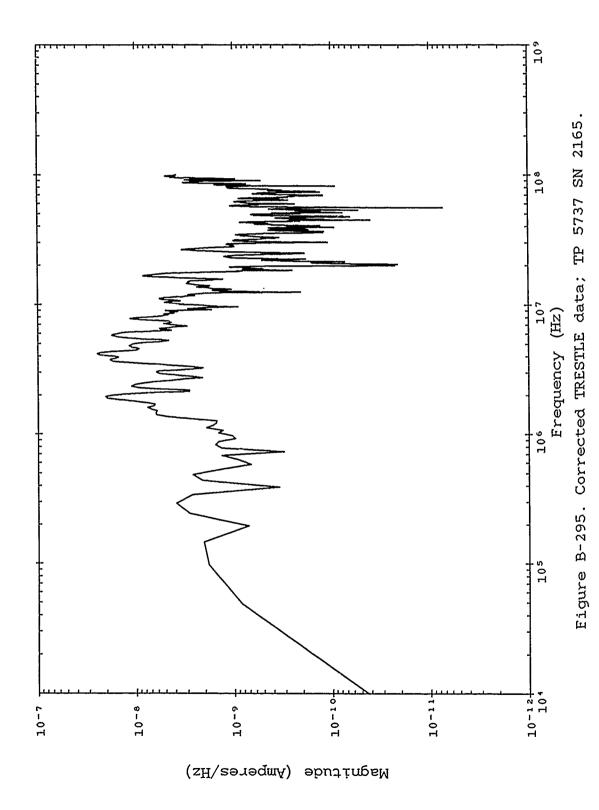


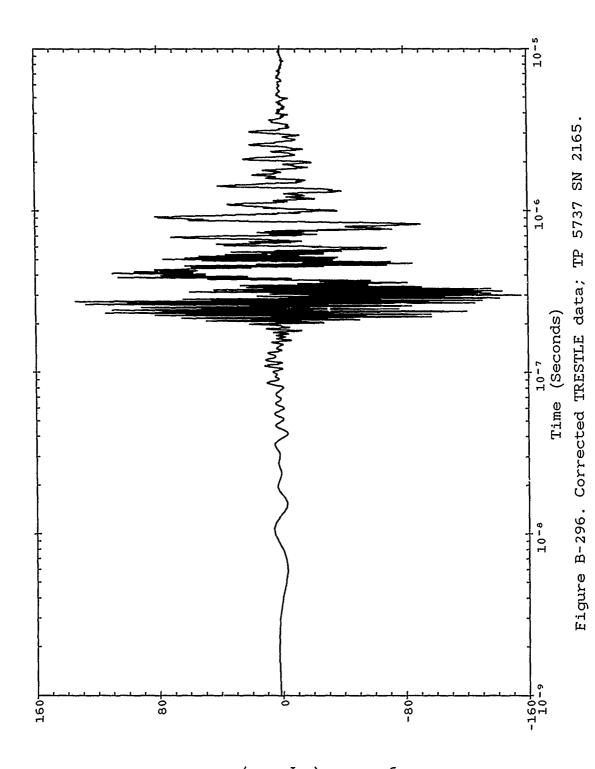




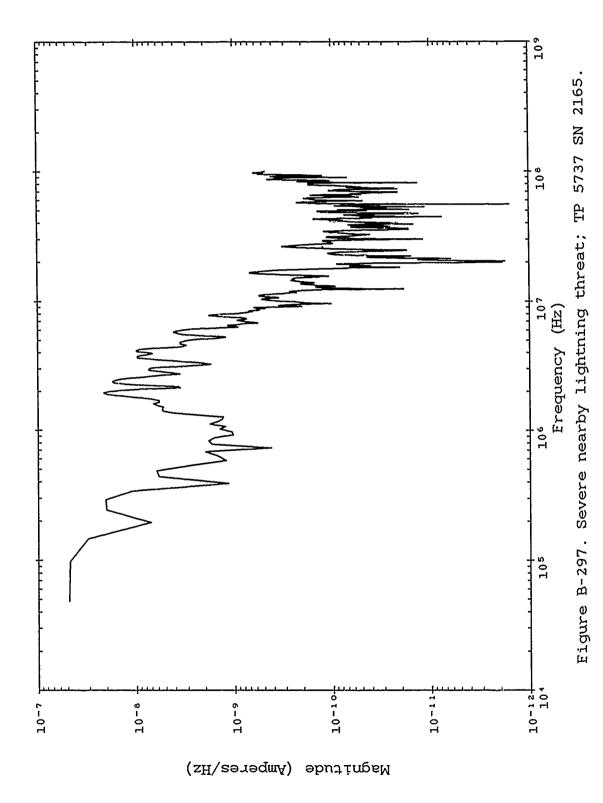


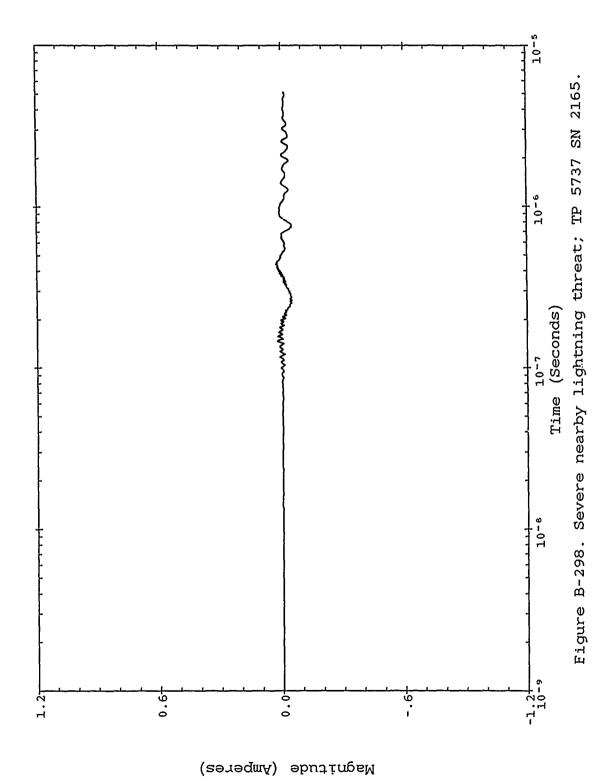


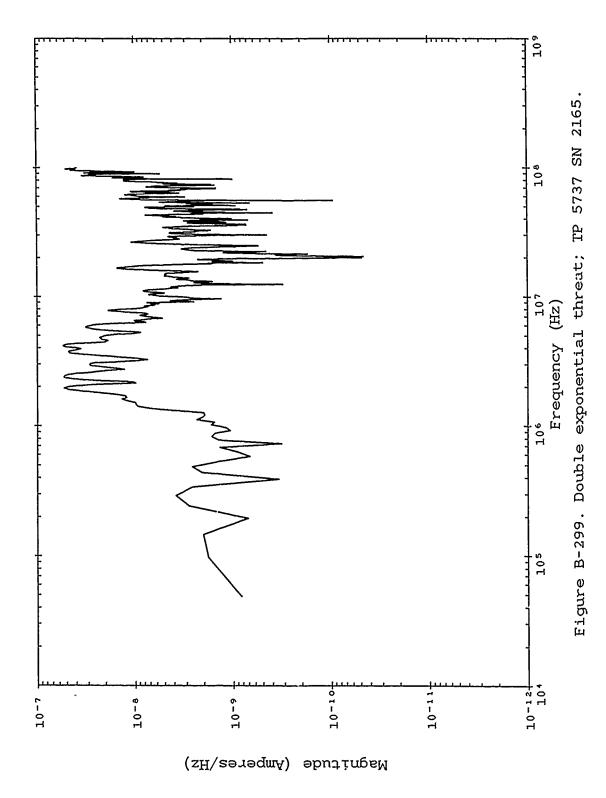


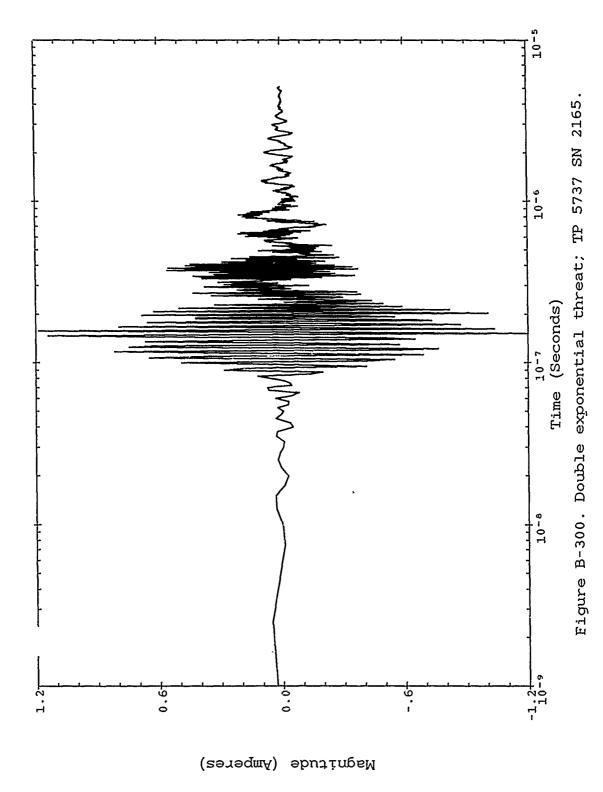


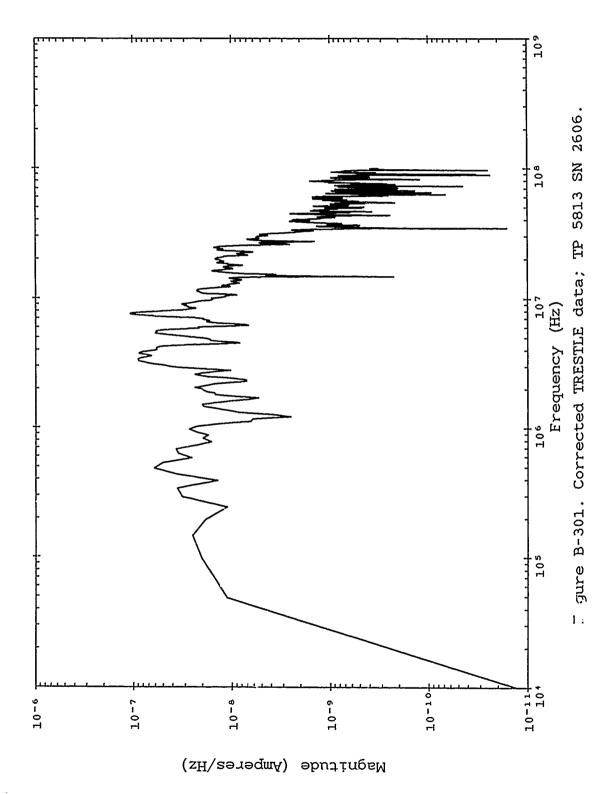
Magnitude (Amperes) x lE-3

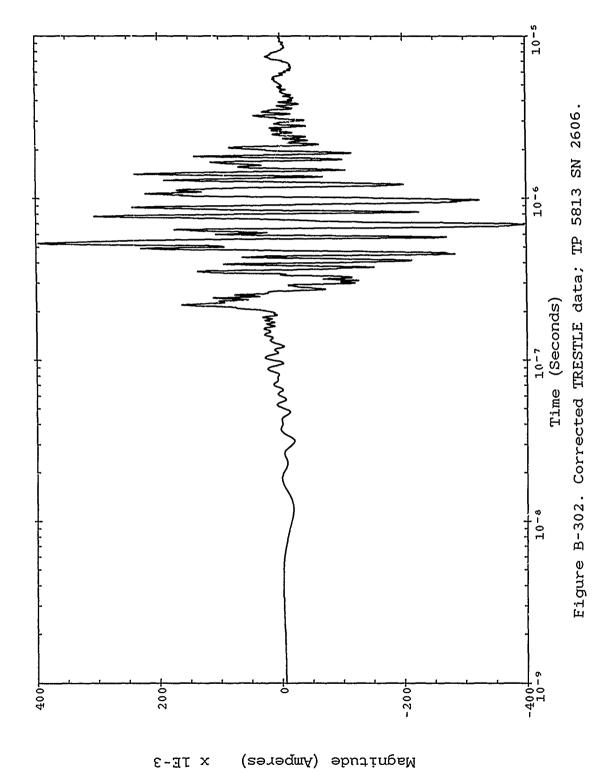


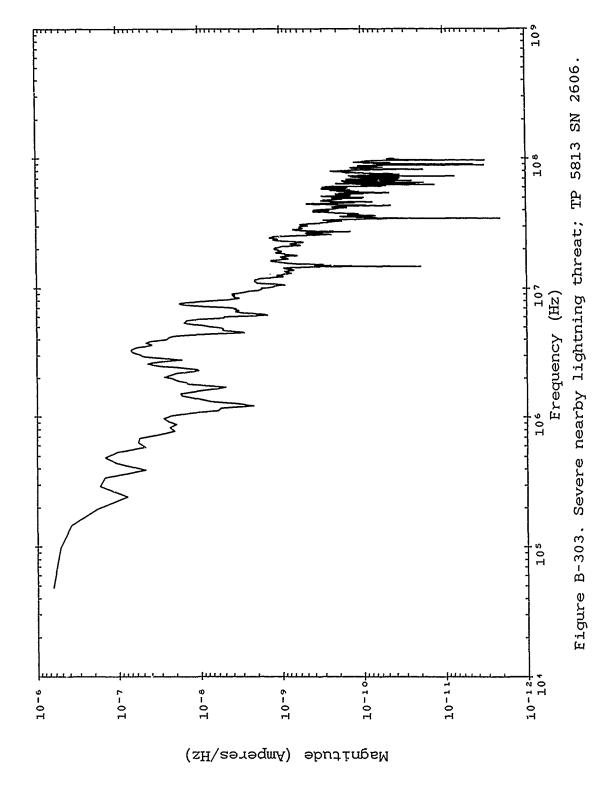




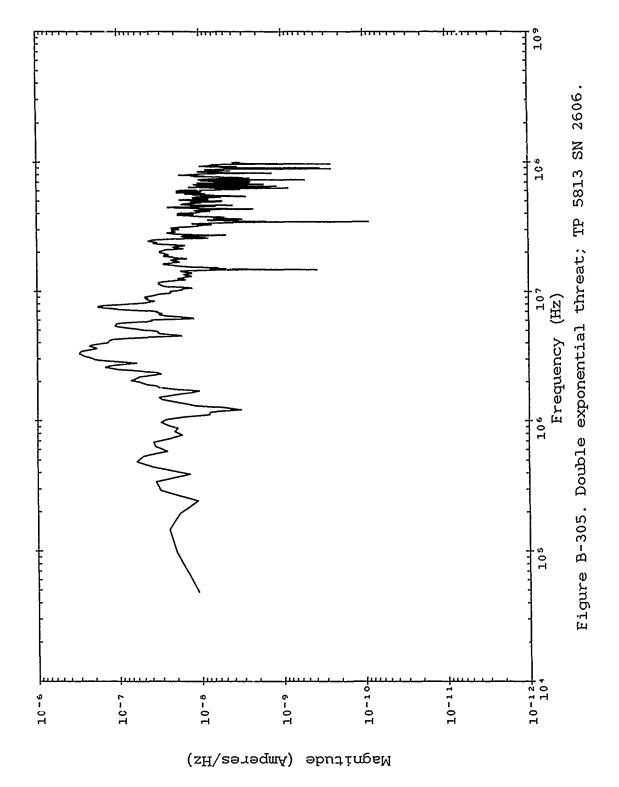


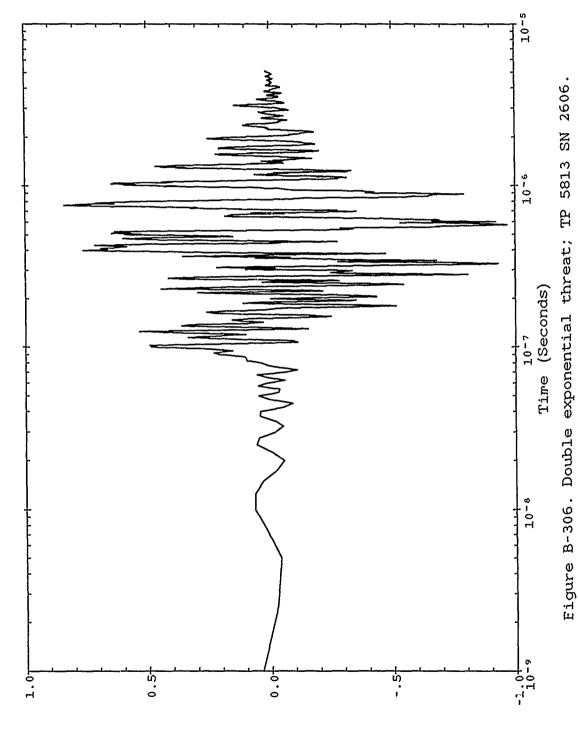




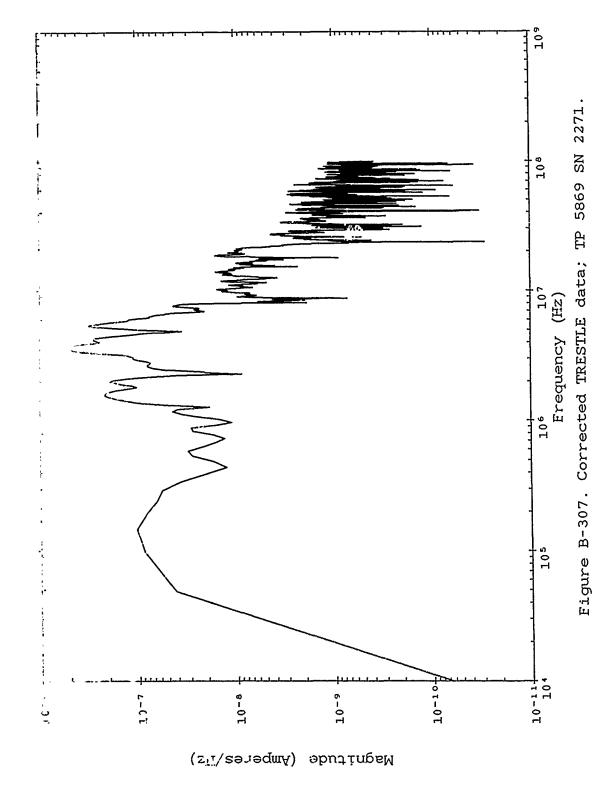


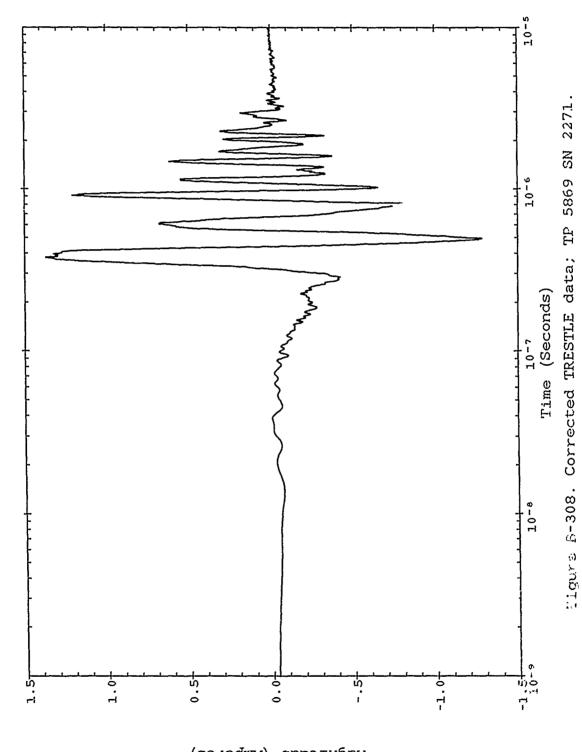
335



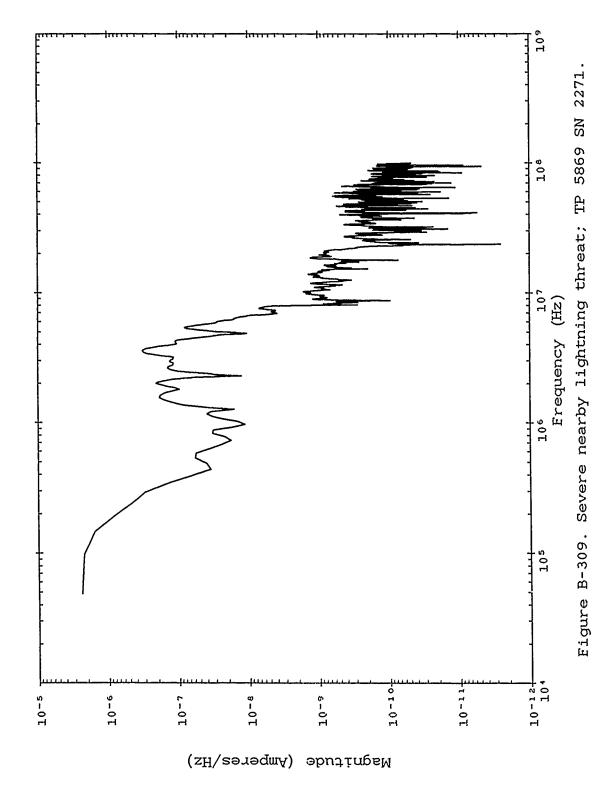


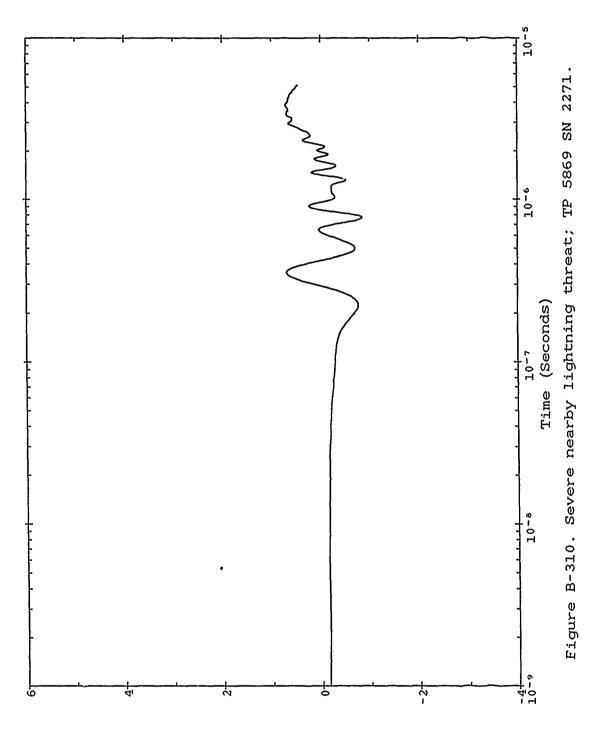
Magnitude (Amperes)



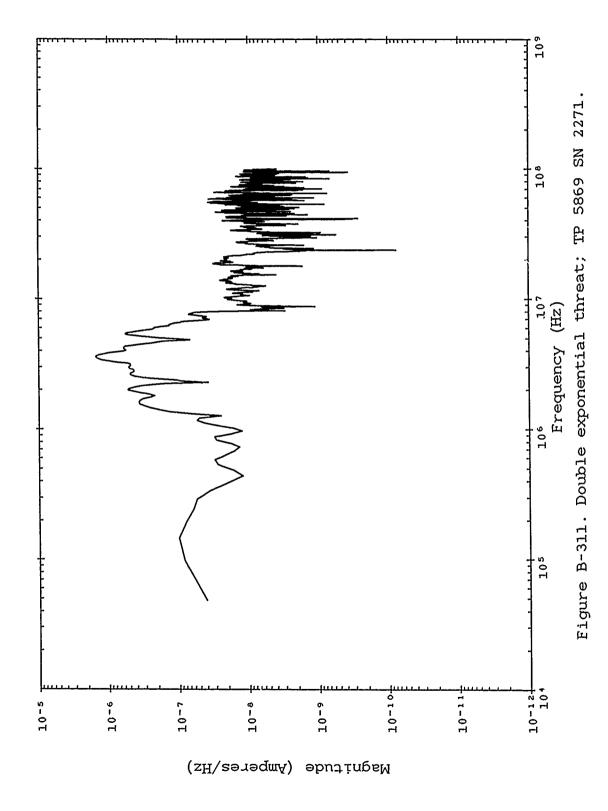


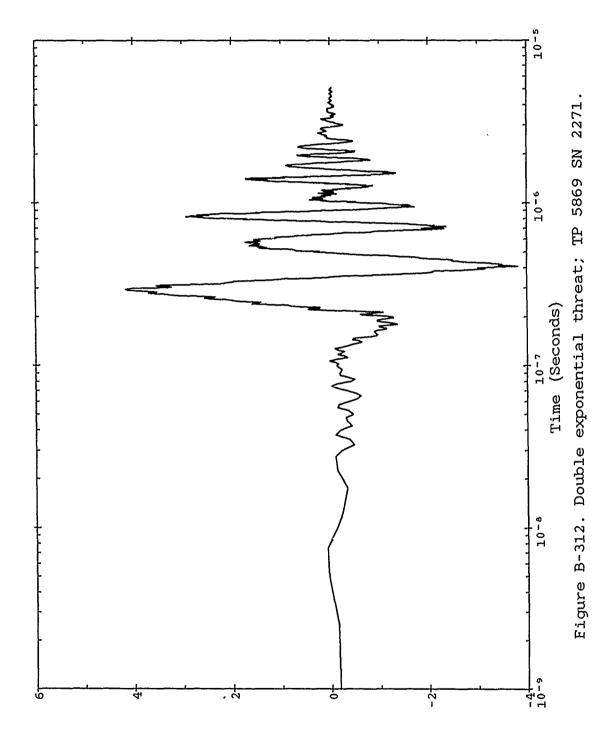
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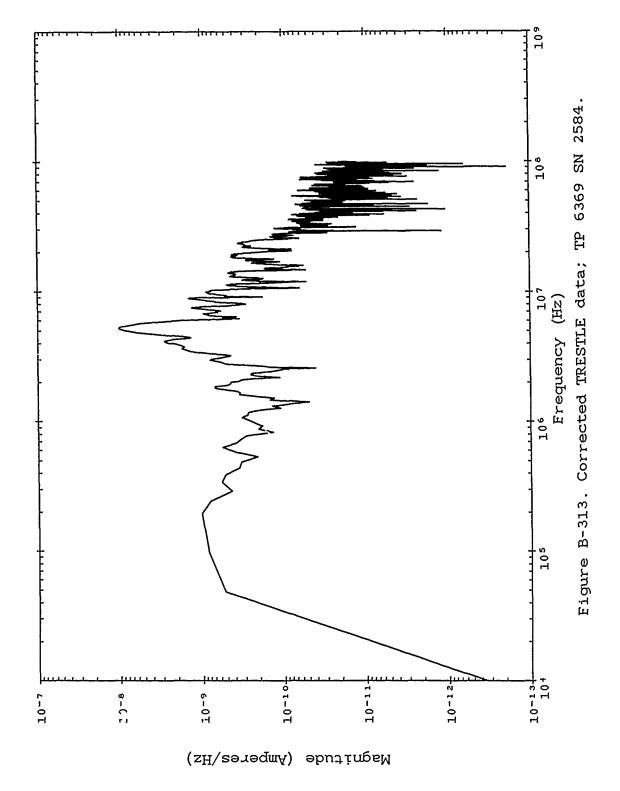


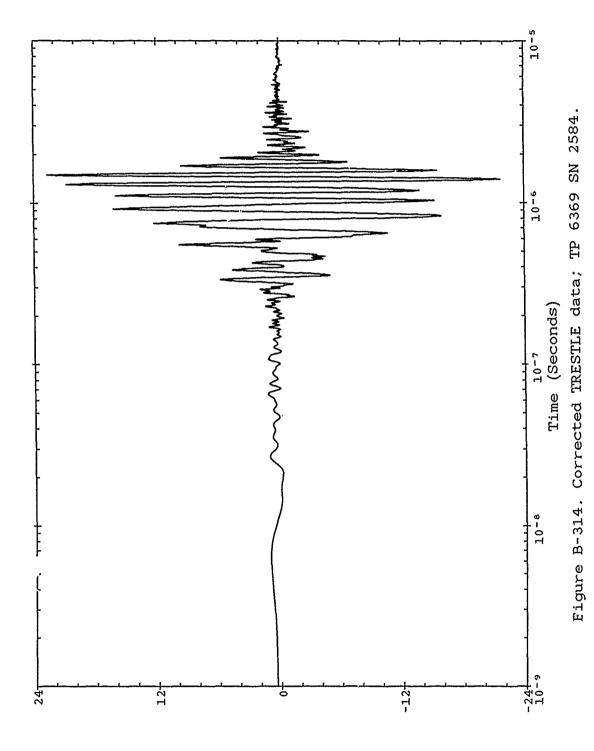
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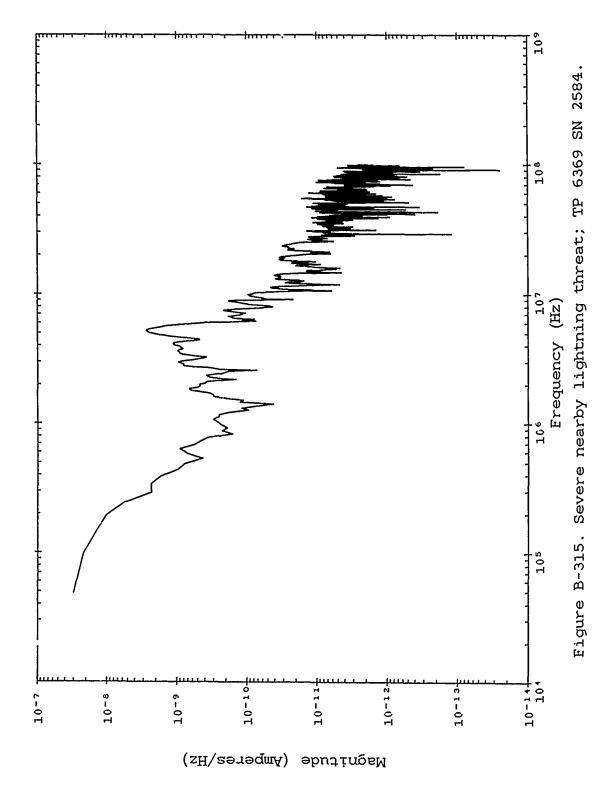


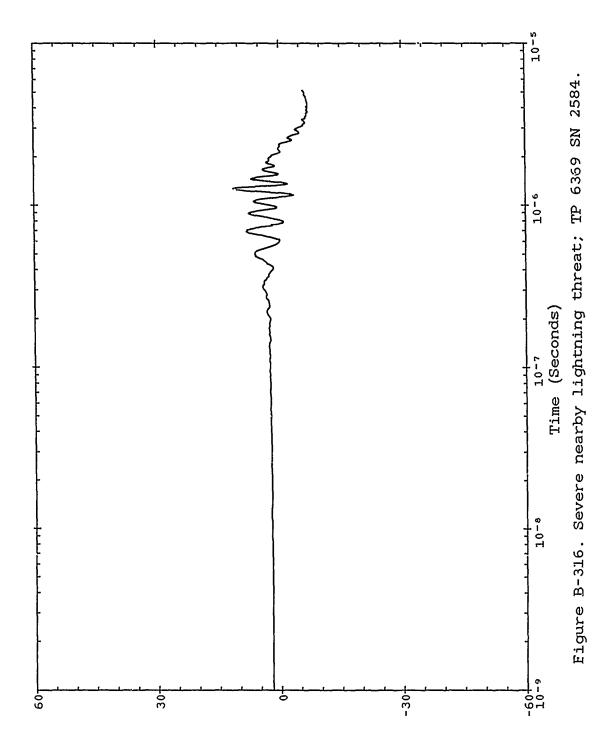
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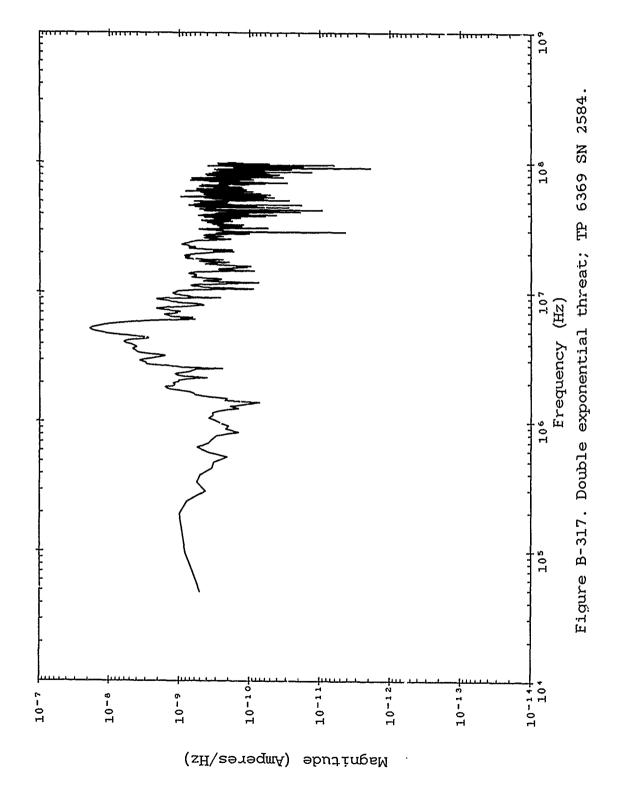
Wagnitude (Amperes) \times 1E-3

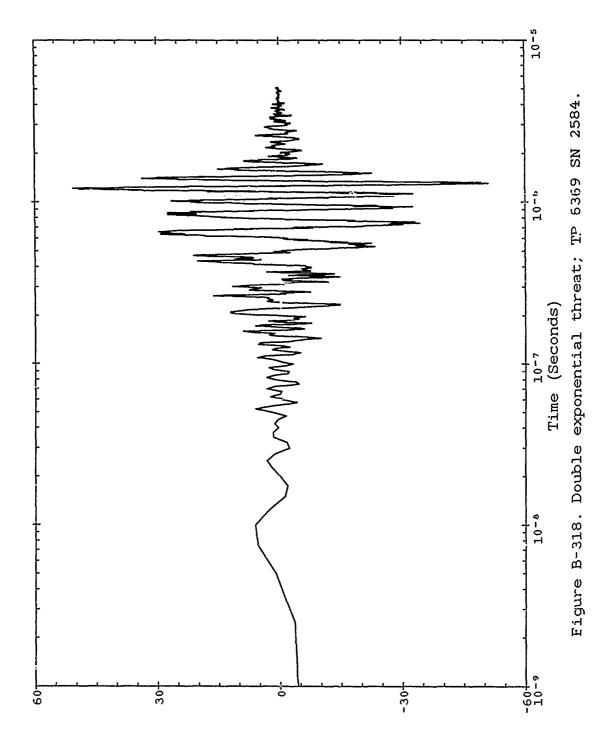




Magnitude (Amperes)

x TE-3



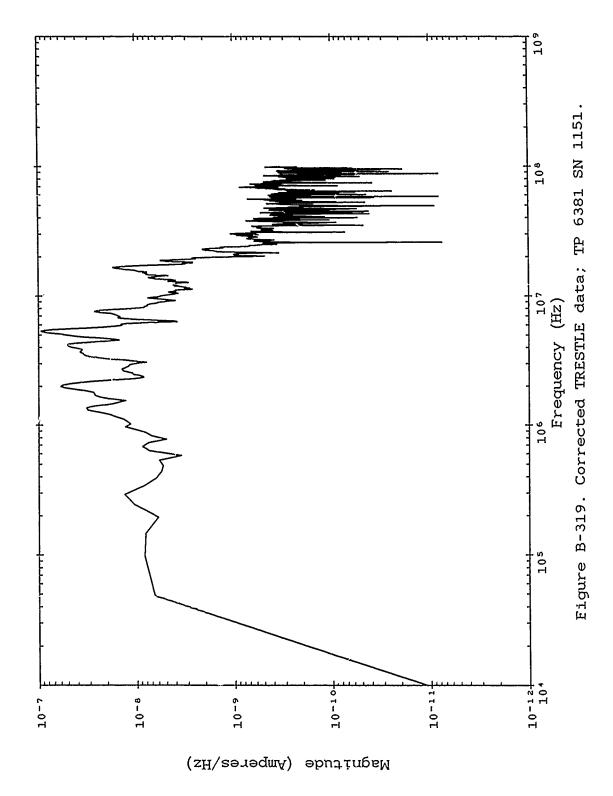


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Magnitude (Amperes)

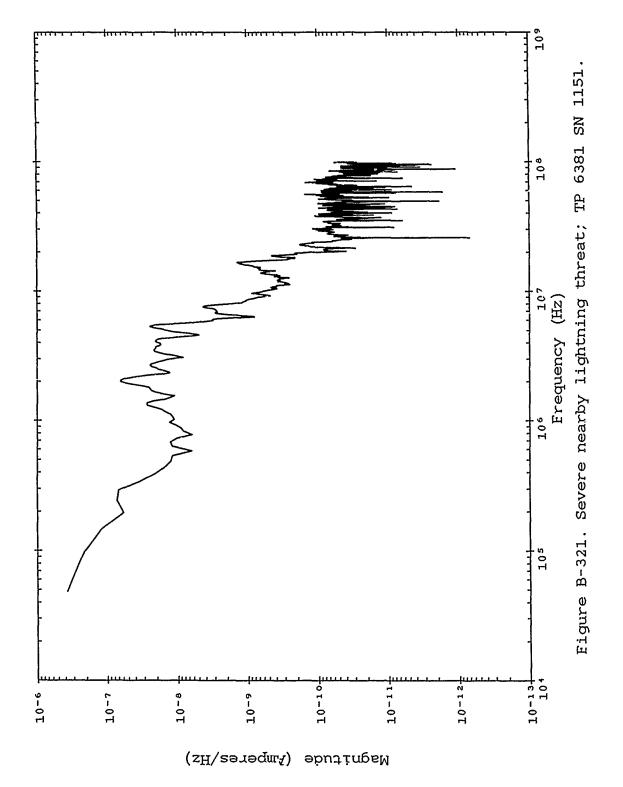
x JE-3

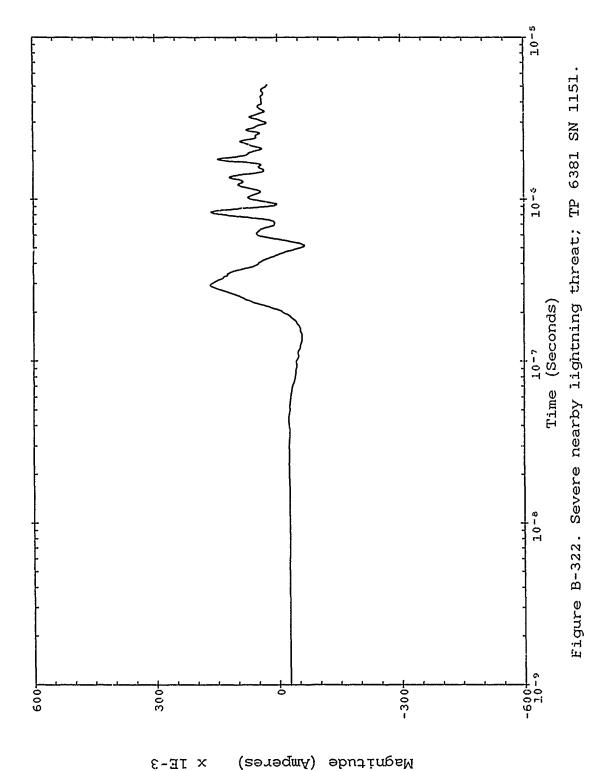


351

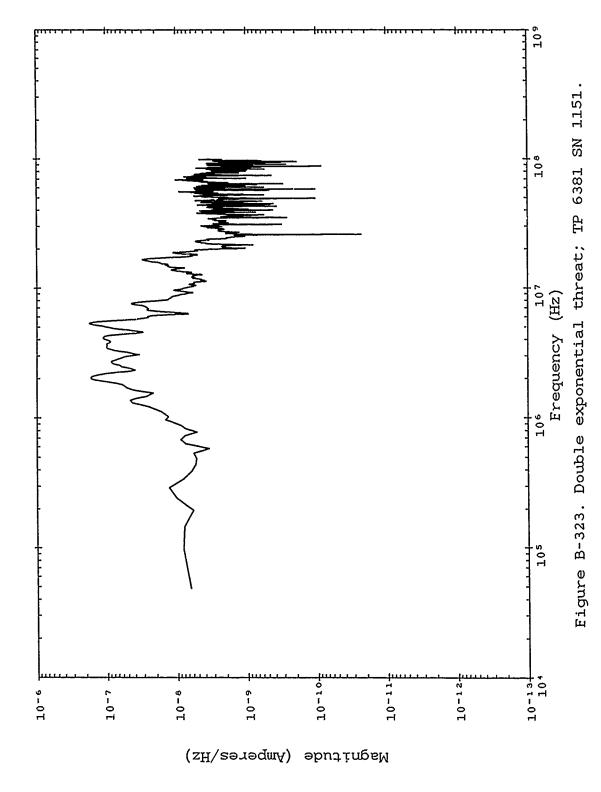
Magnitude (Amperes)

 \times TE-3





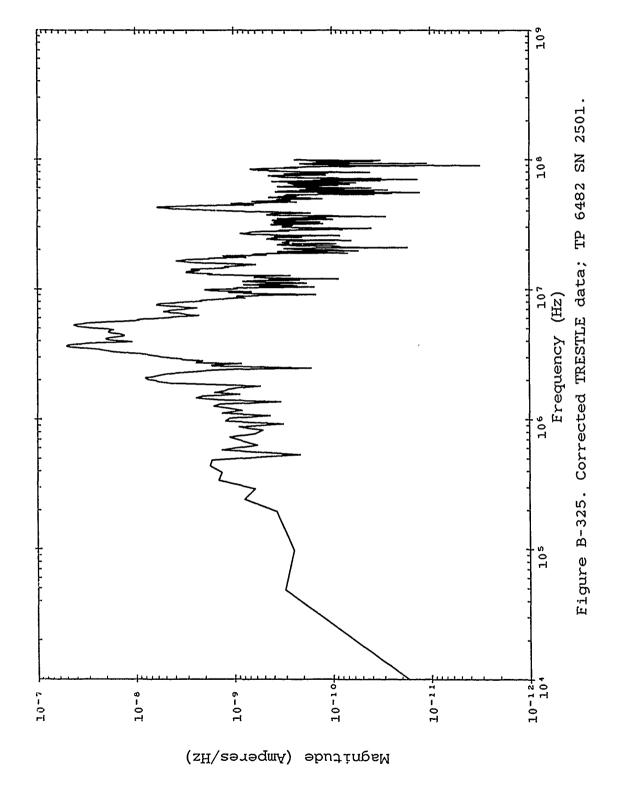
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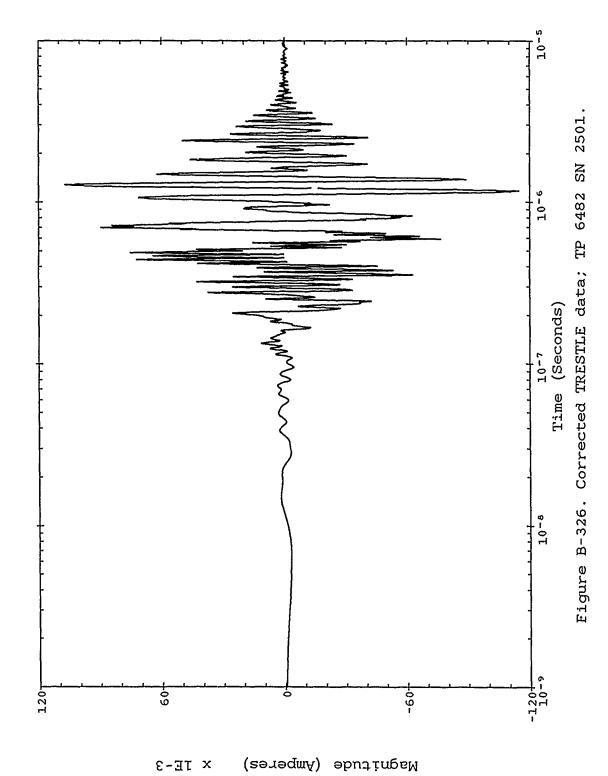


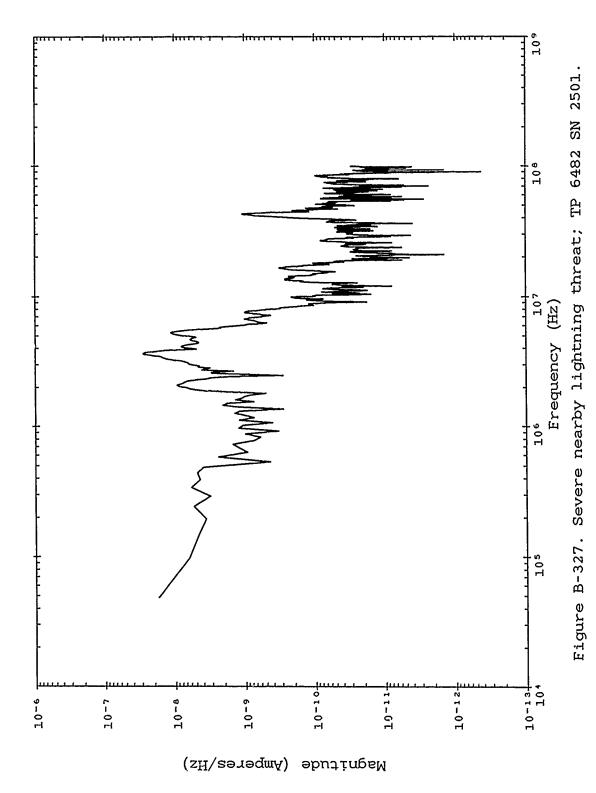
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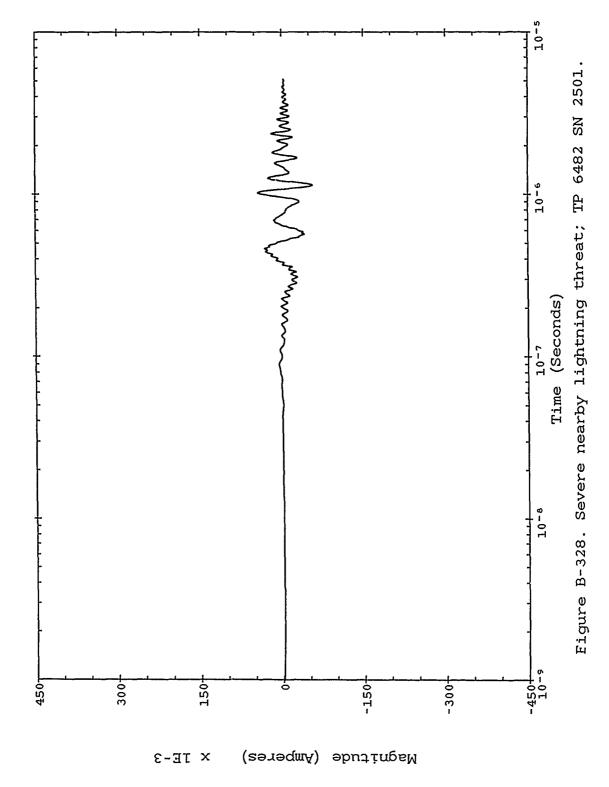
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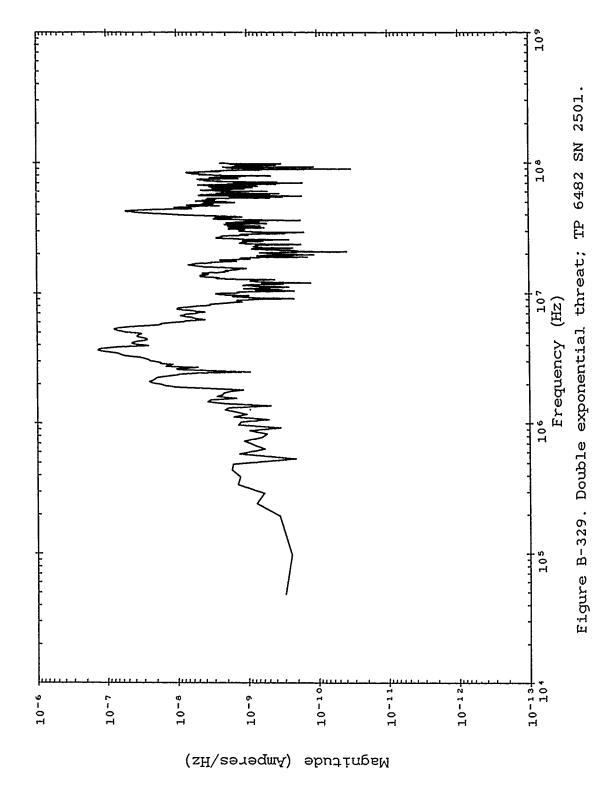
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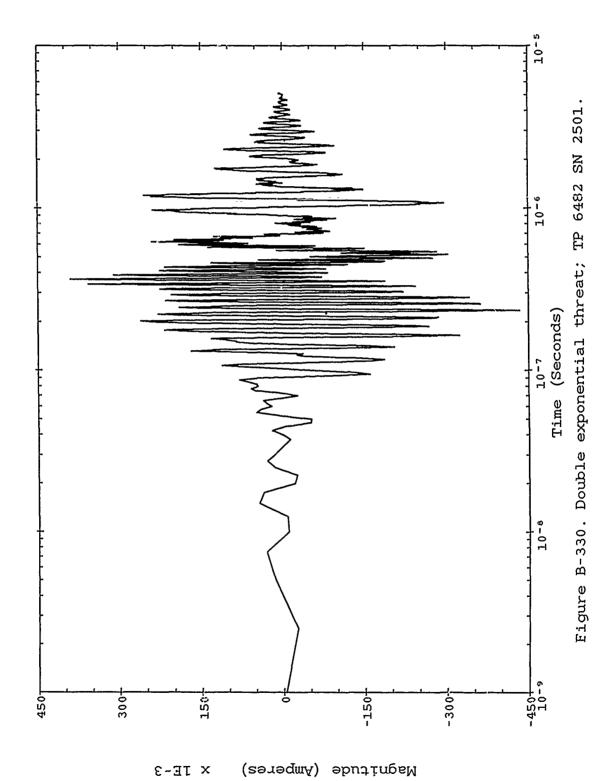


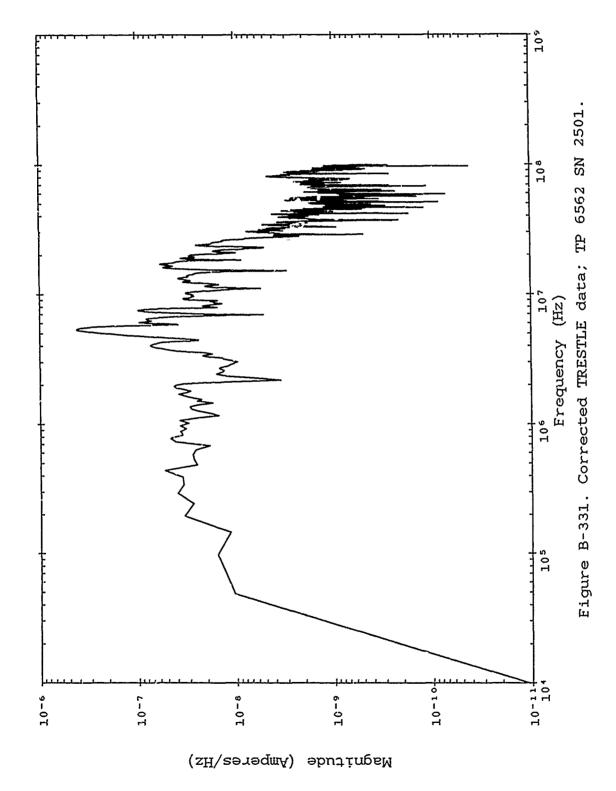


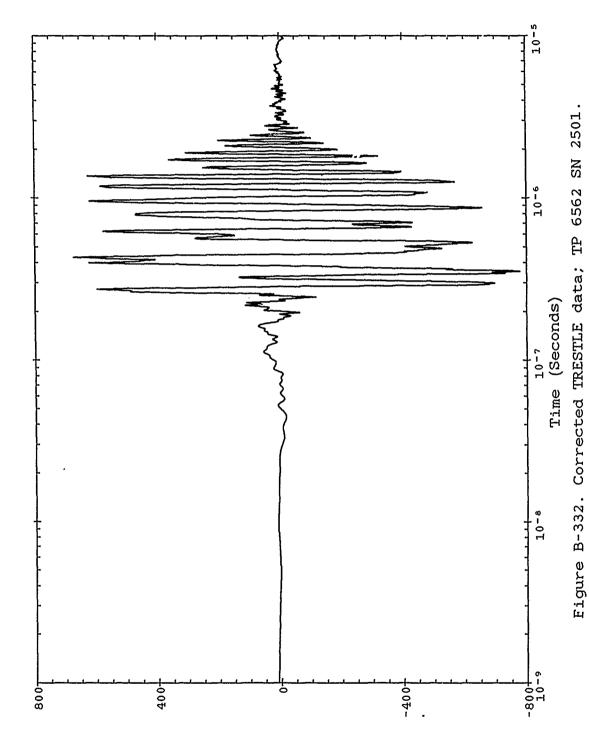




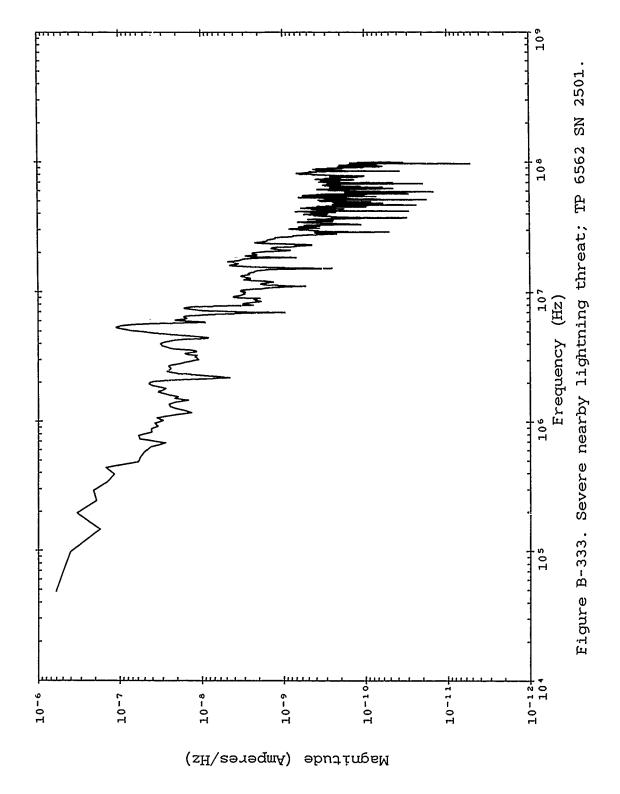


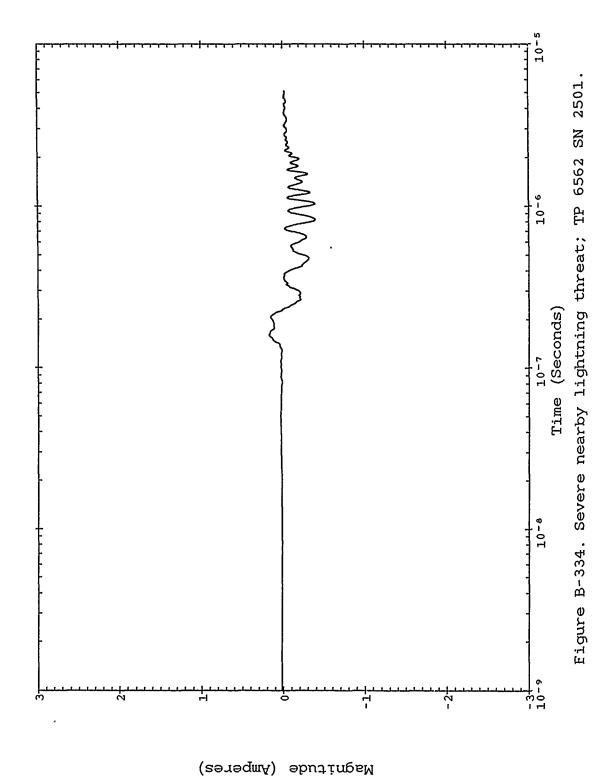


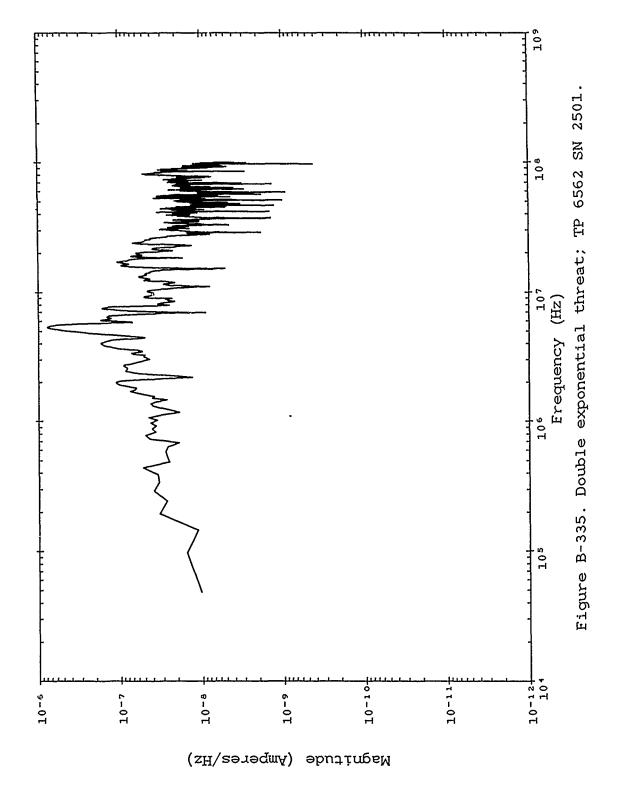


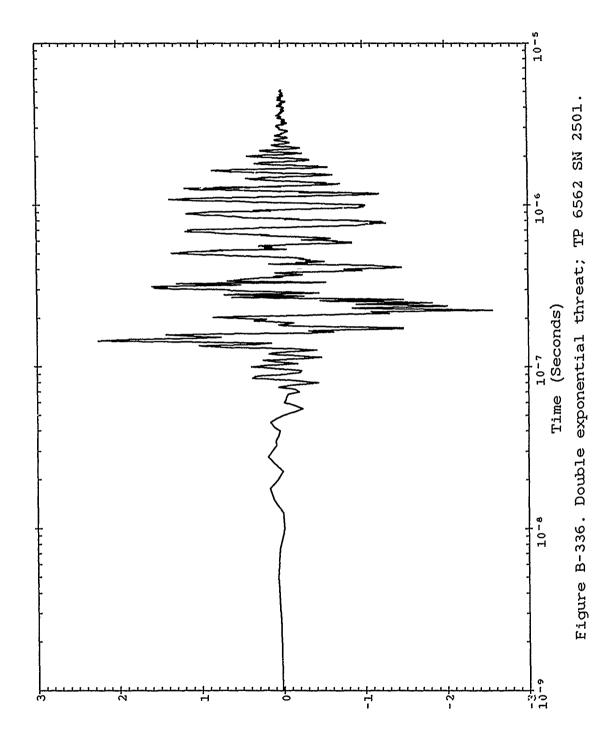
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Magnitude (Amperes) x lE-3

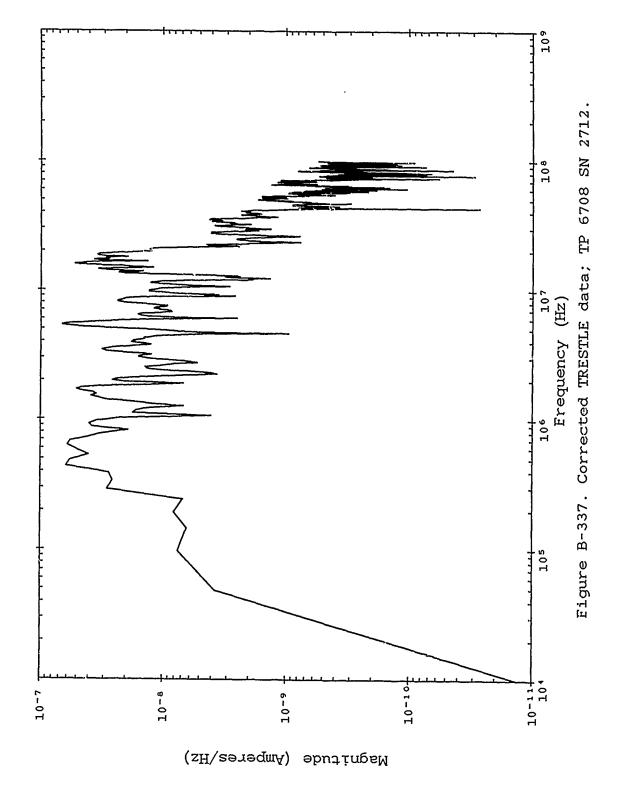


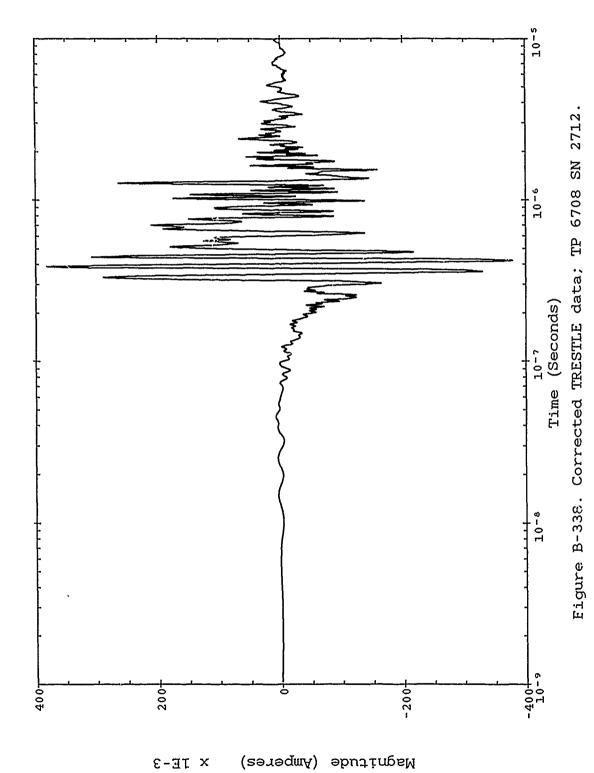




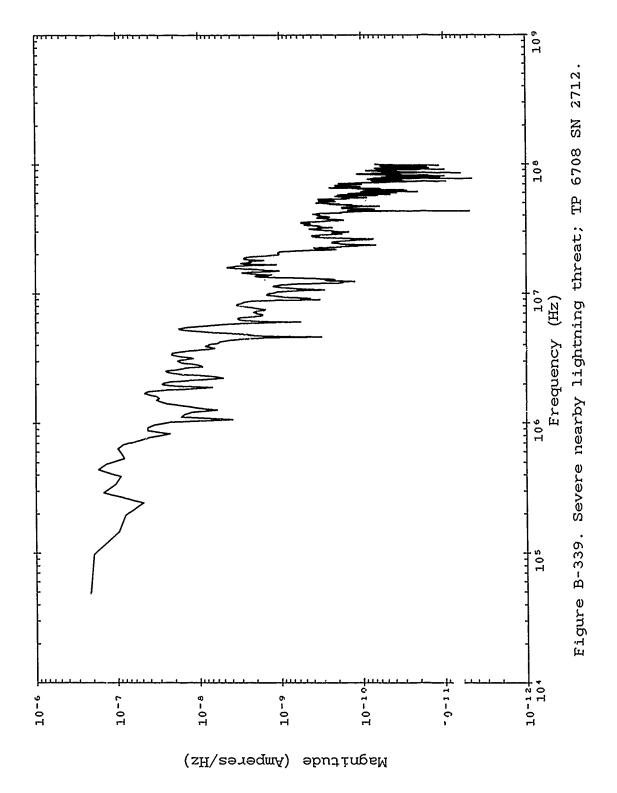


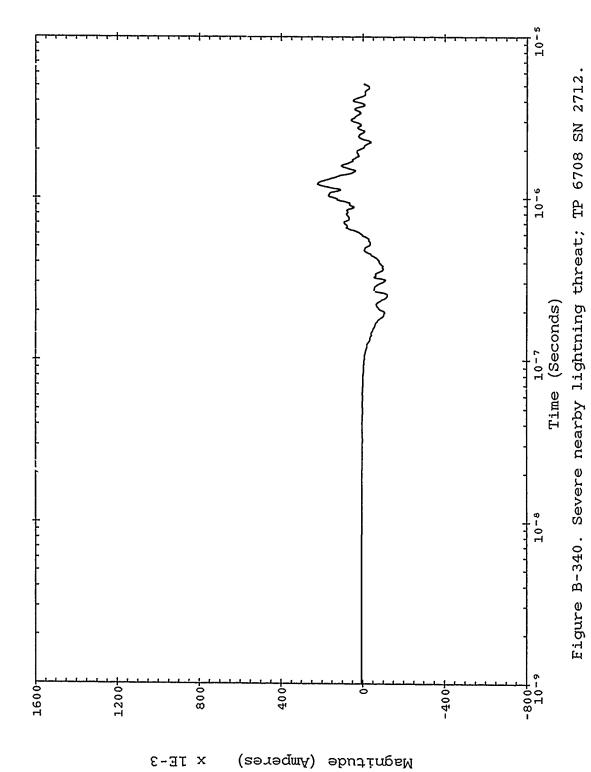
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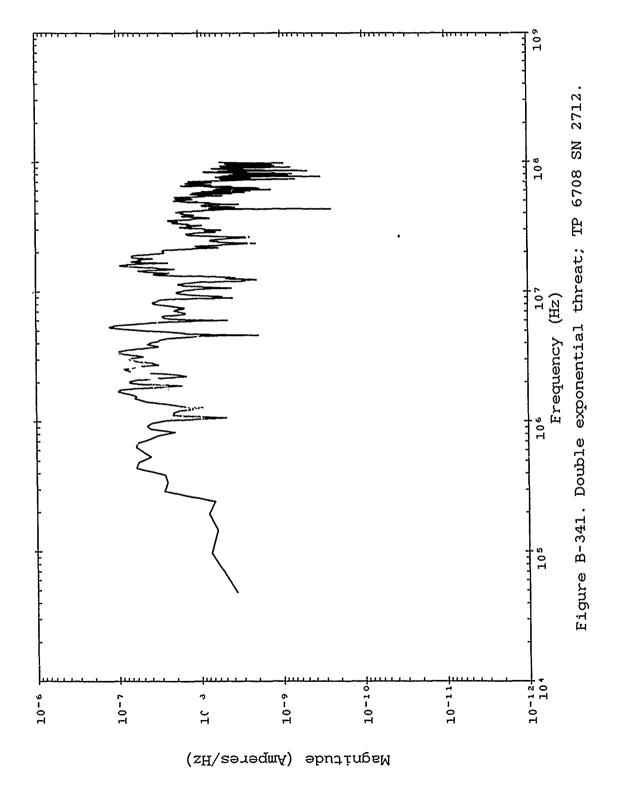


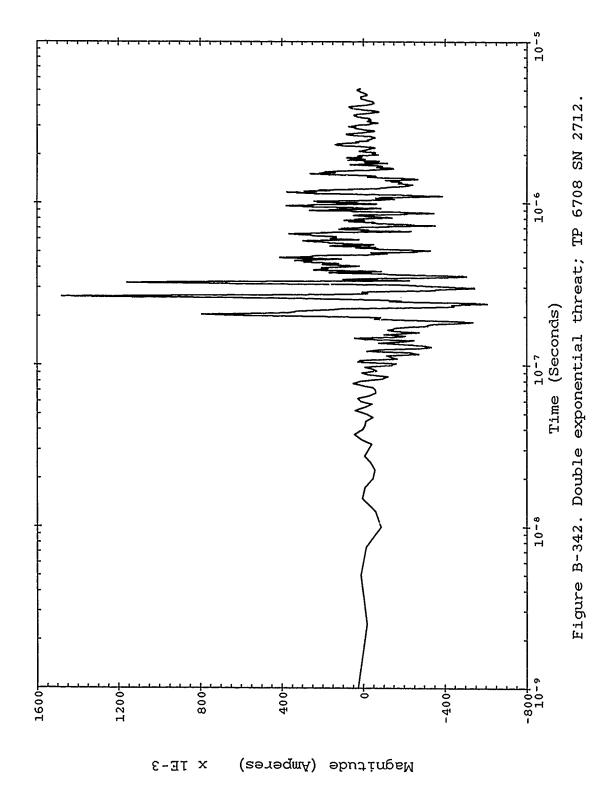


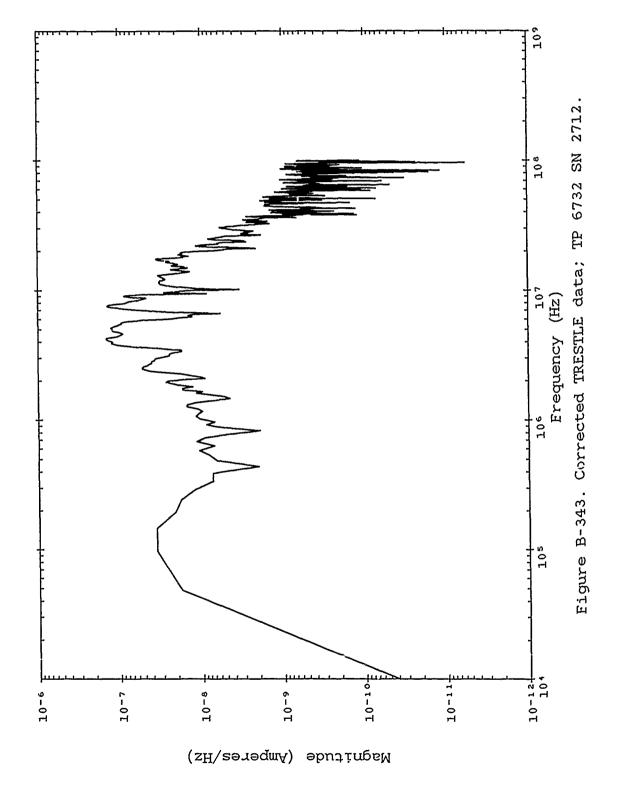
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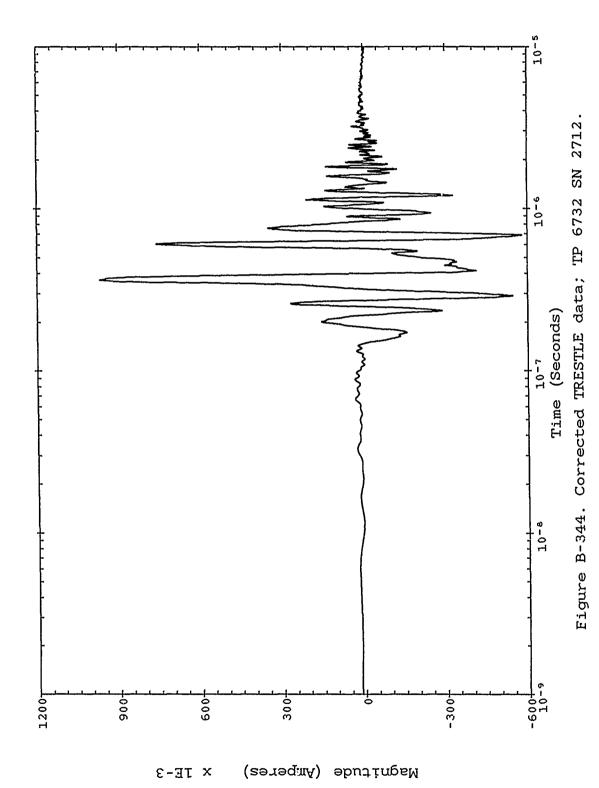


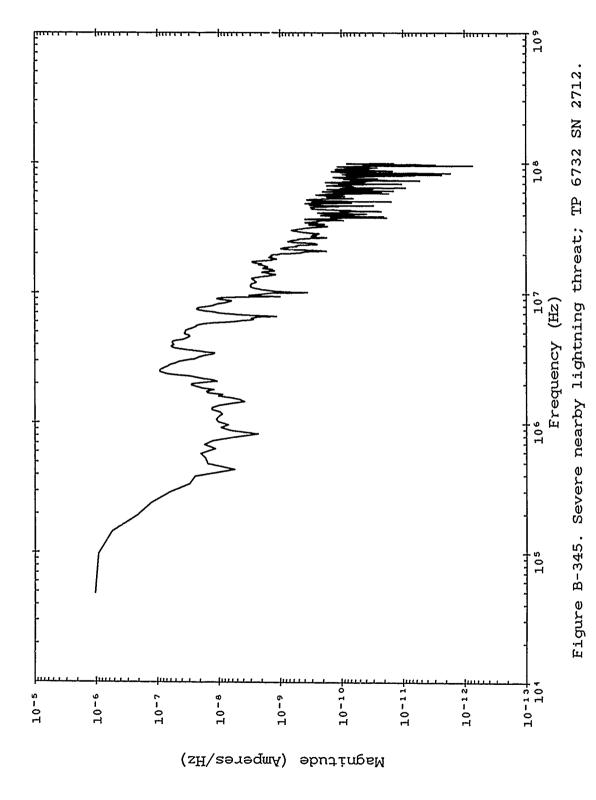


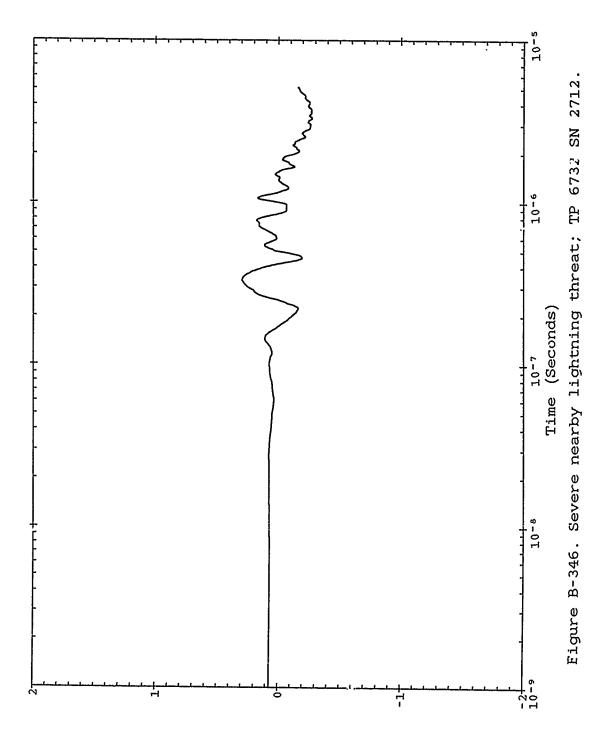




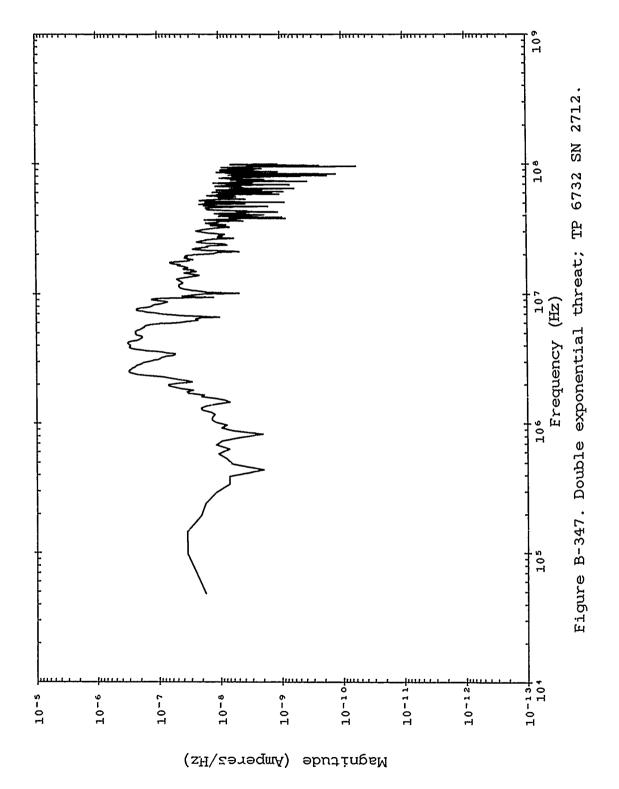


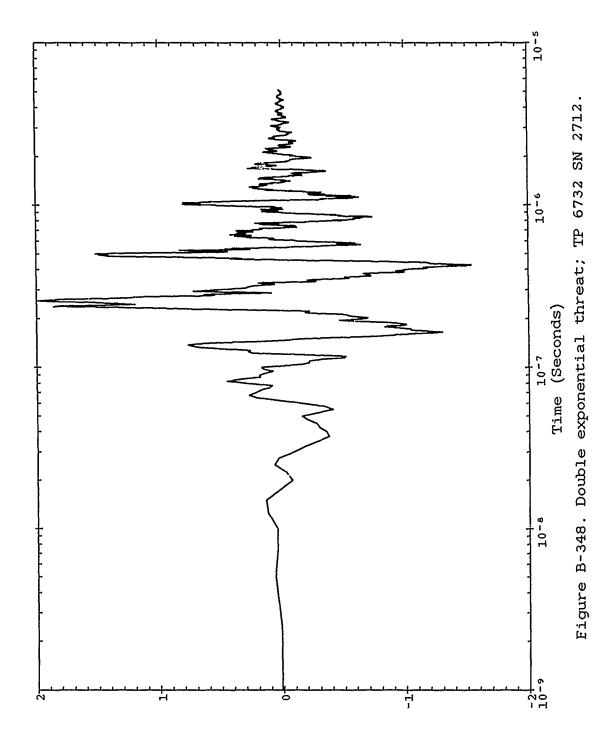




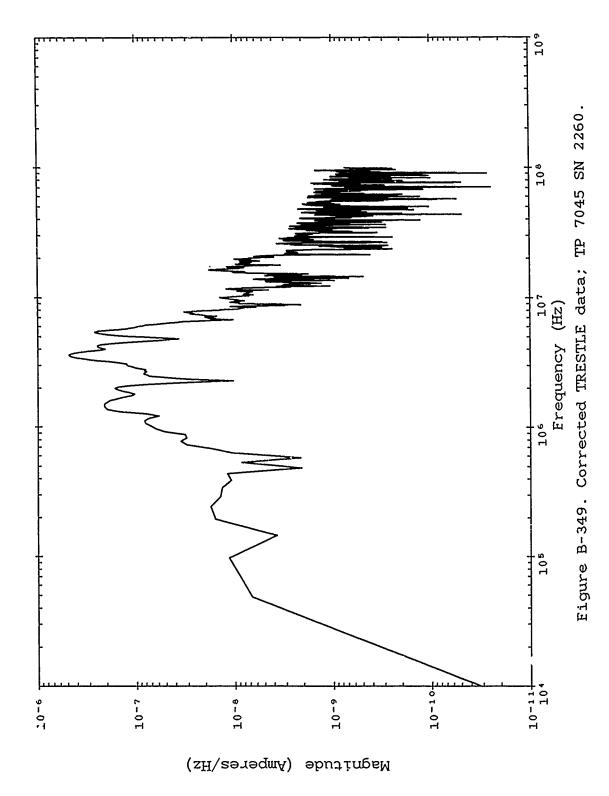


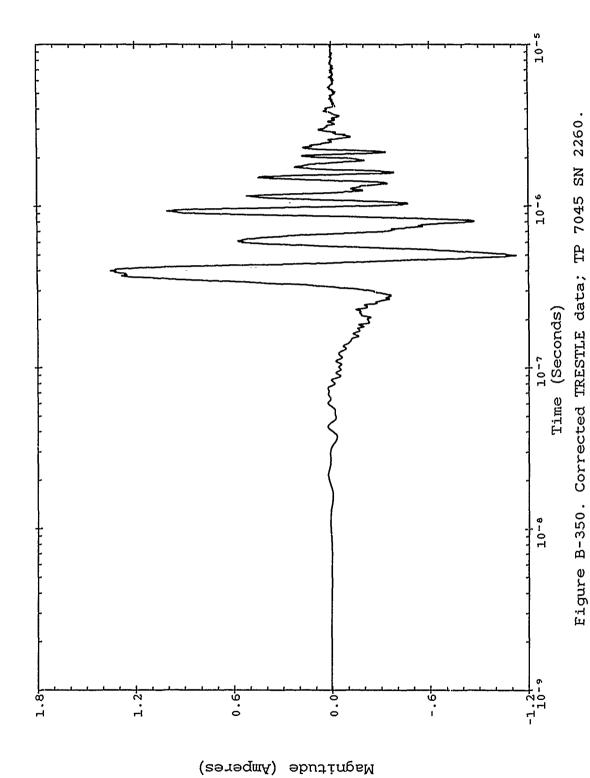
Magnitude (Amperes)

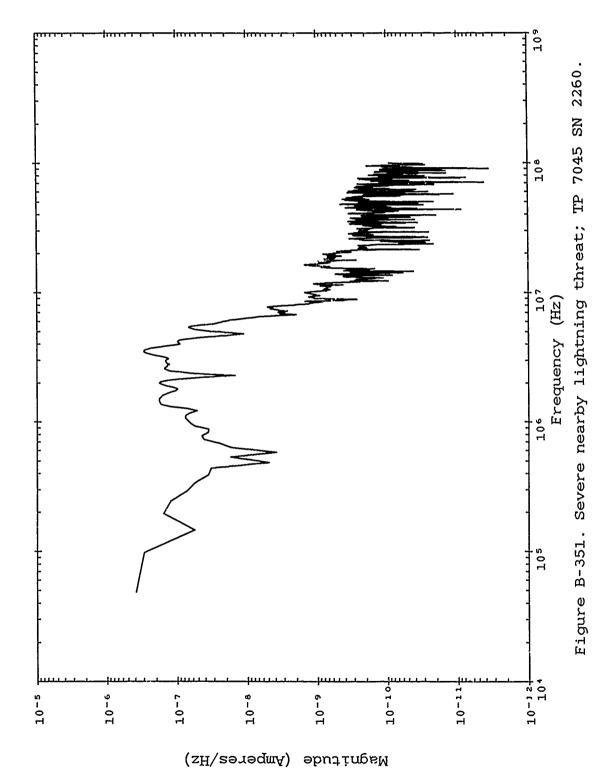


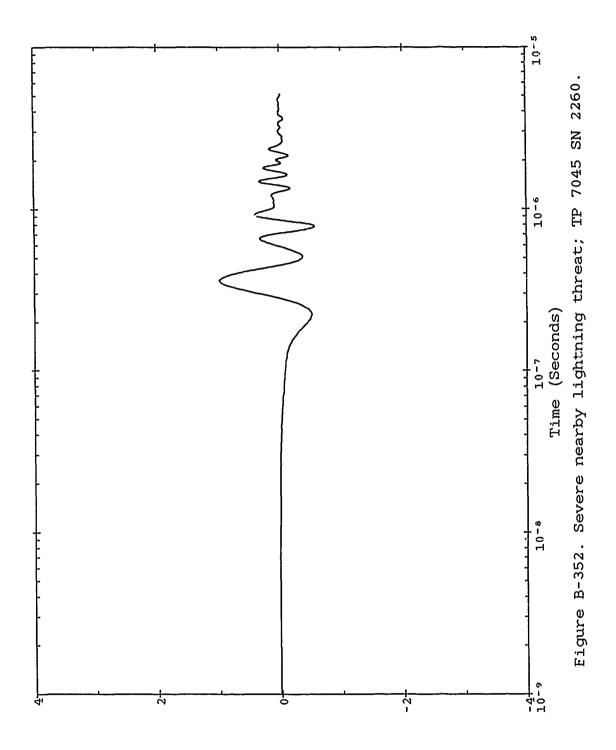


Magnitude (Amperes)



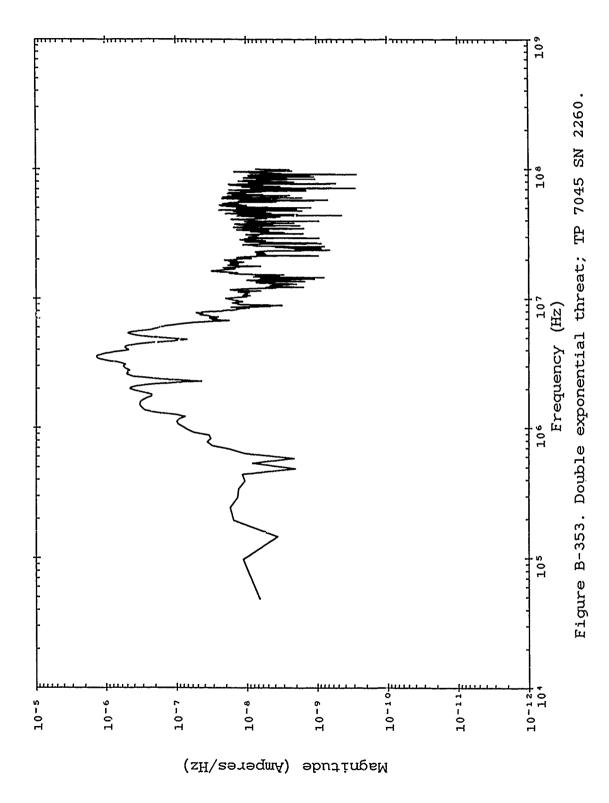


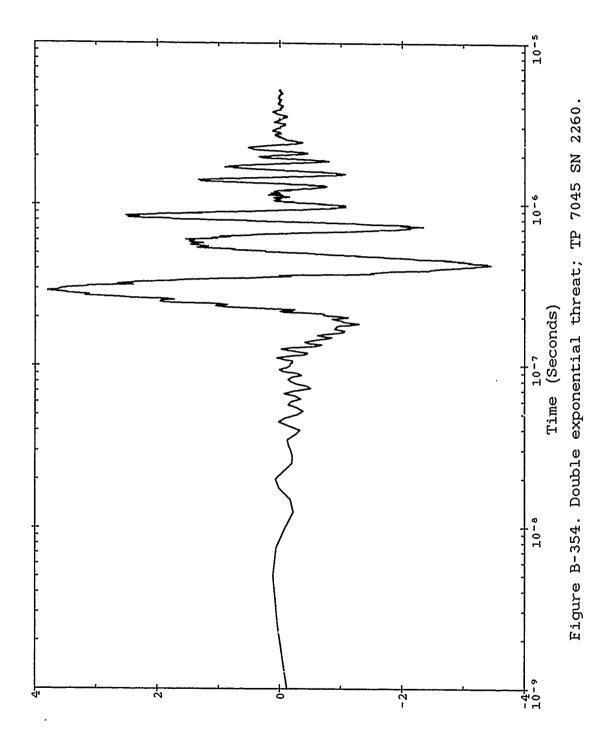




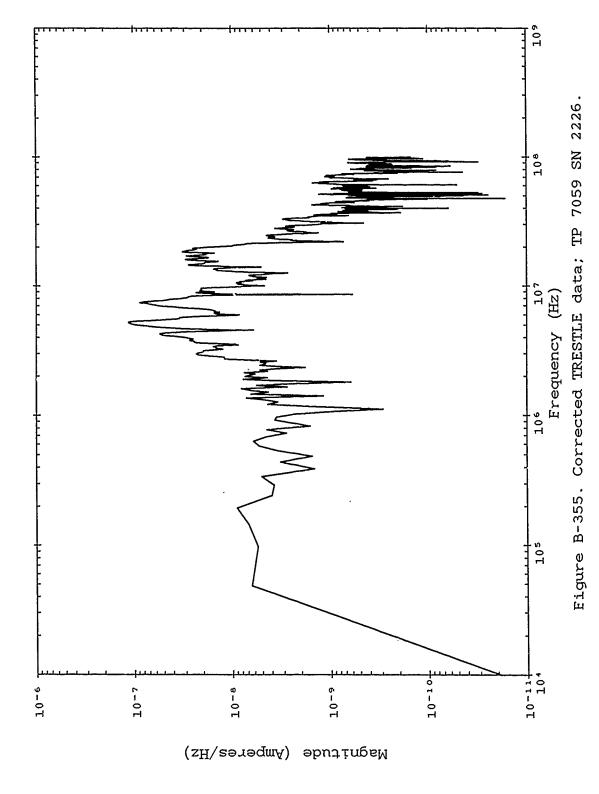
383

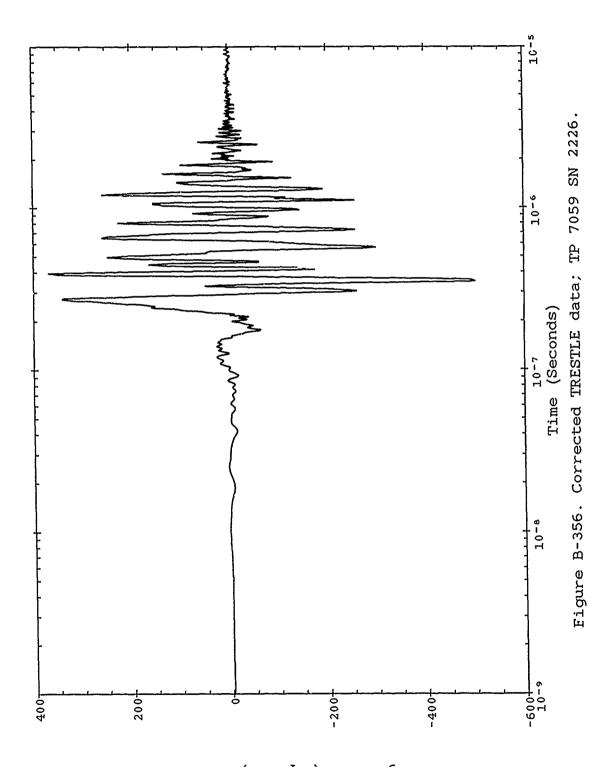
Magnitude (Amperes)





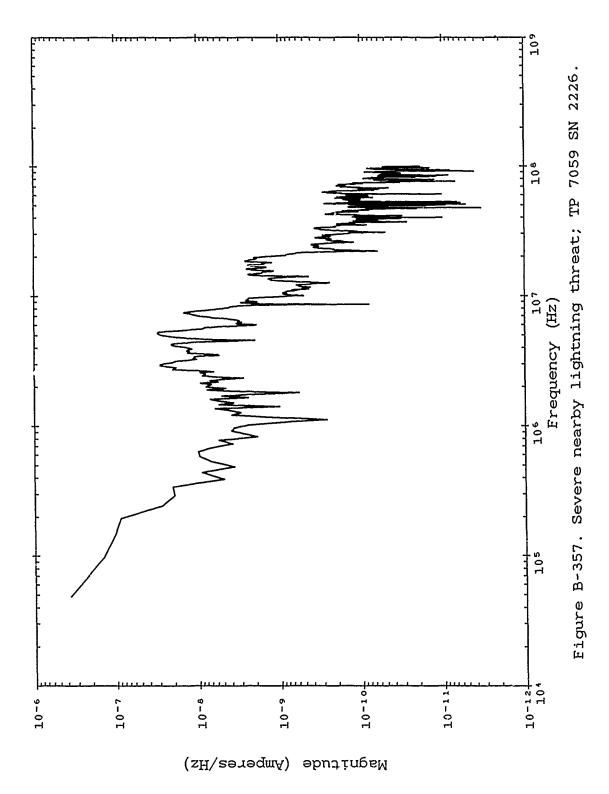
Magnitude (Amperes)





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Magnitude (Amperes) x lE-3



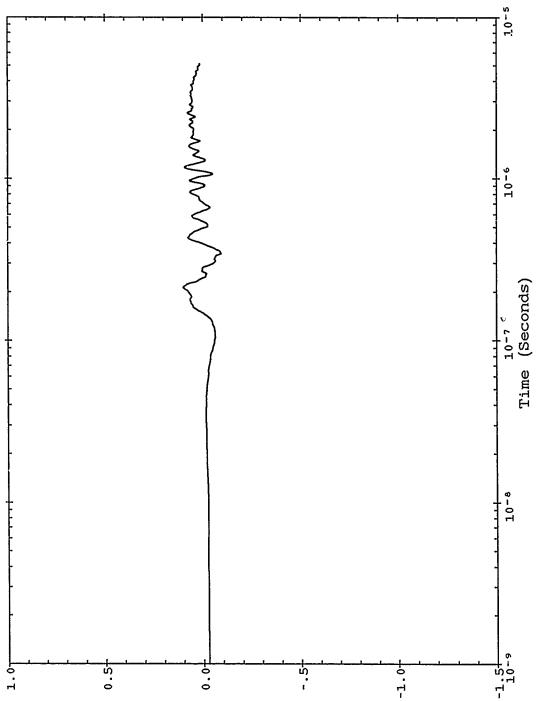
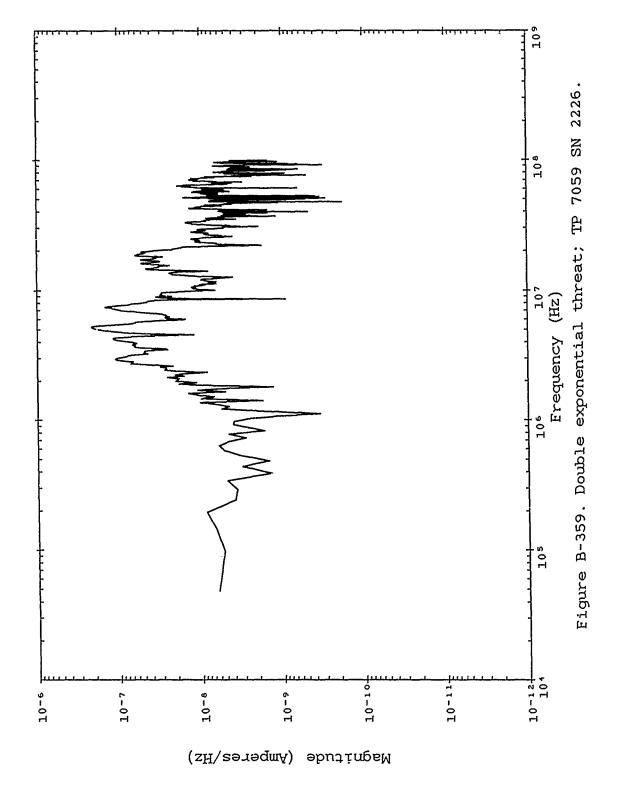
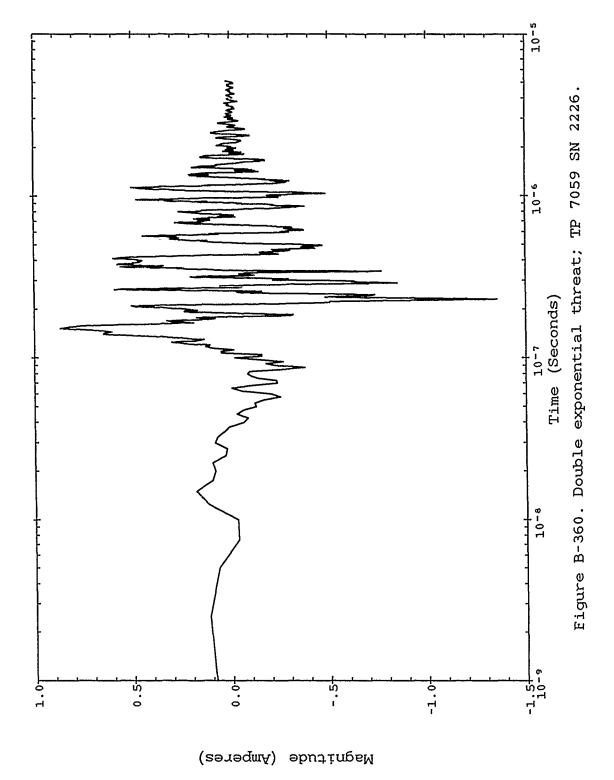
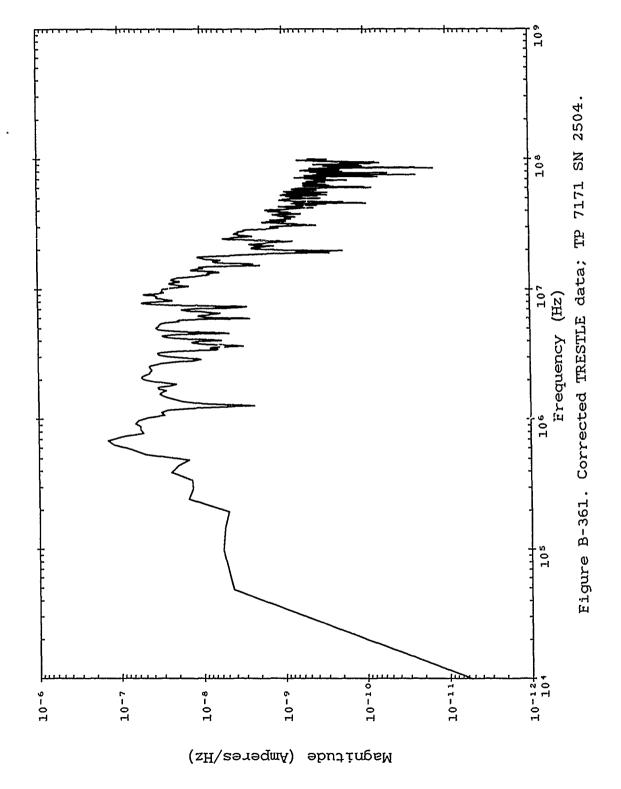


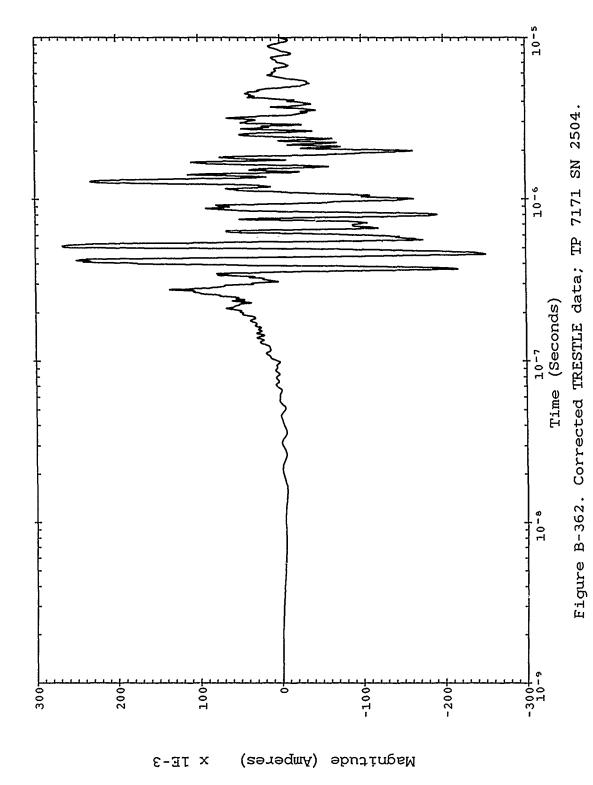
Figure B-358. Severe nearby lightning threat; TP 7059 SN 2226.

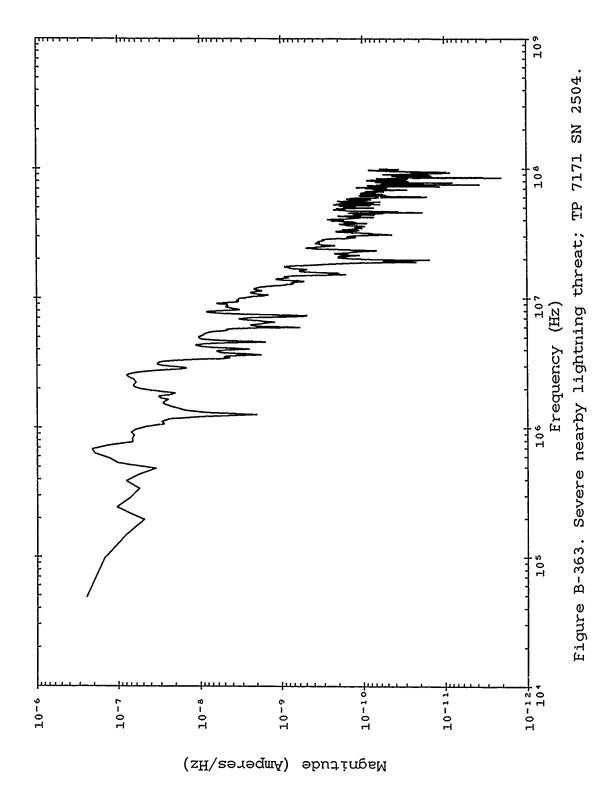
Magnit:ude (Amperes)

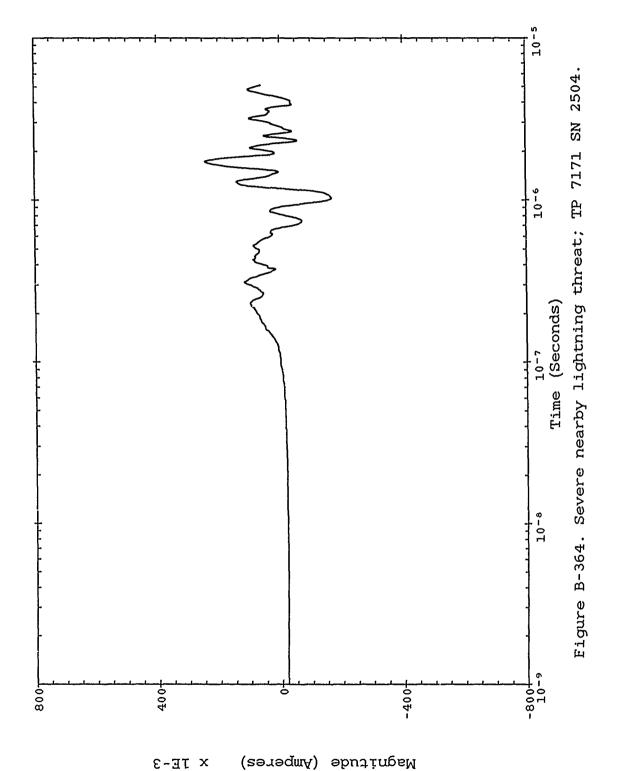


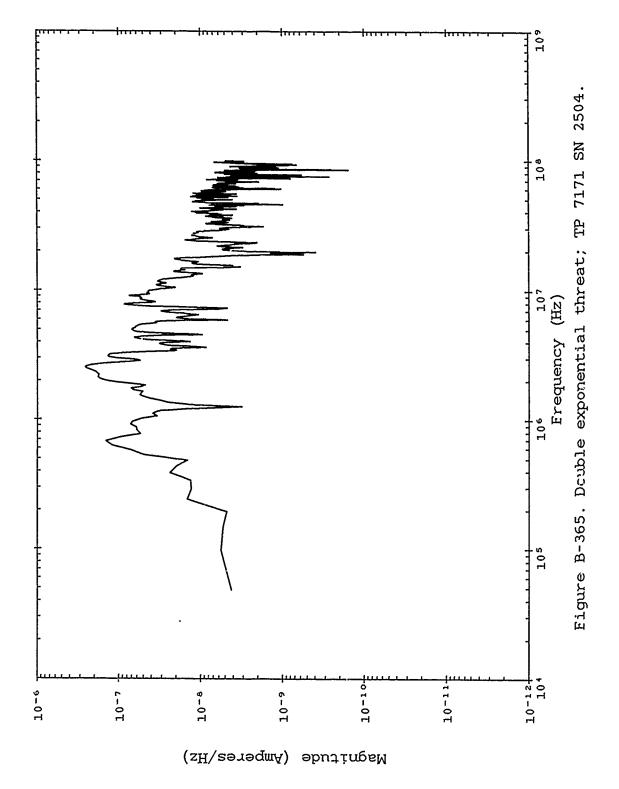


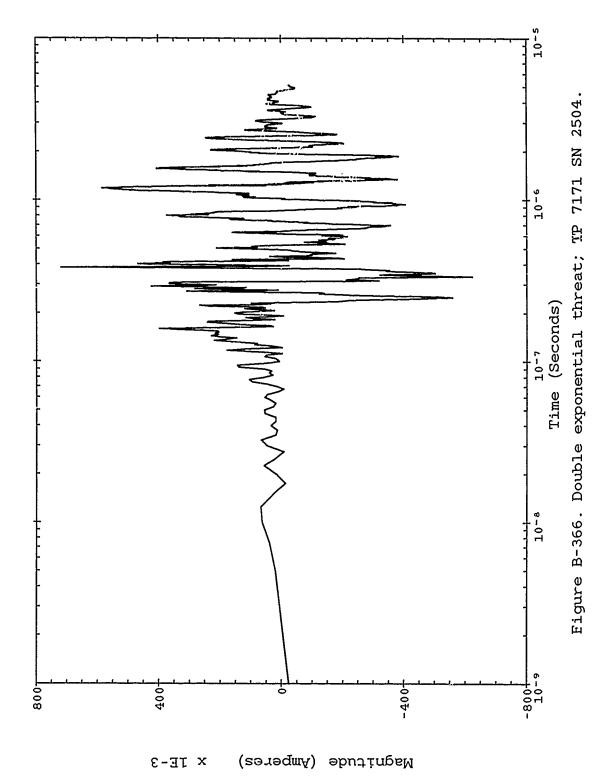


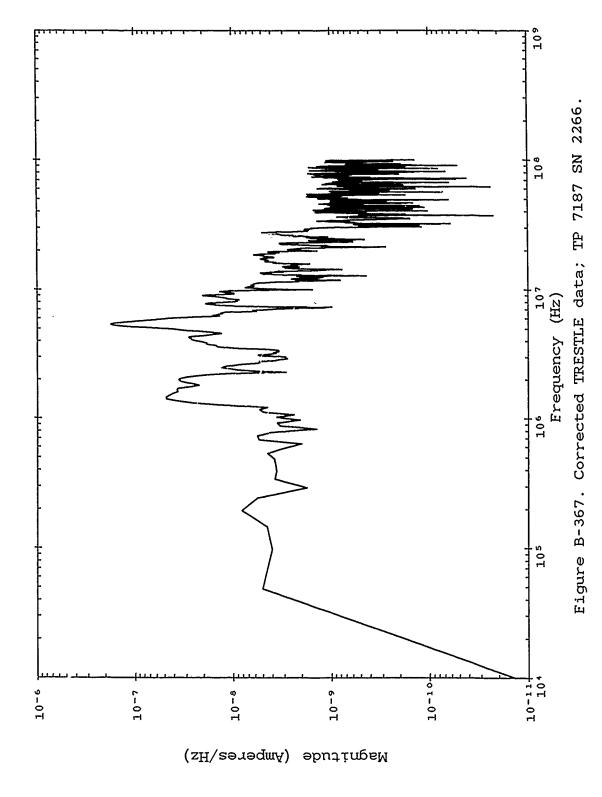


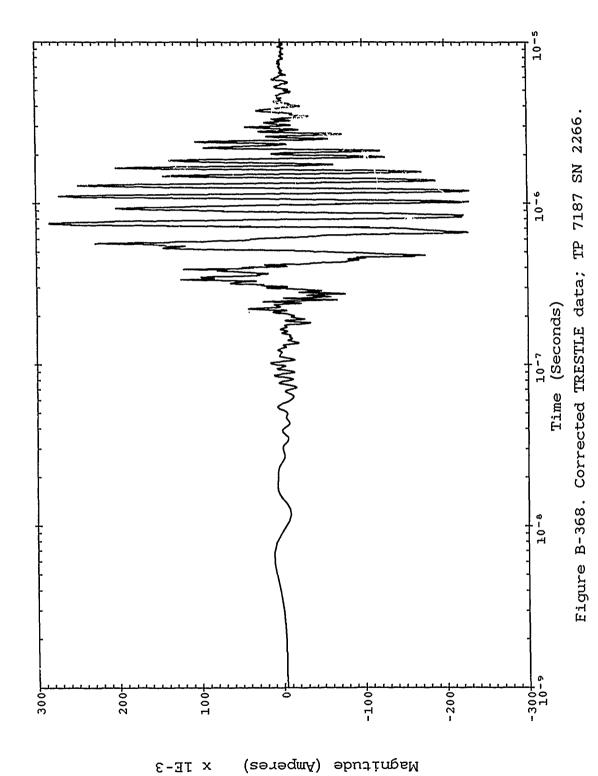


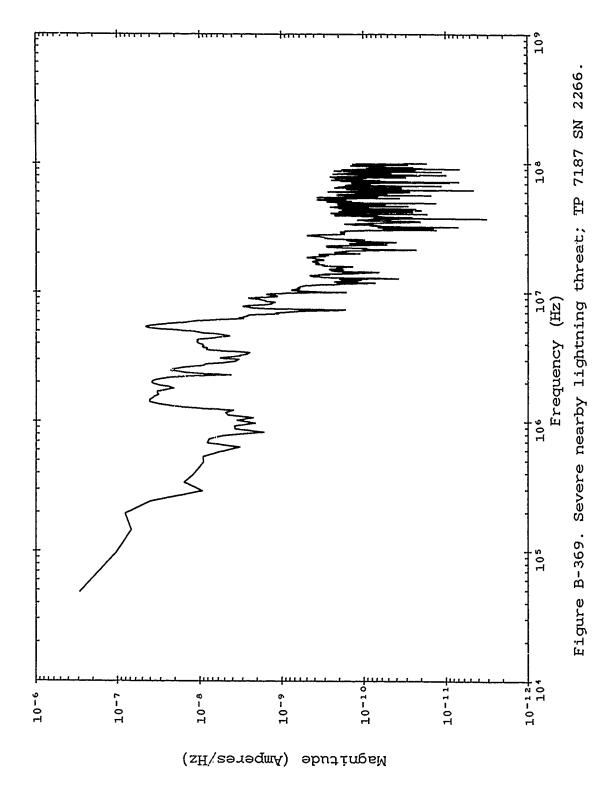


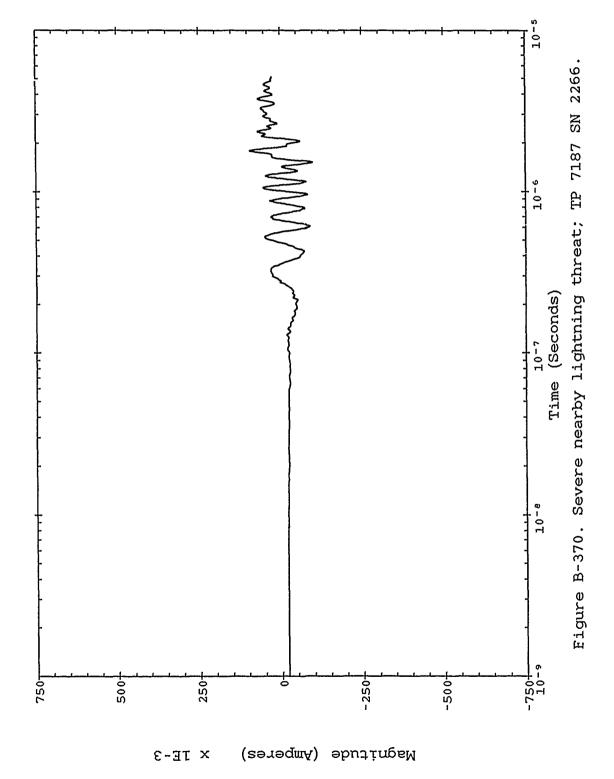




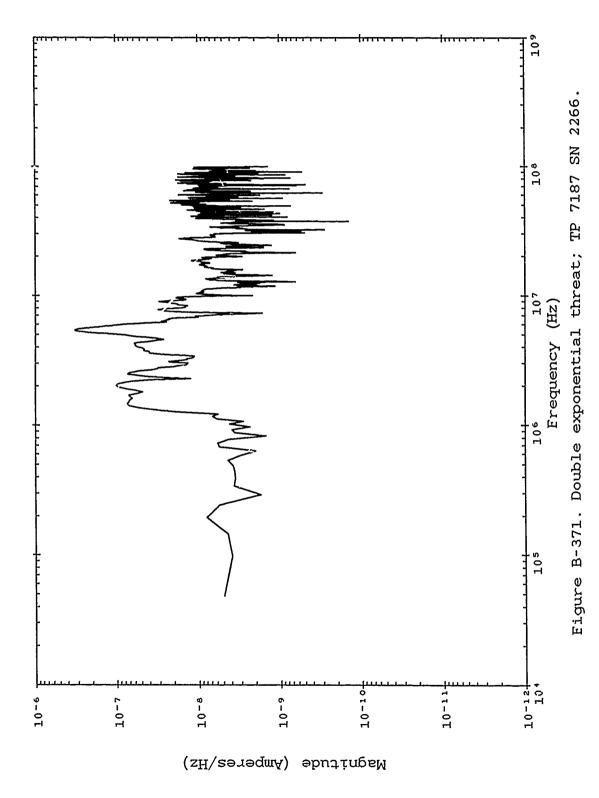


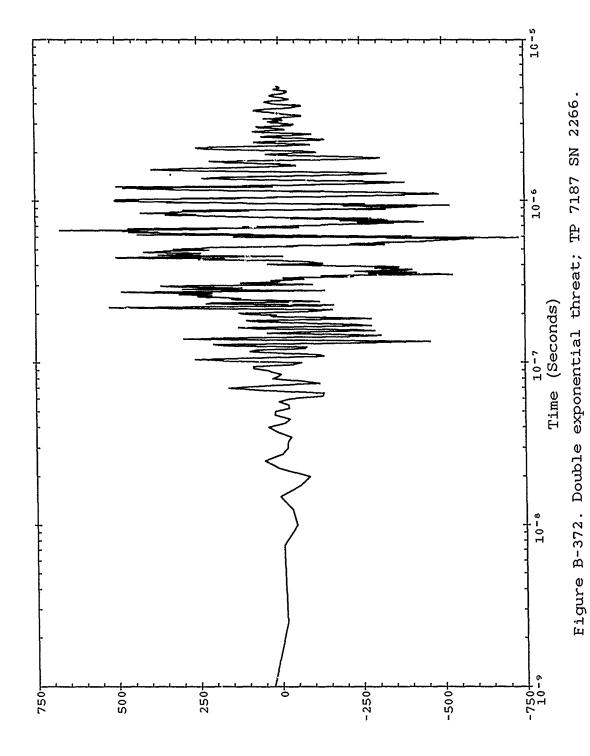




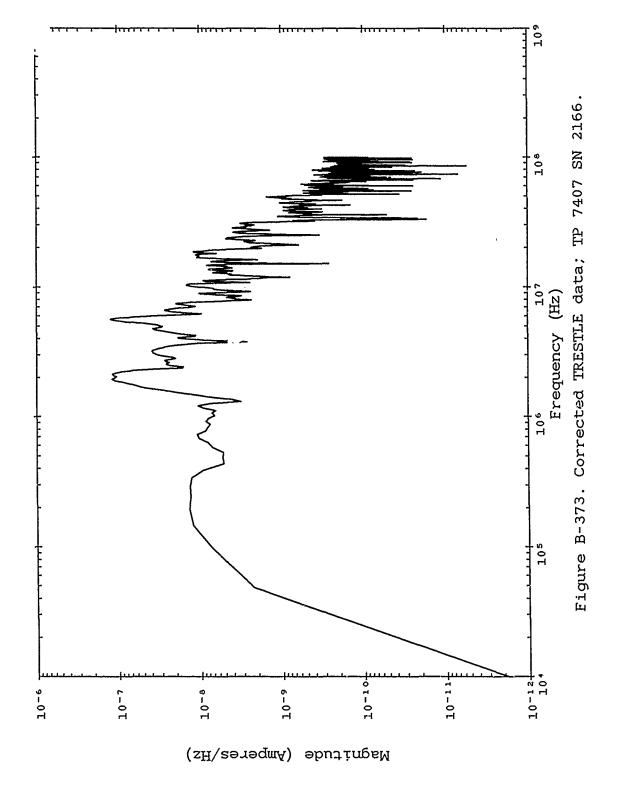


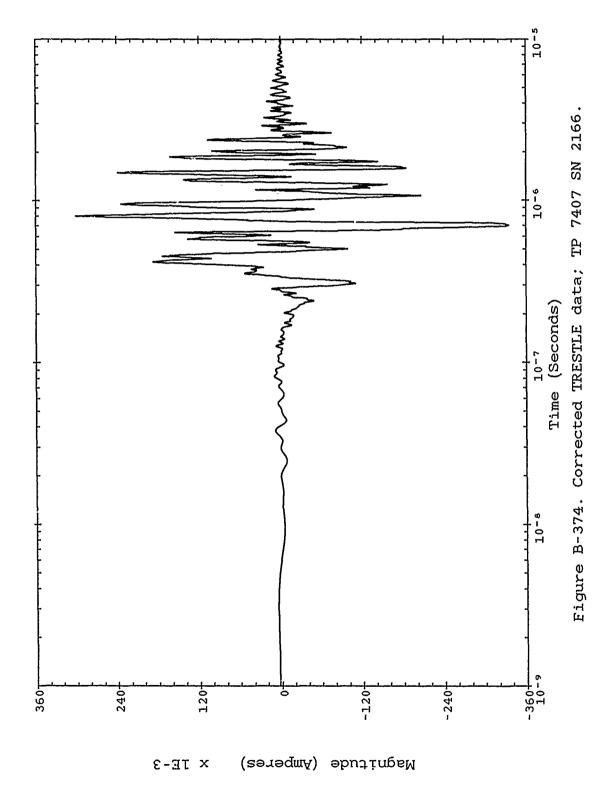
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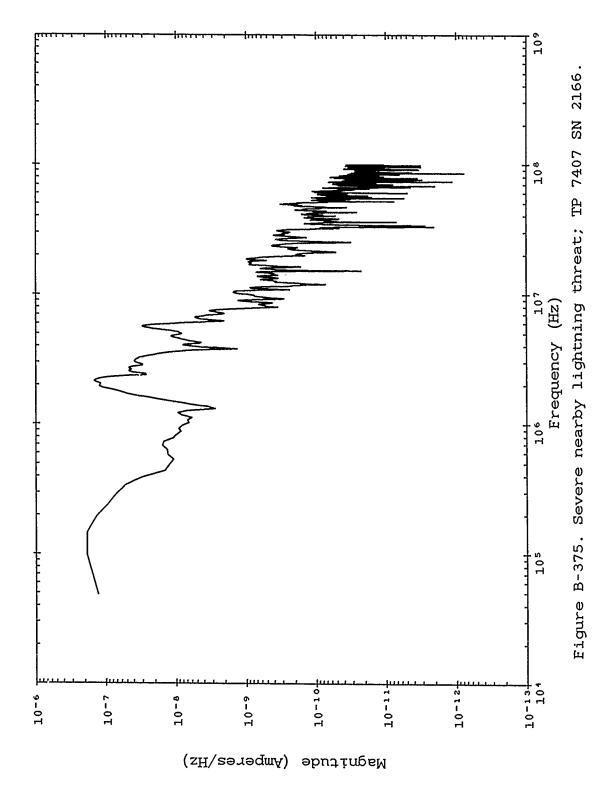


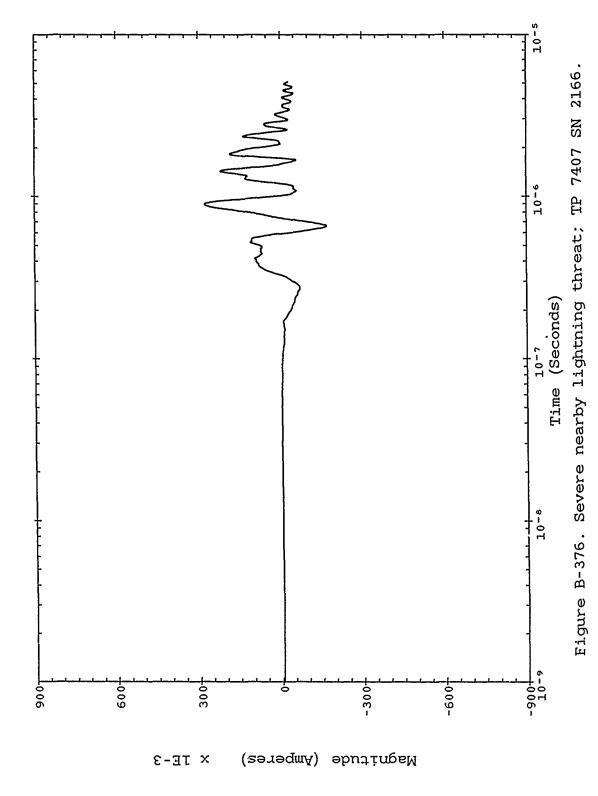


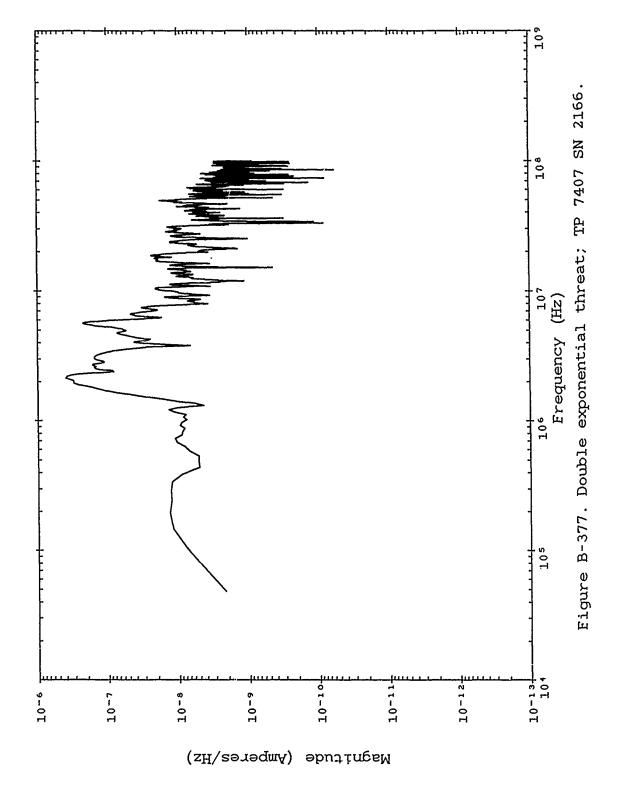
Magnitude (Amperes) x lE-3

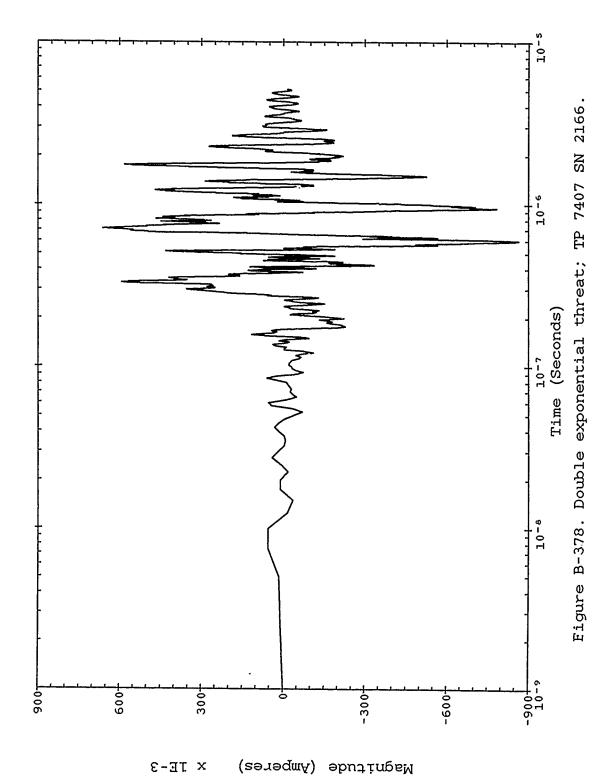


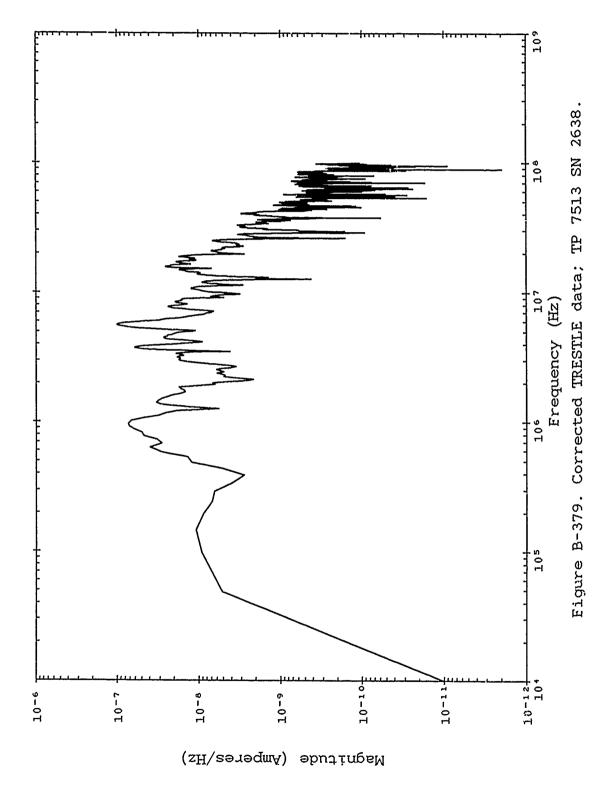


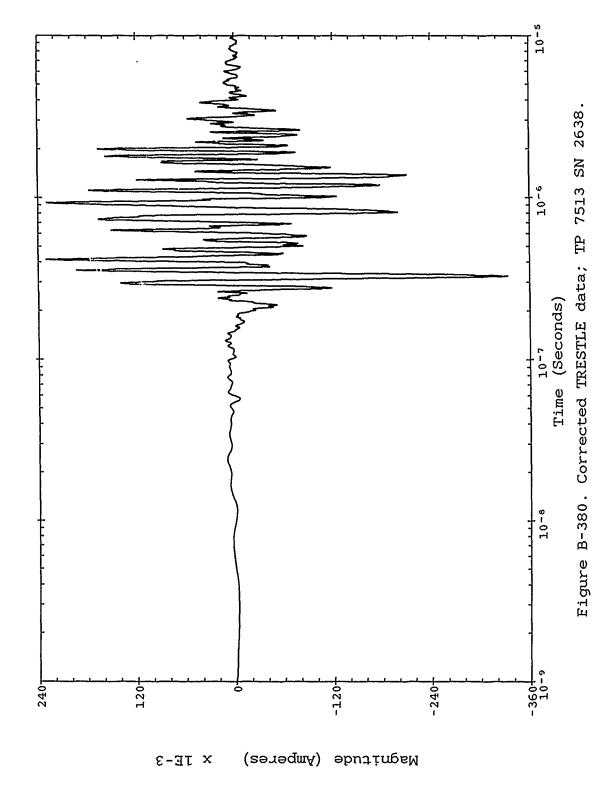


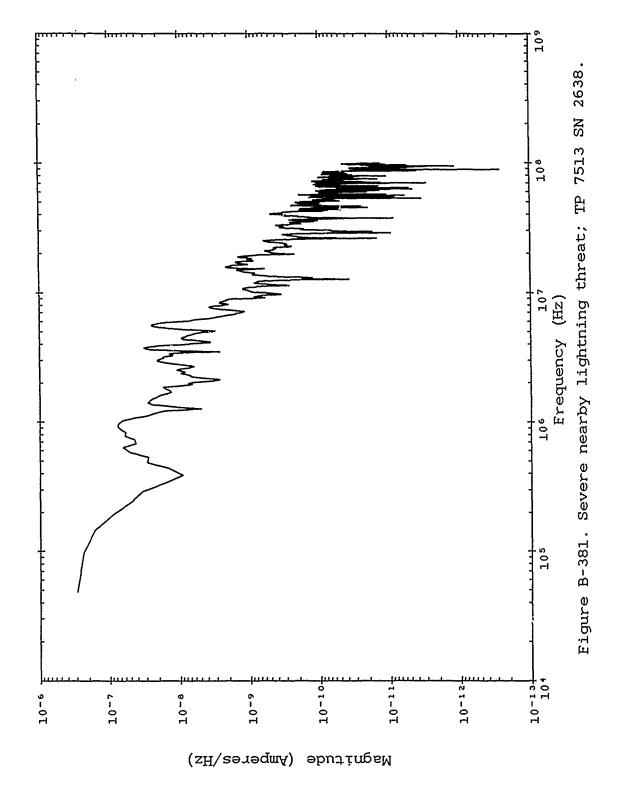


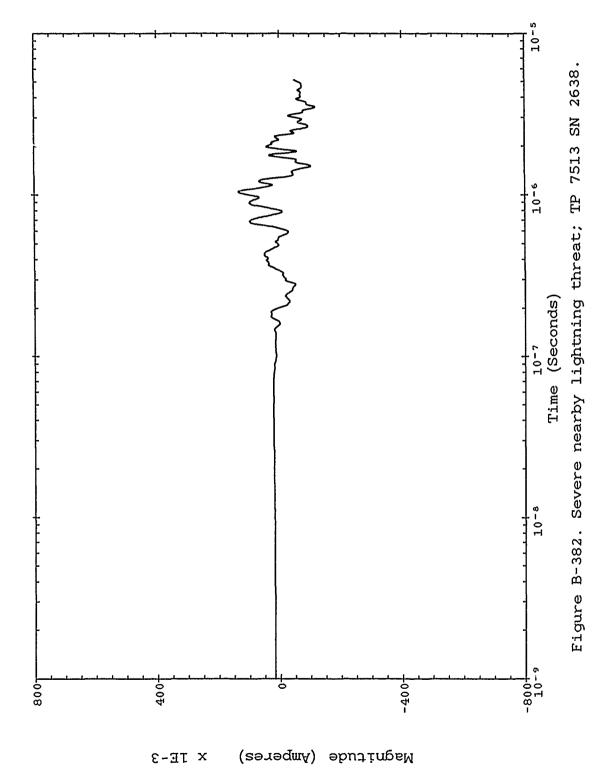


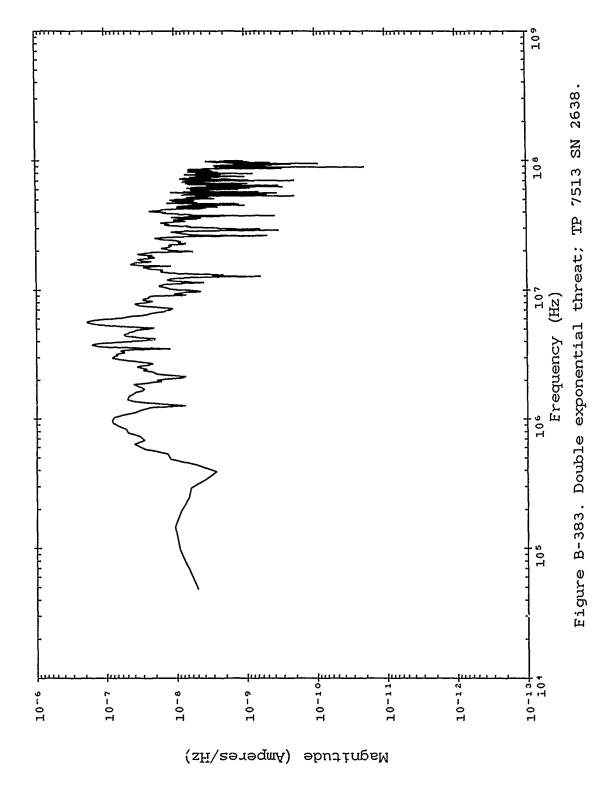


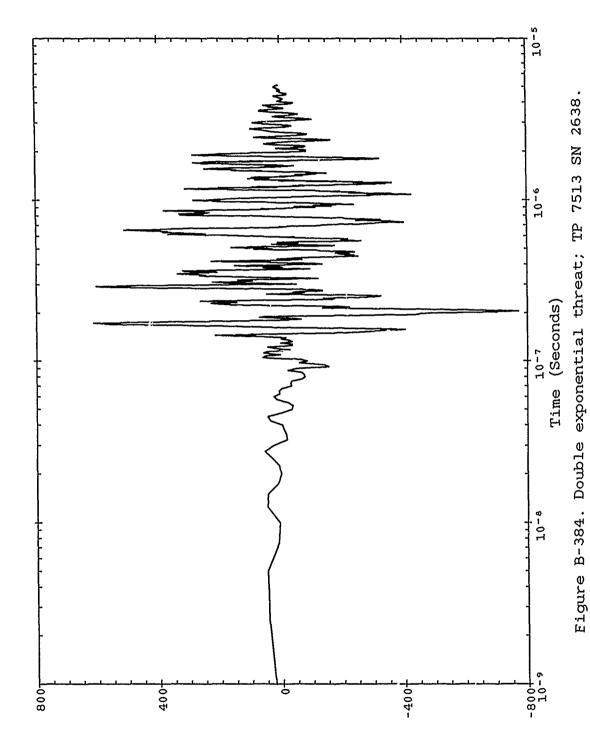




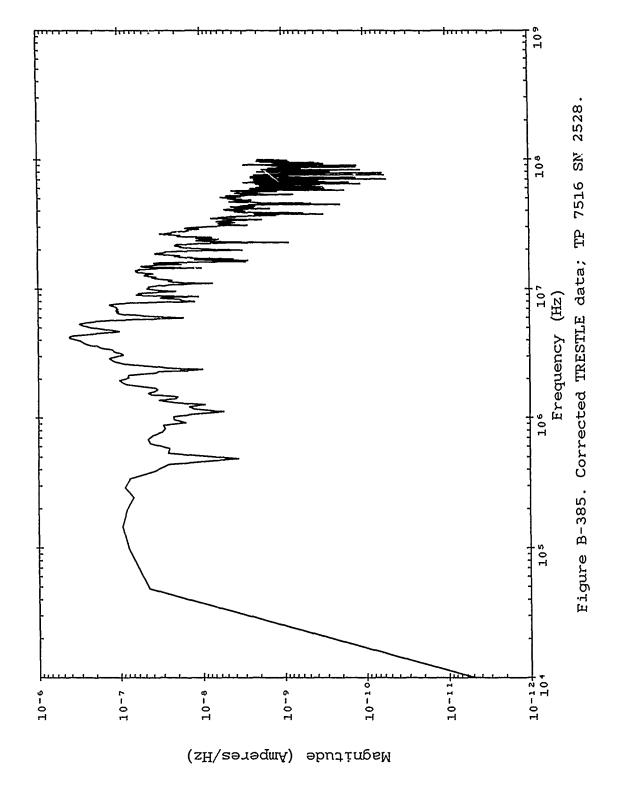


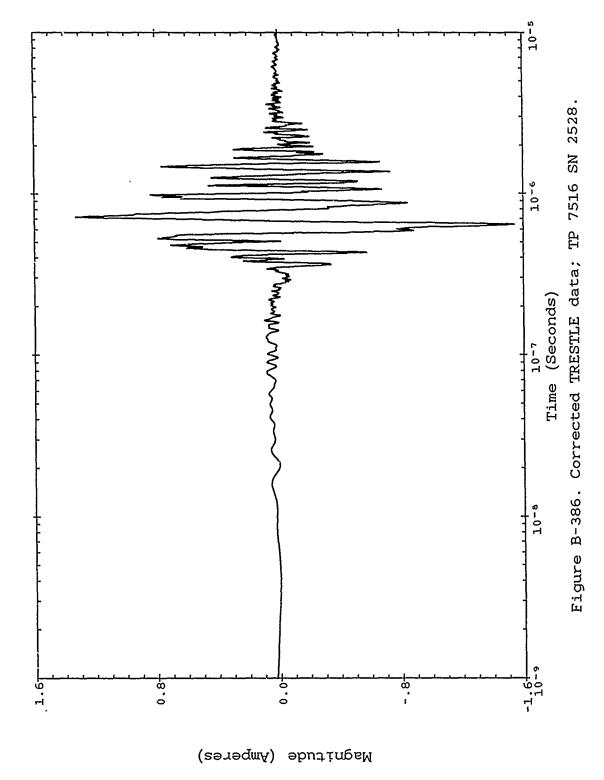


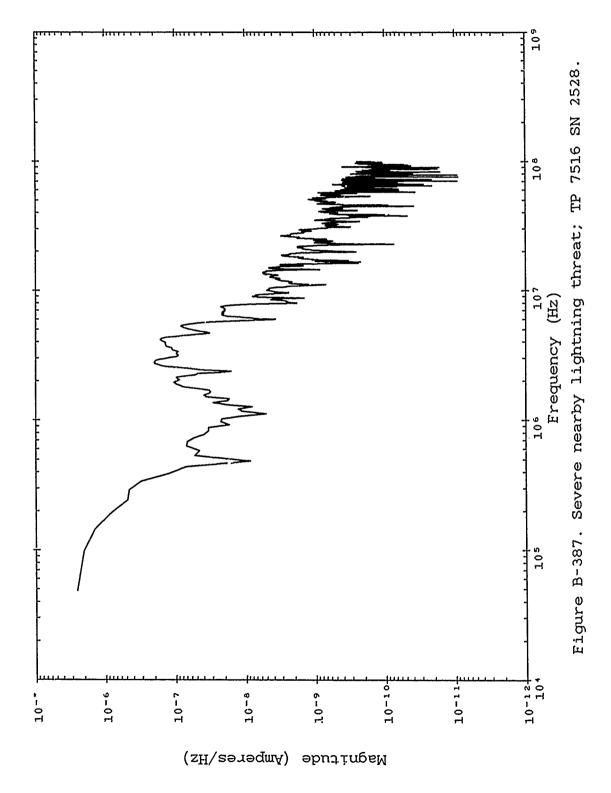


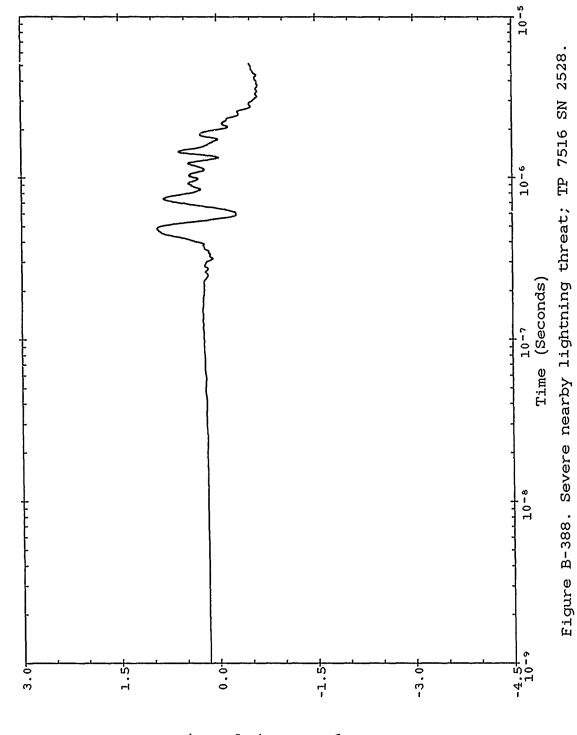


Wagnitude (Amperes) x 1E-3

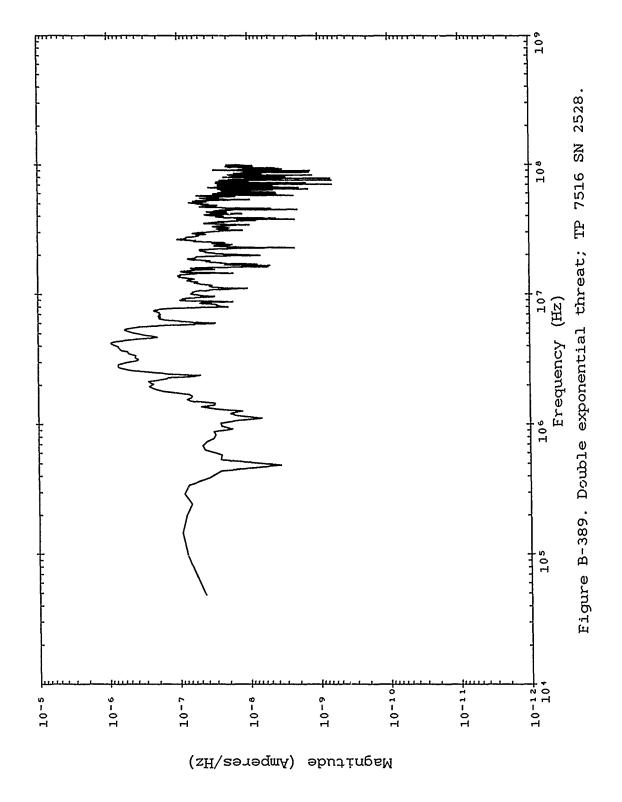


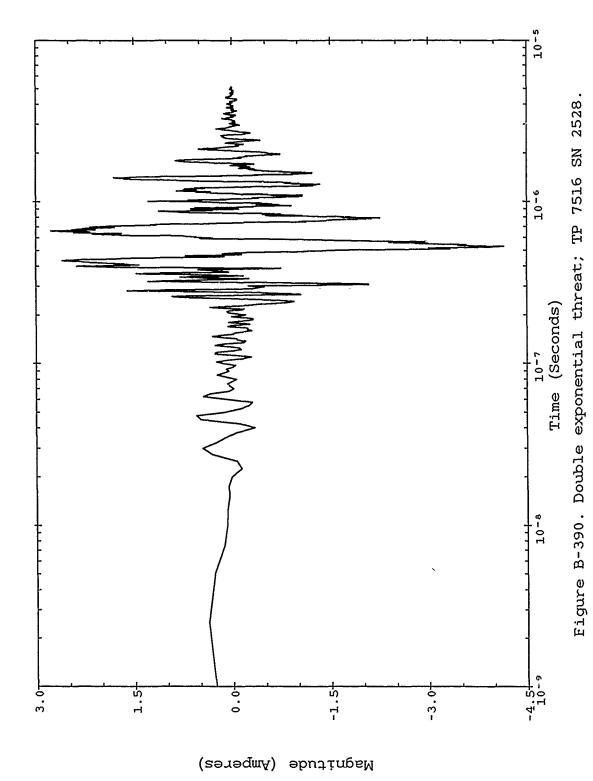


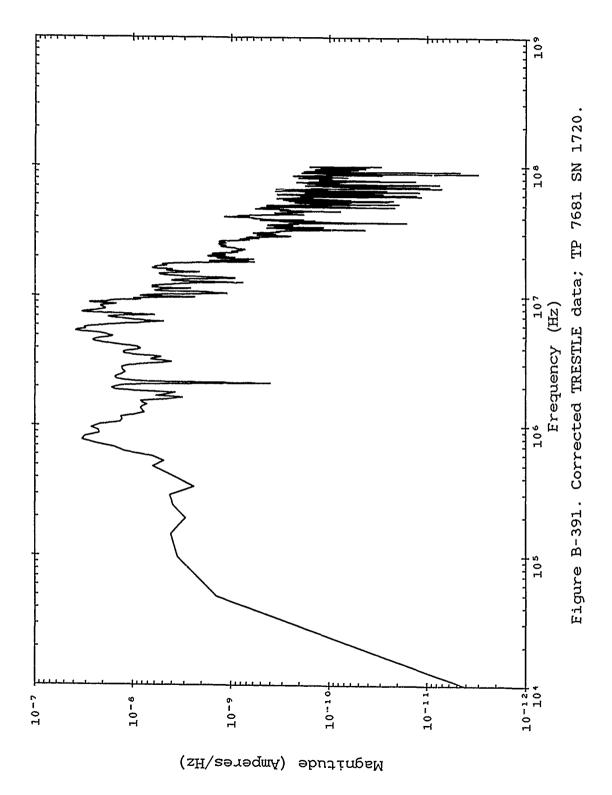


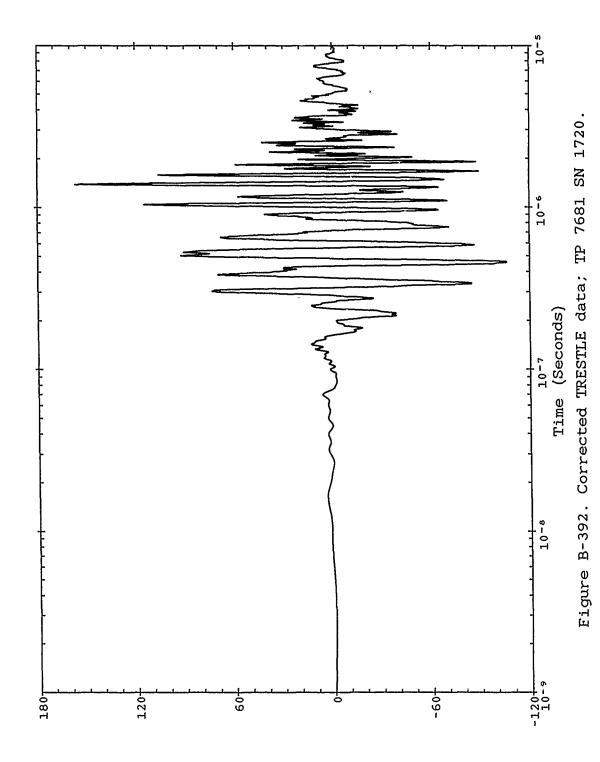


Magnitude (Amperes)

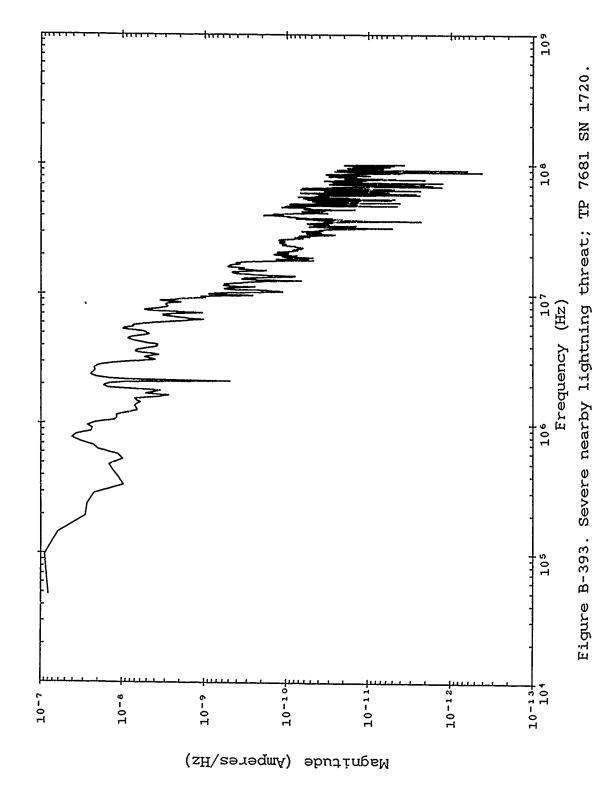


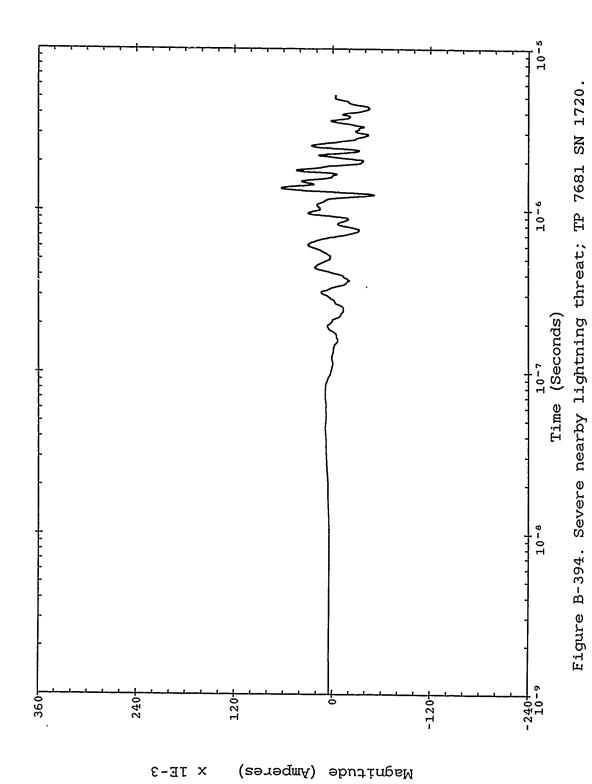


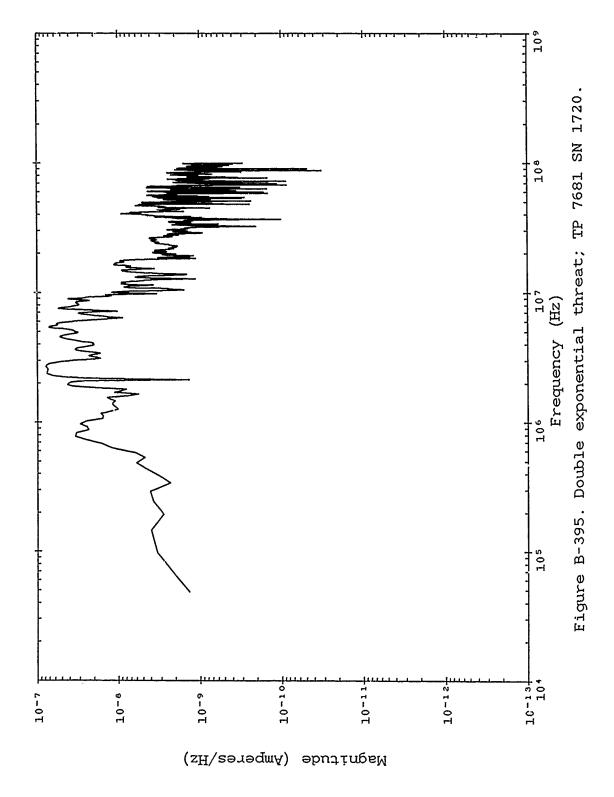


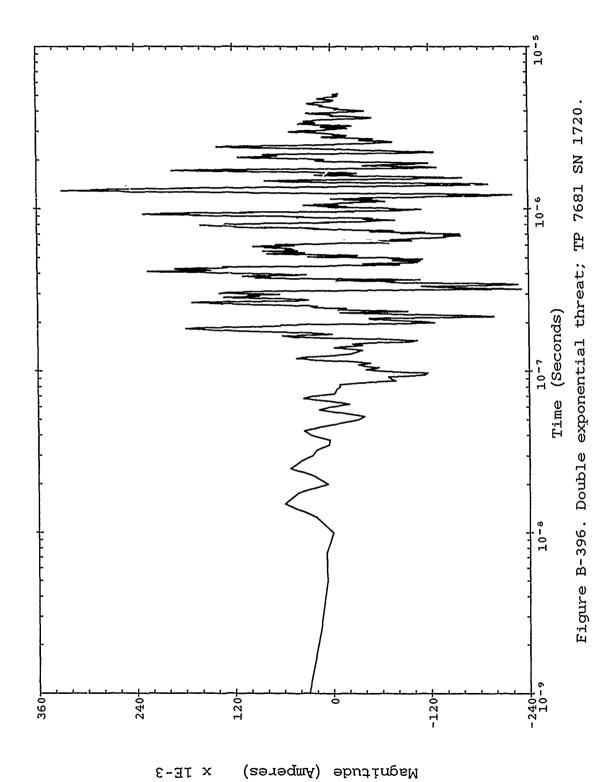


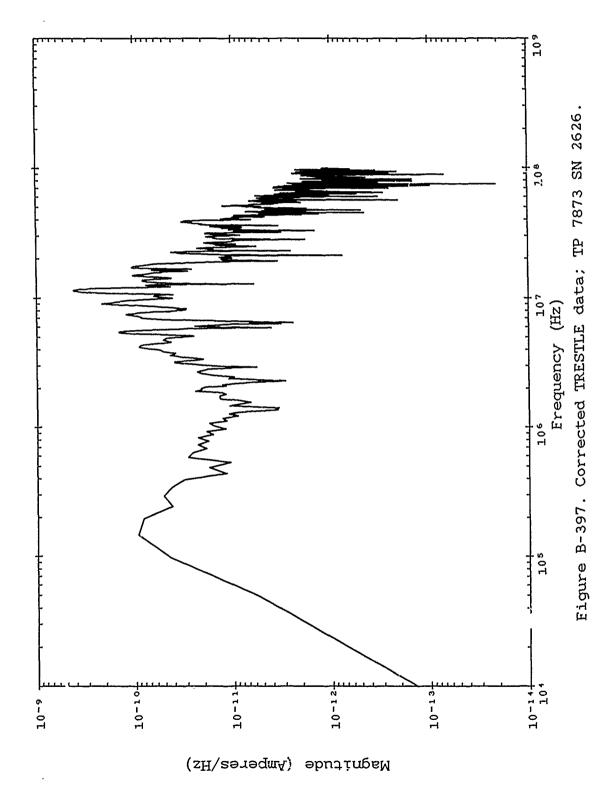
Magnitude (Amperes) x lE-3

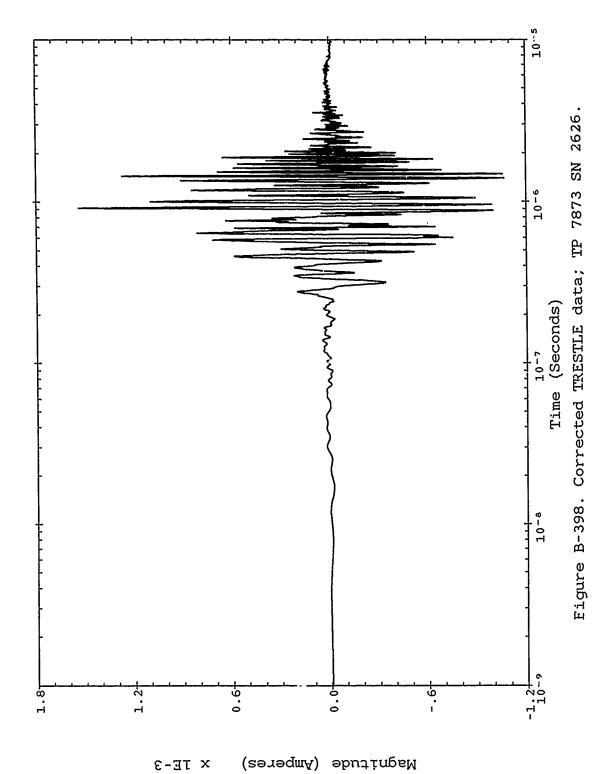


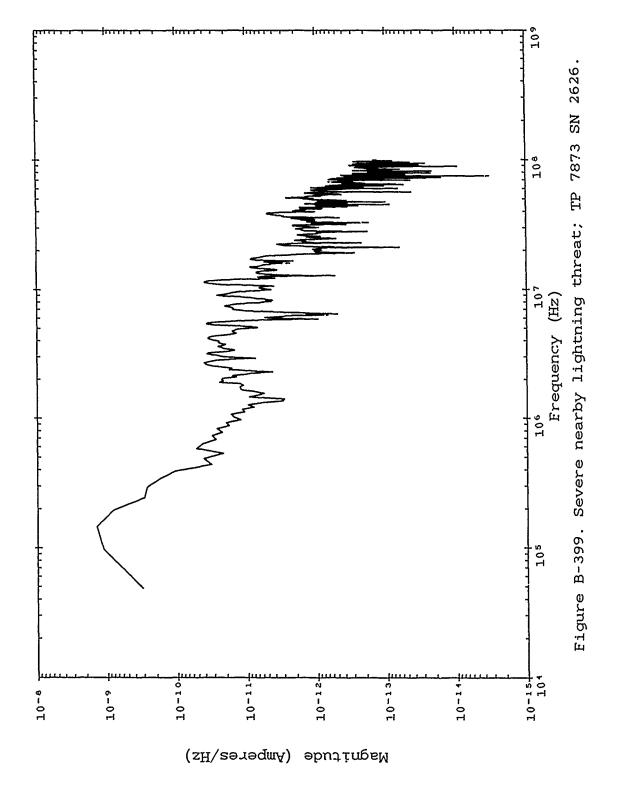


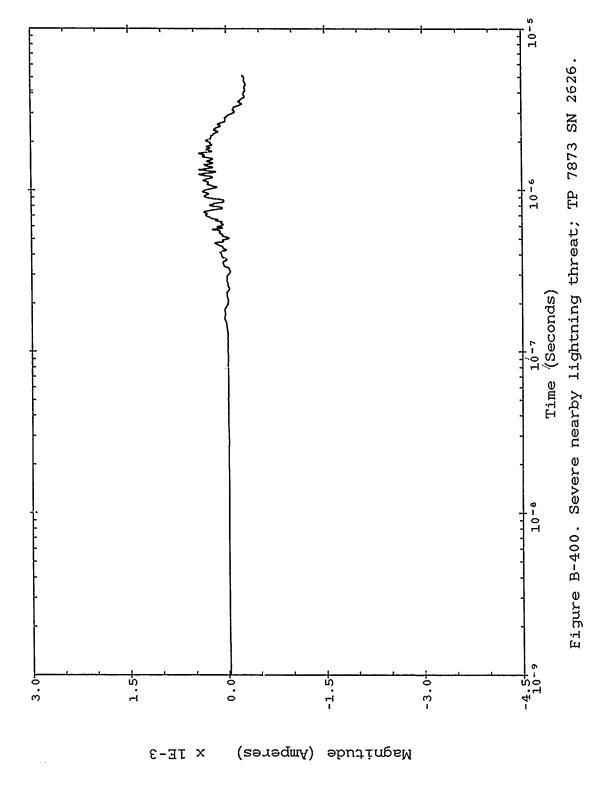


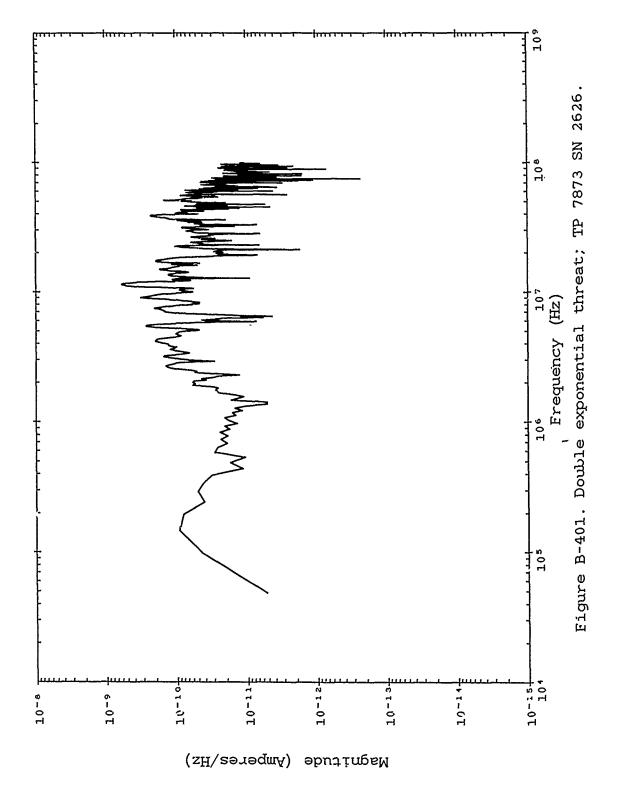


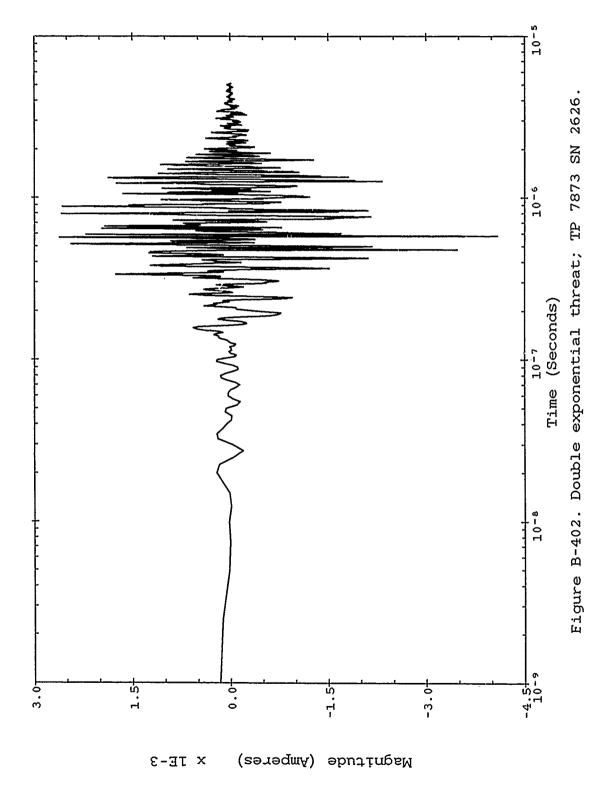


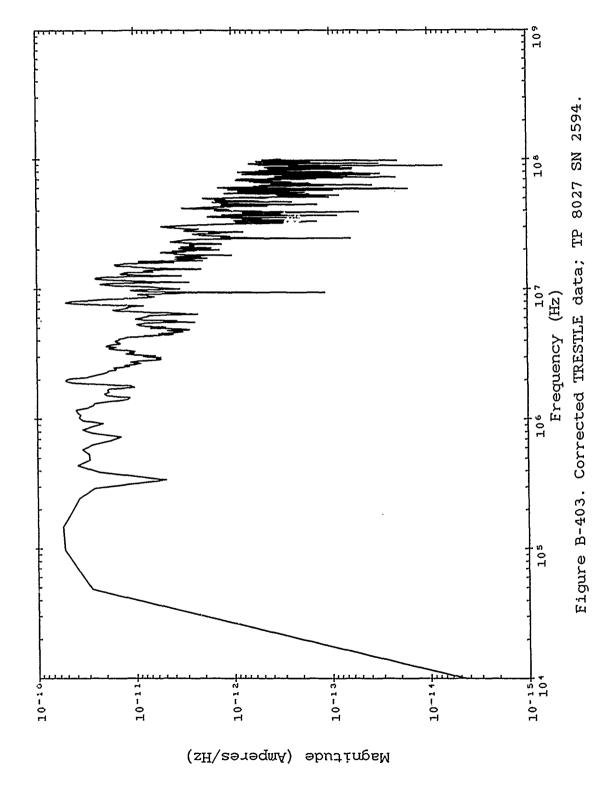


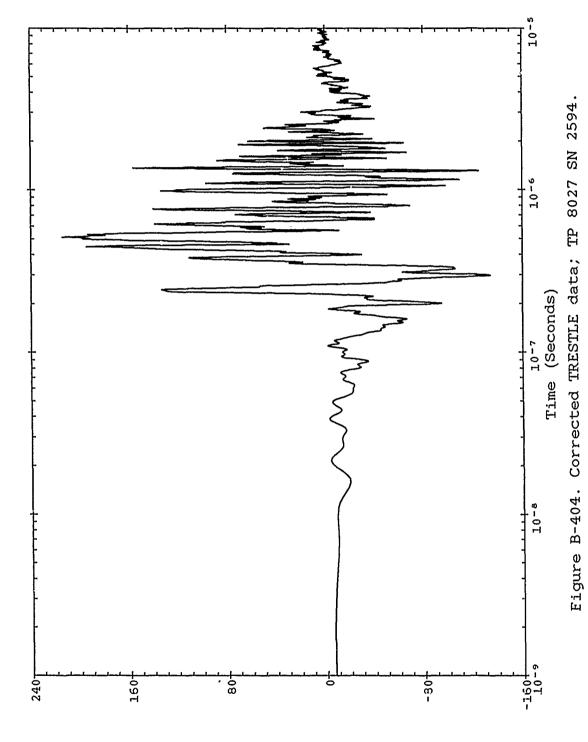




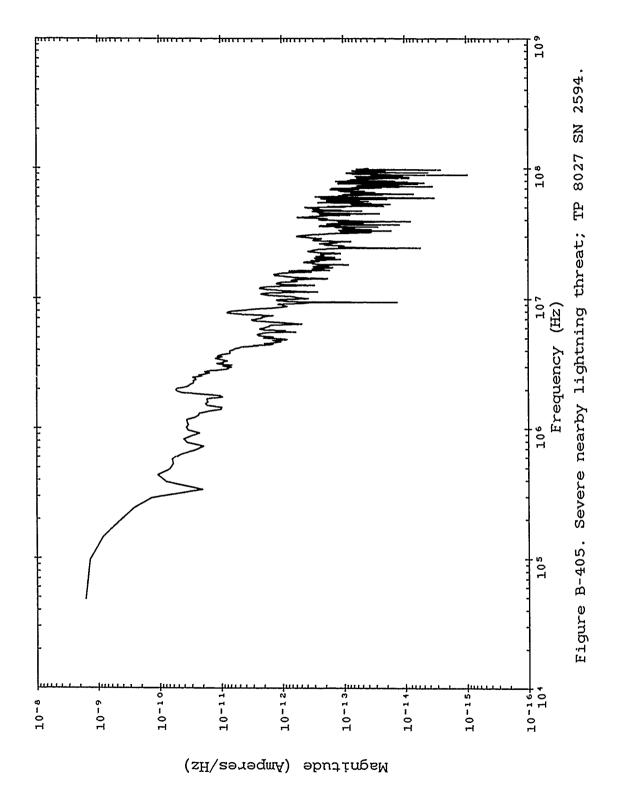








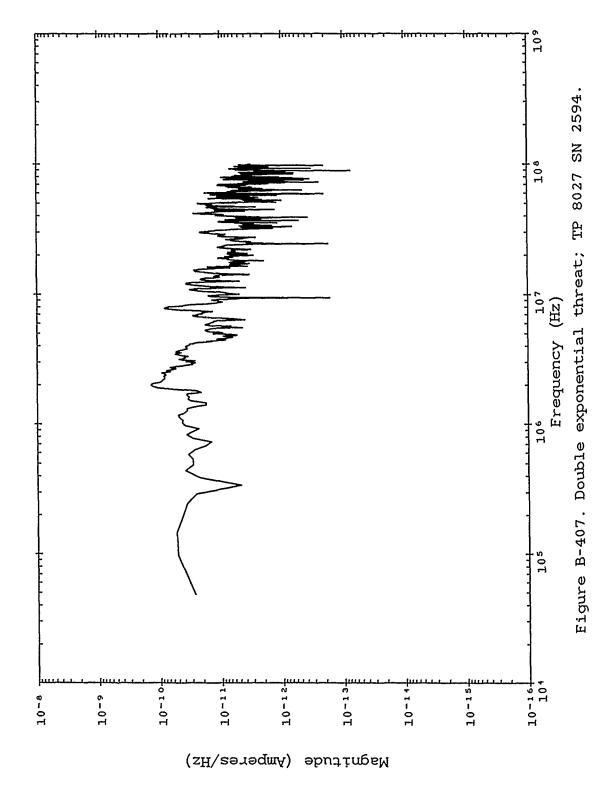
Magnitude (Amperes) x lE-6

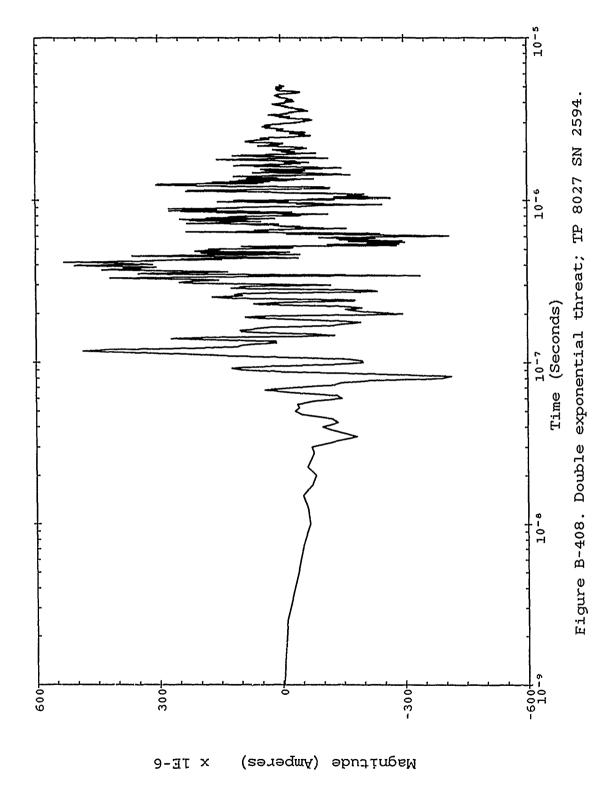


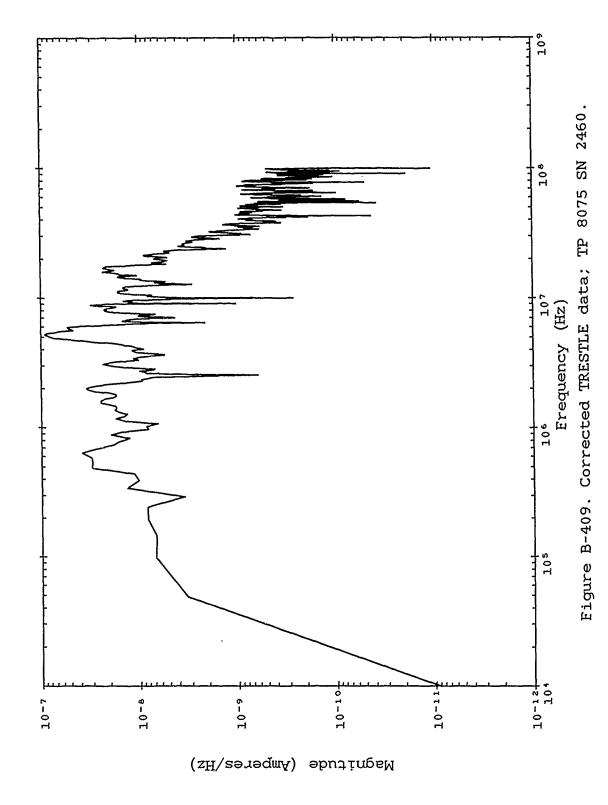
437

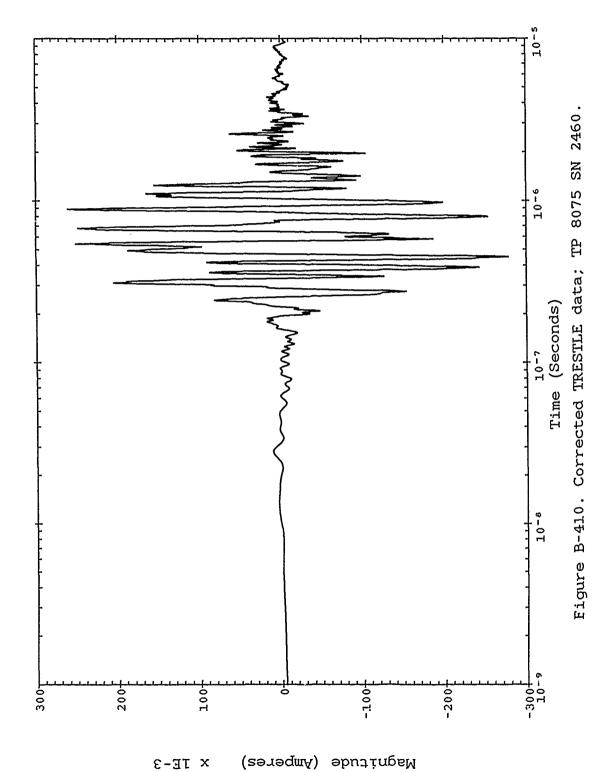
Magnitude (Amperes)

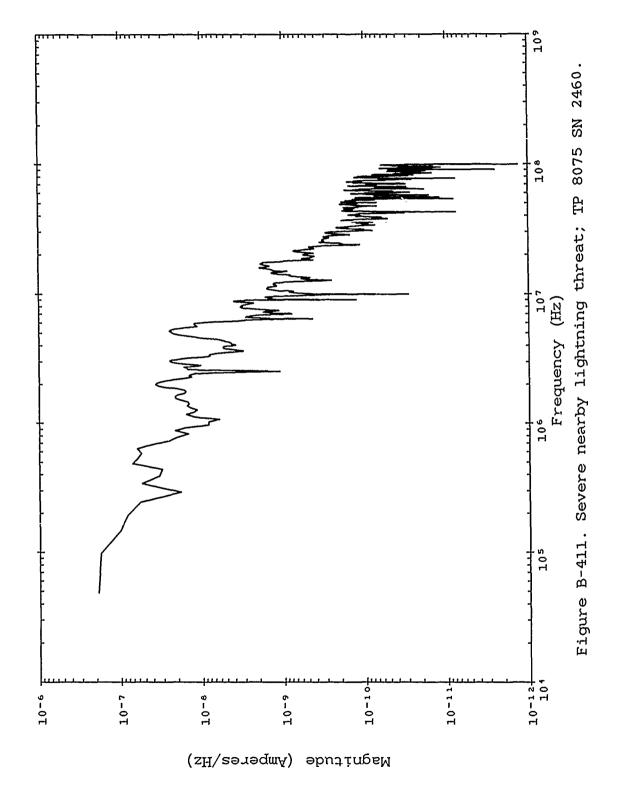
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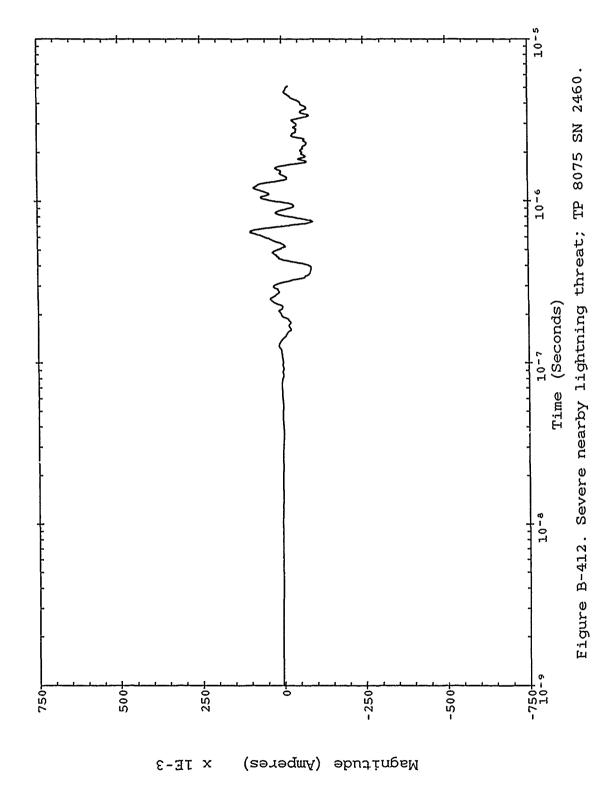


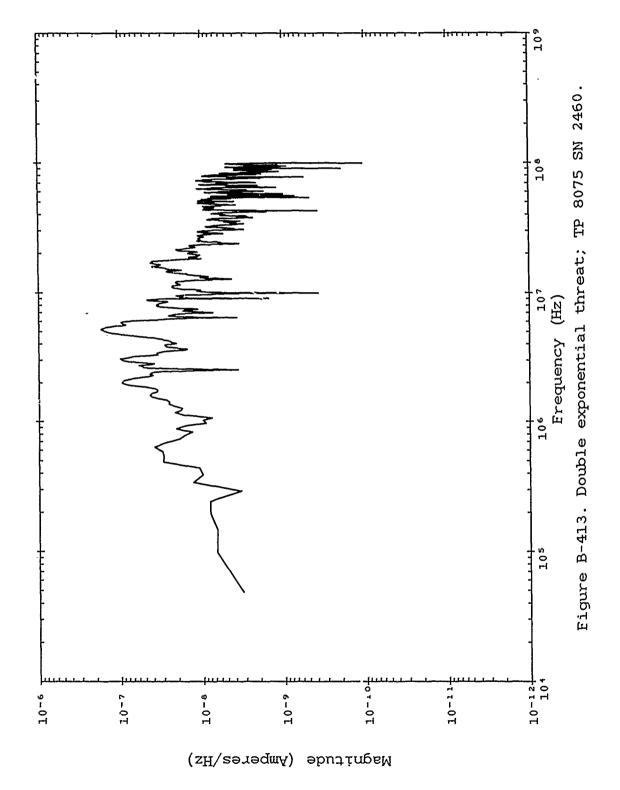


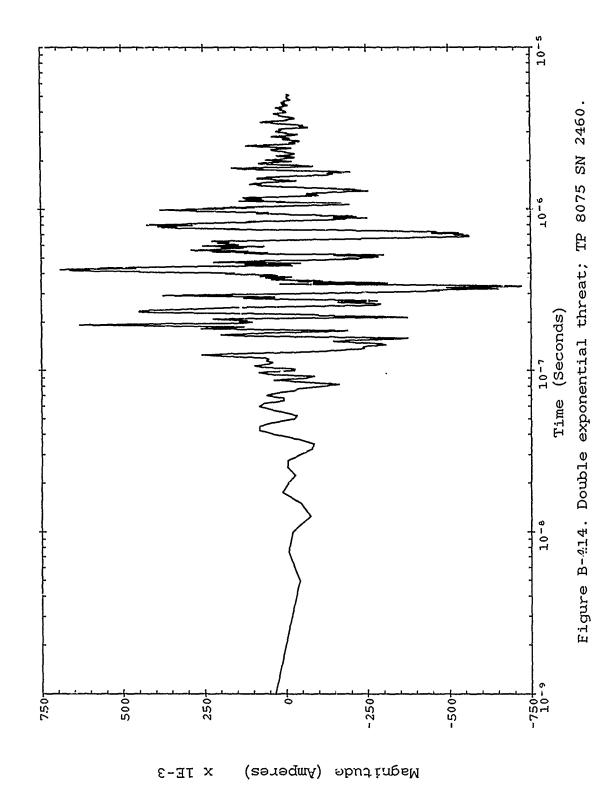


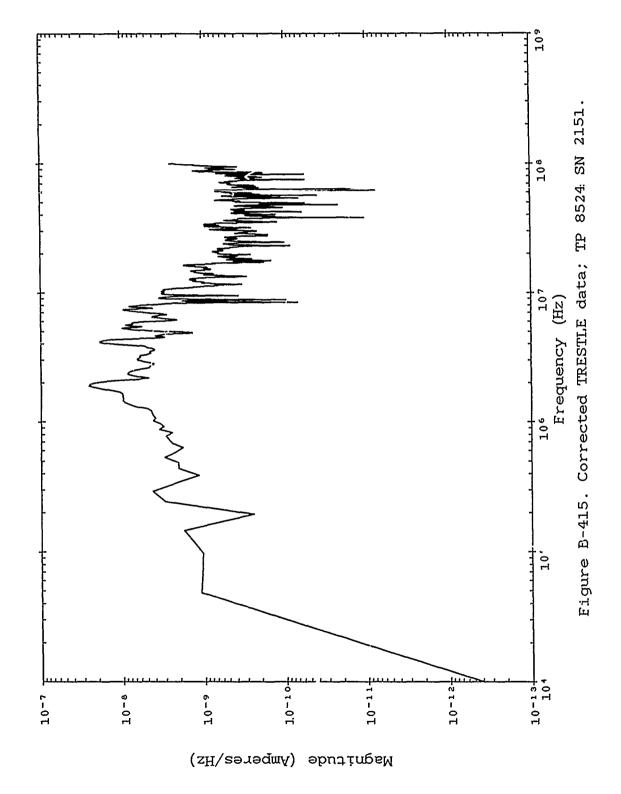


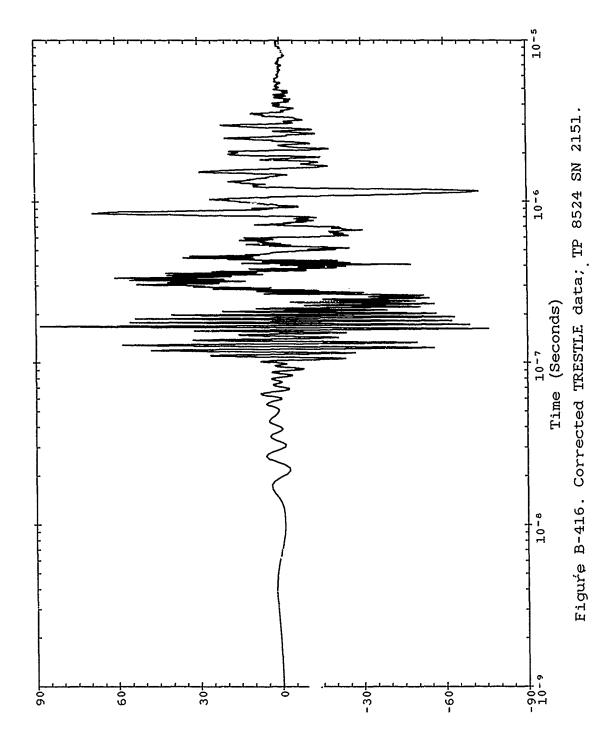






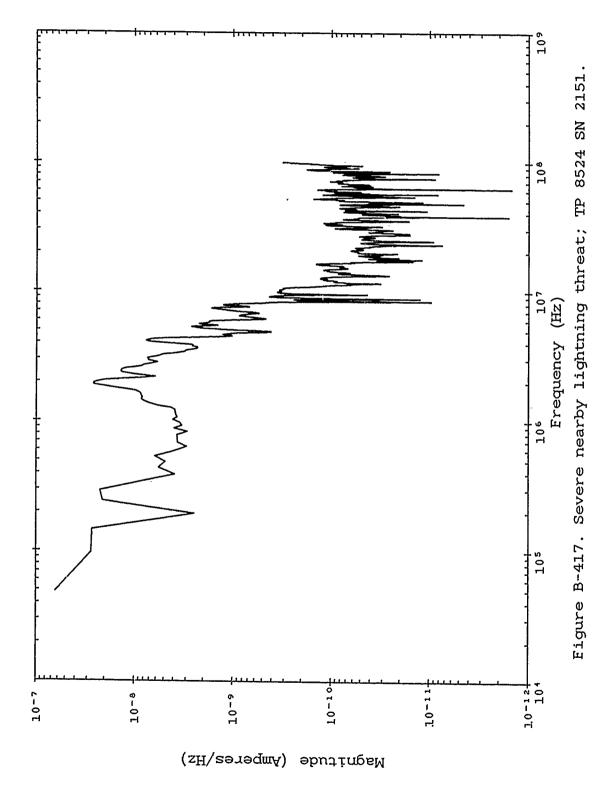






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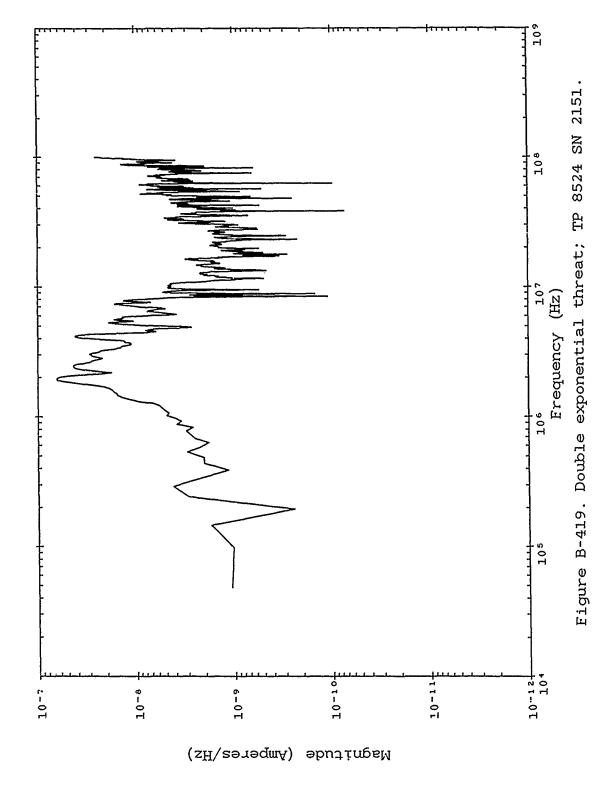
Magnitude (Amperes) x lE-3

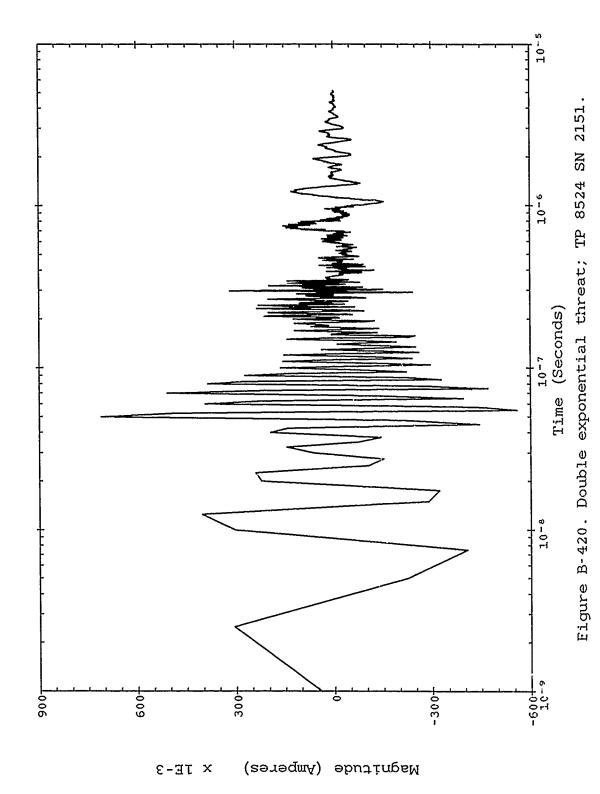


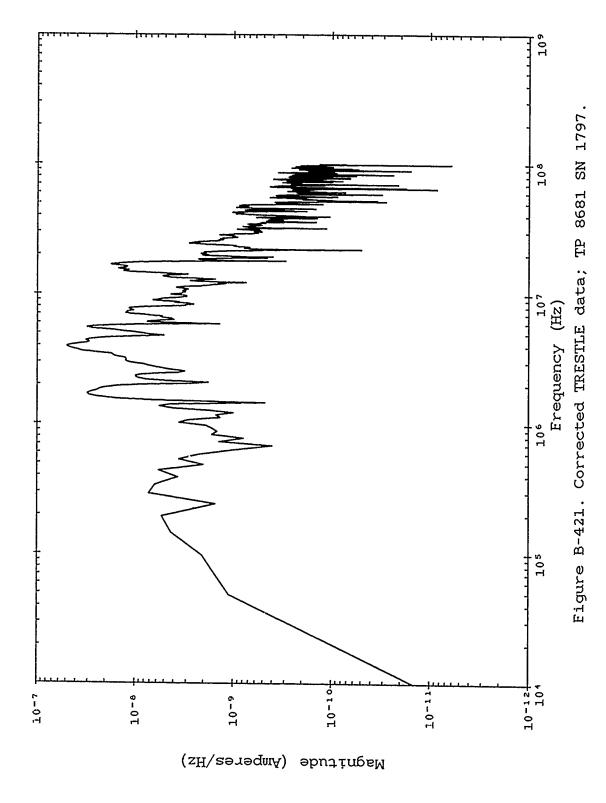
449

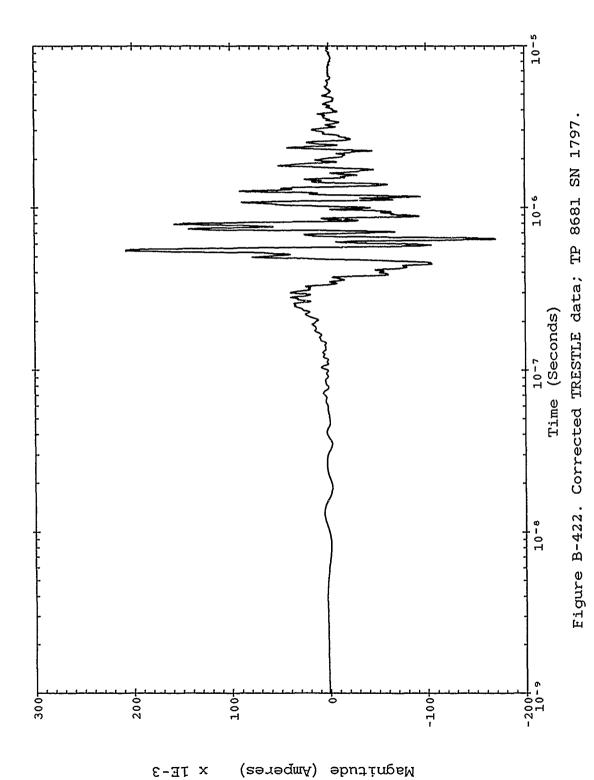
Magnitude (Amperes)

x TE-3

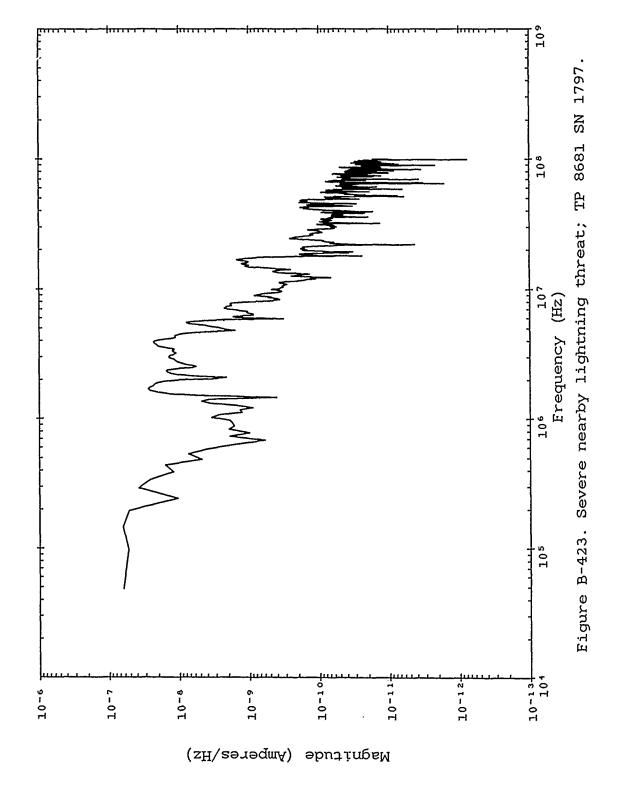


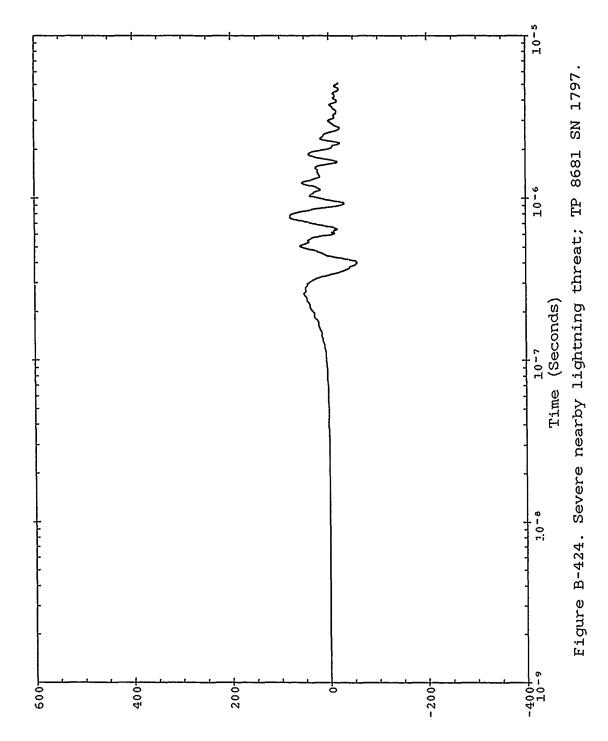






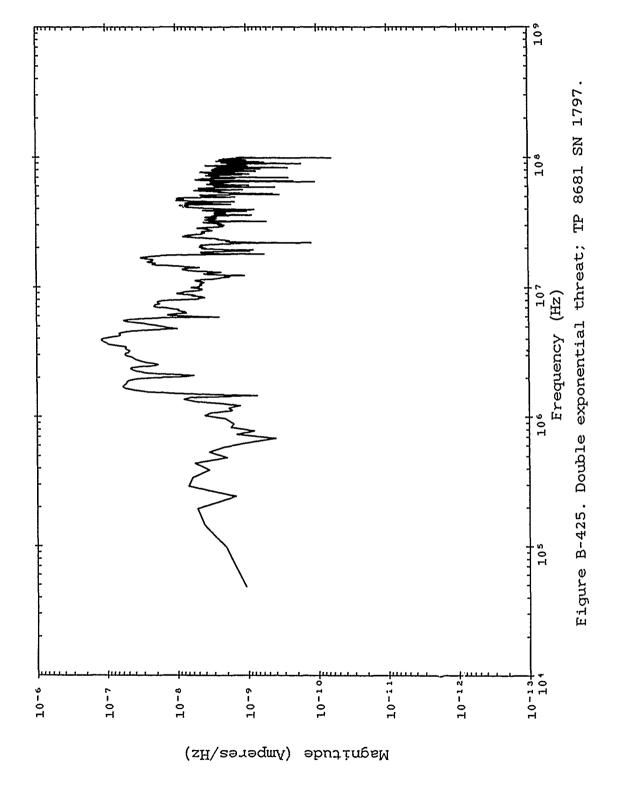
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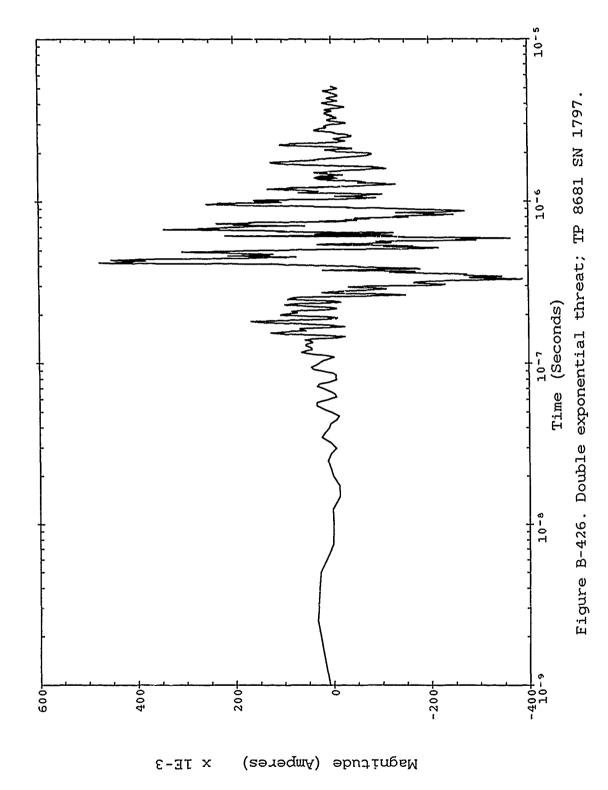


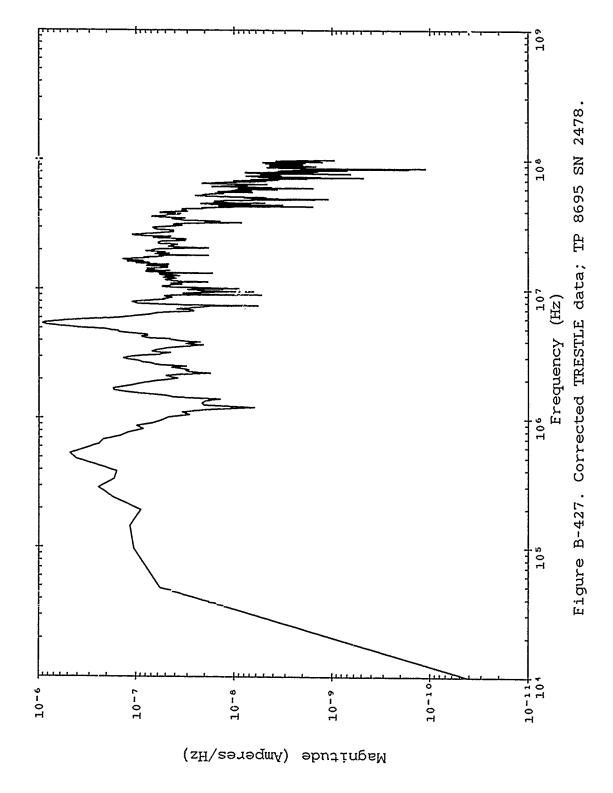


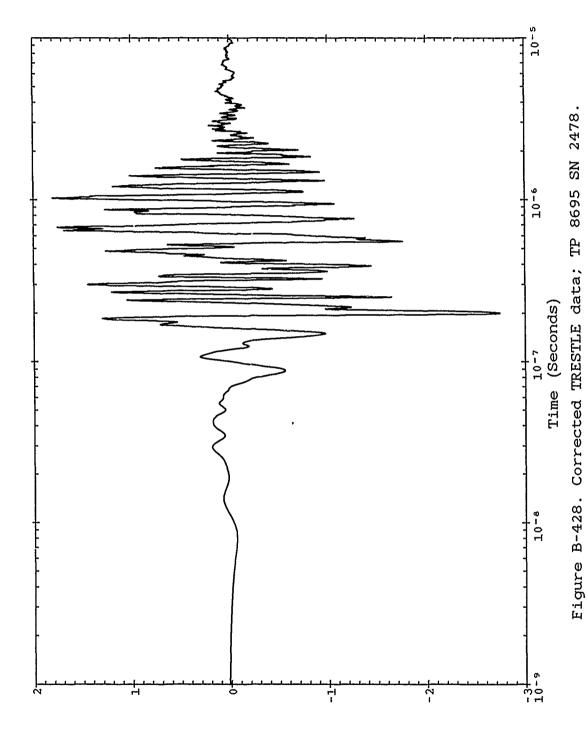
Magnitude (Amperes)

x IE-3

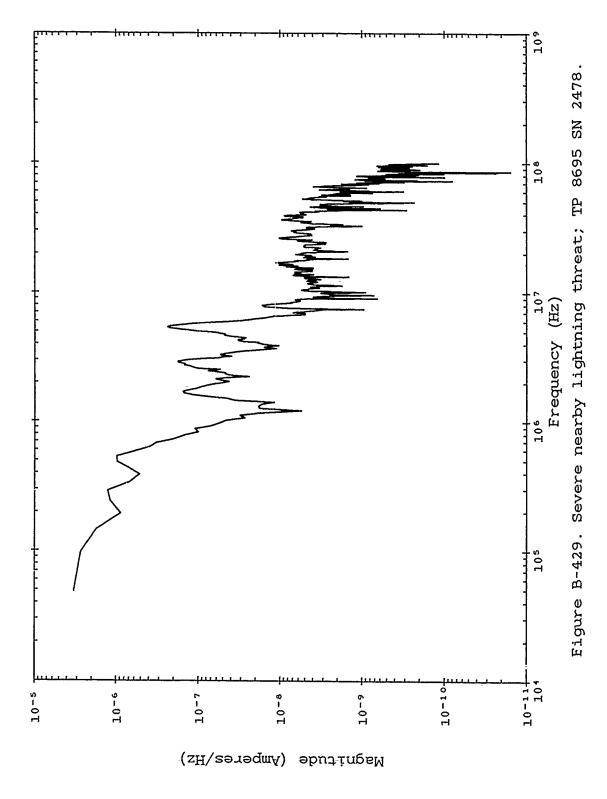


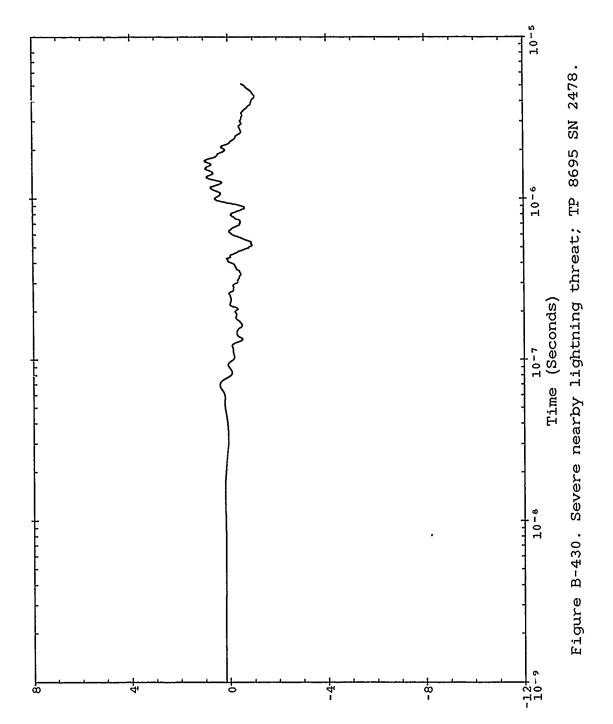




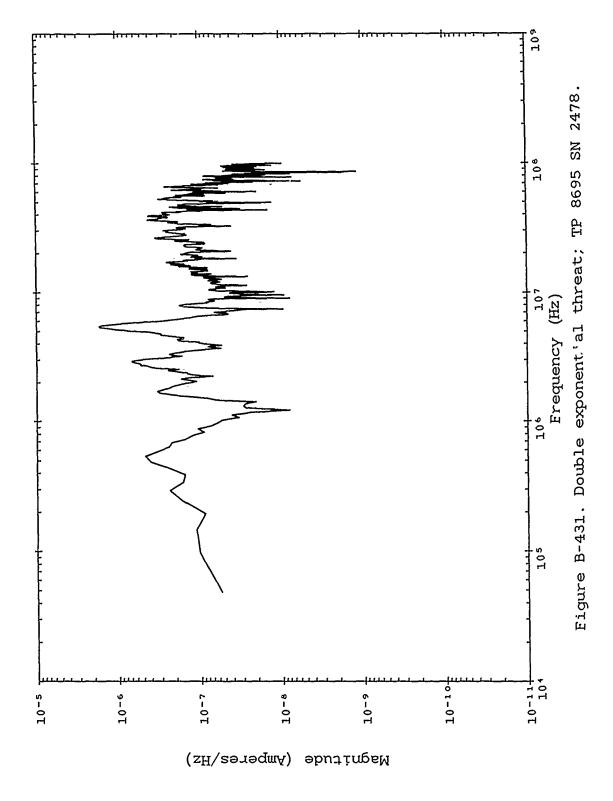


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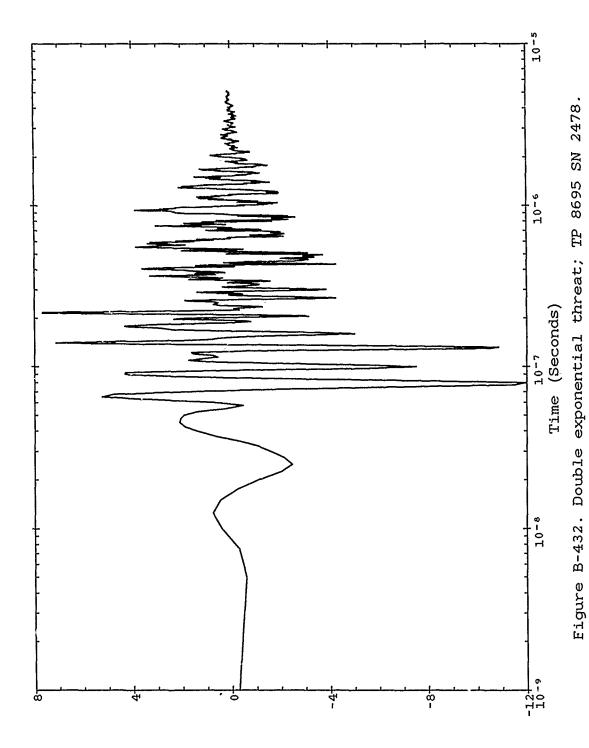


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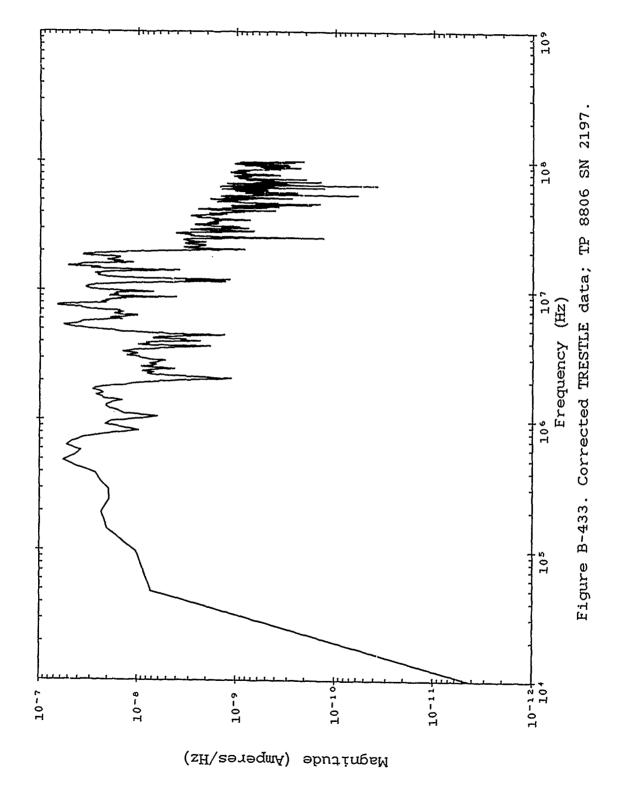


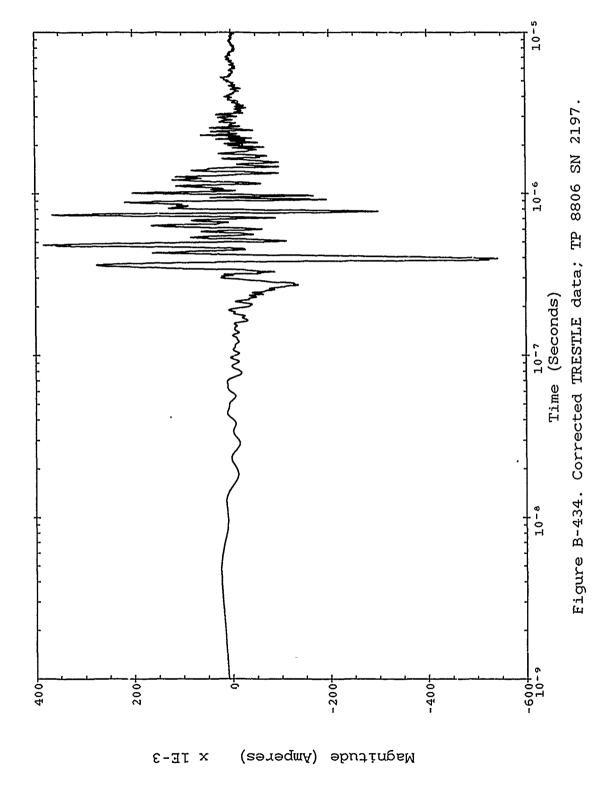
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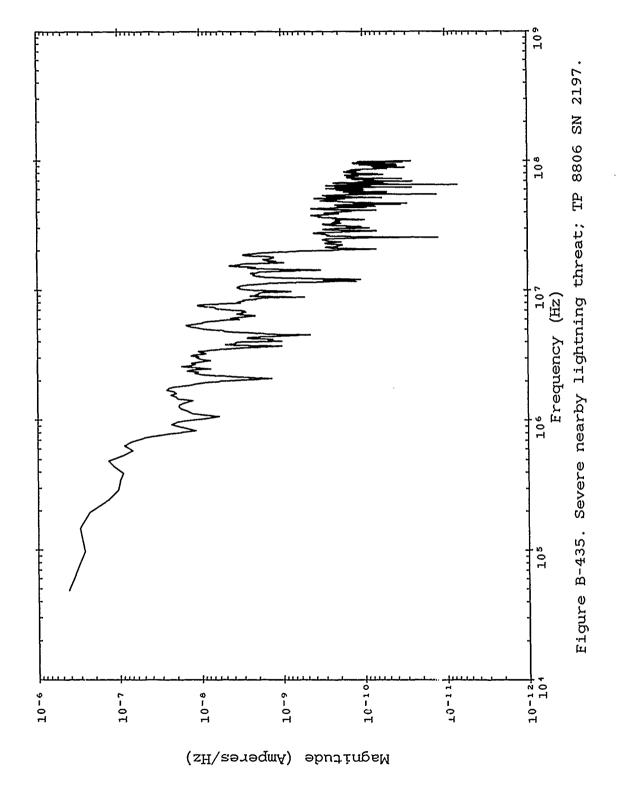
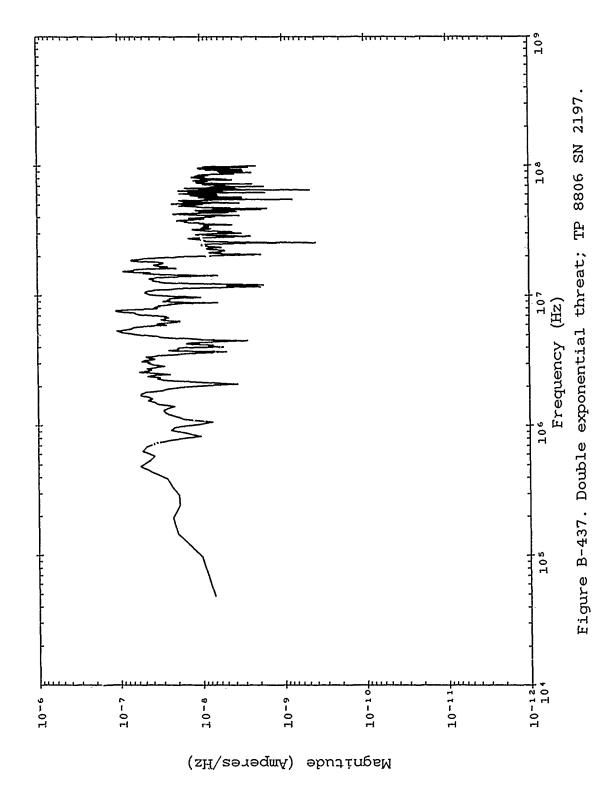
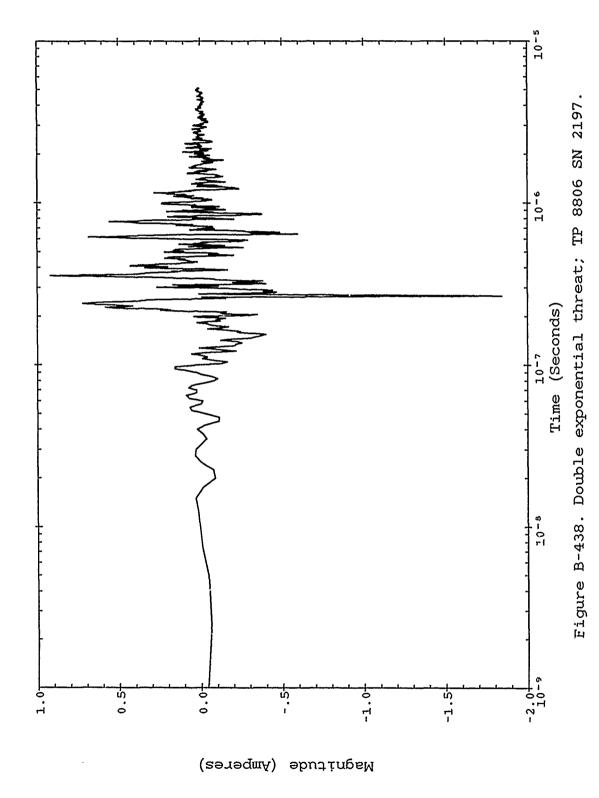


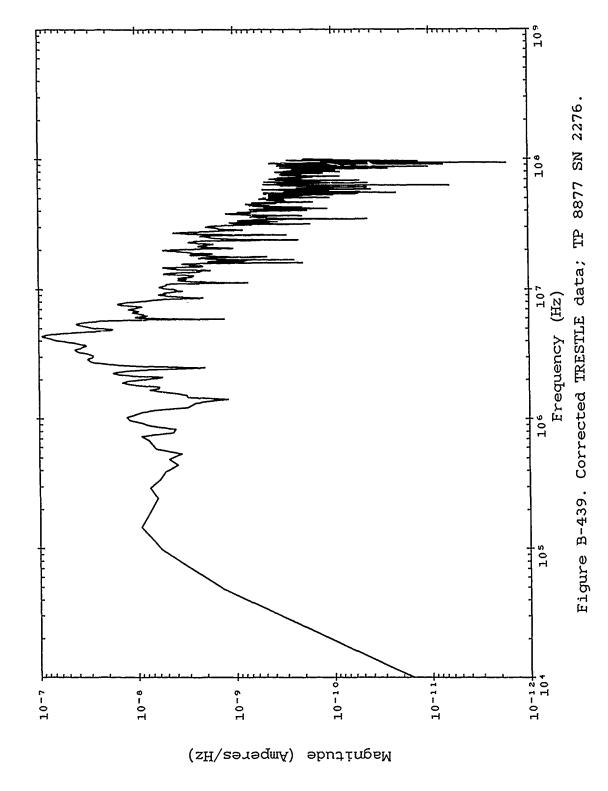
Figure B-436. Severe nearby lightning threat; TP 8806 SN 2197.

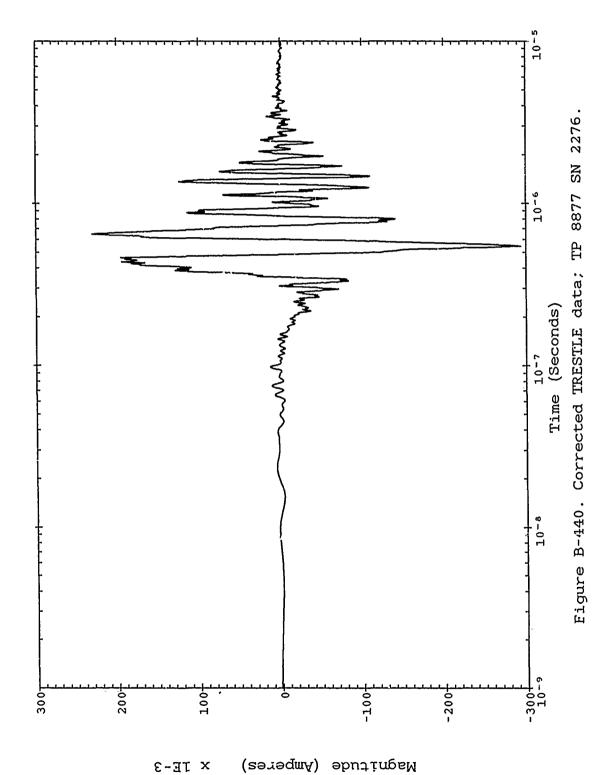
467

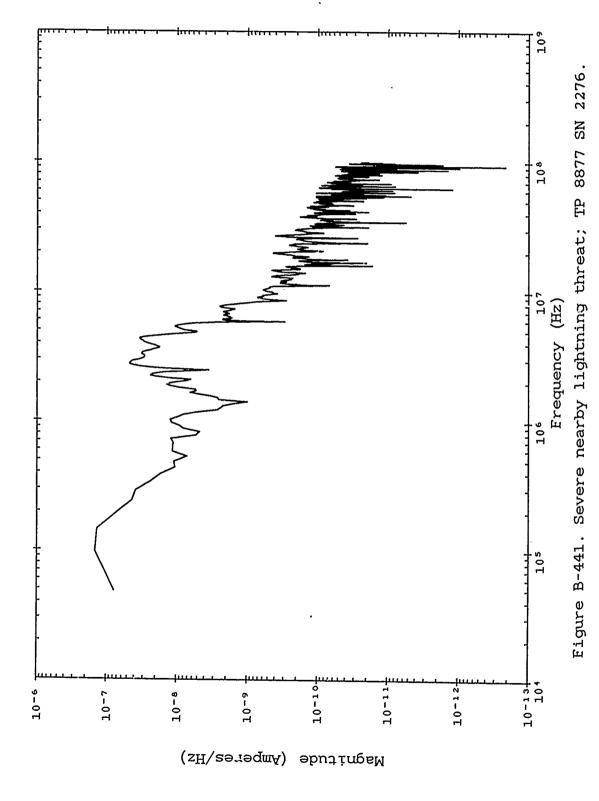
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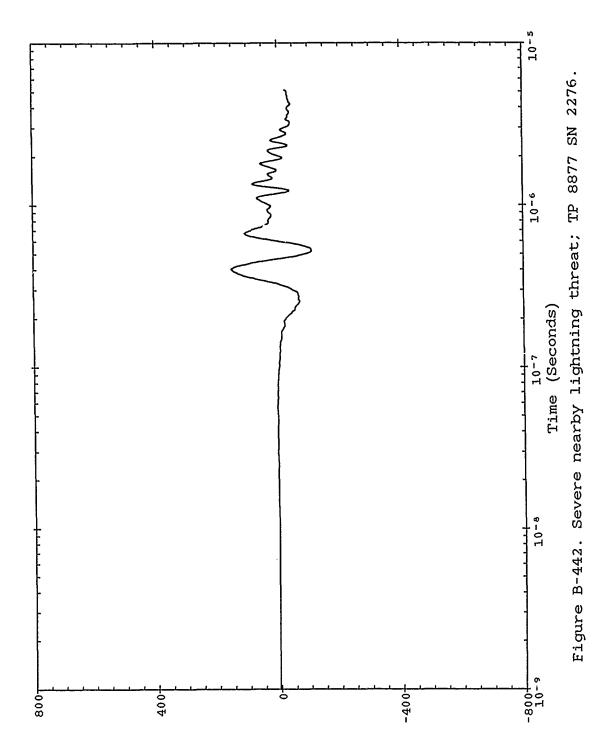








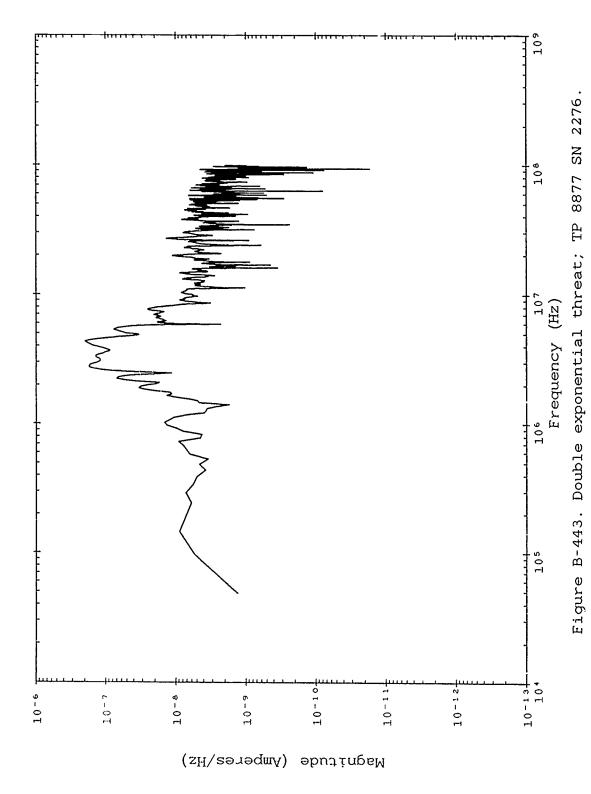


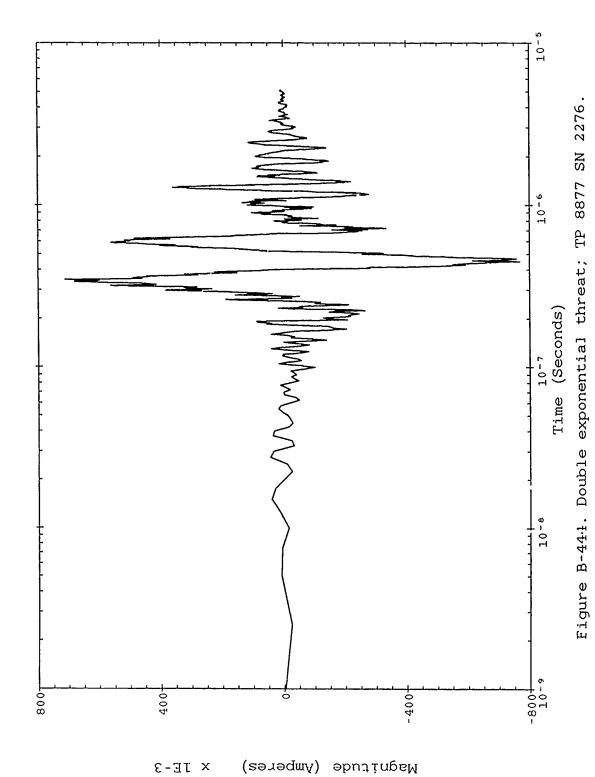


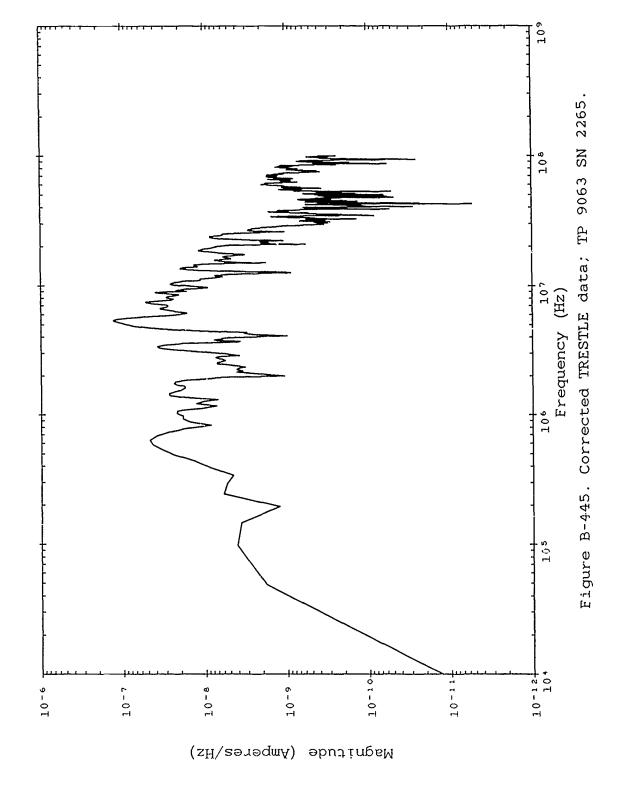
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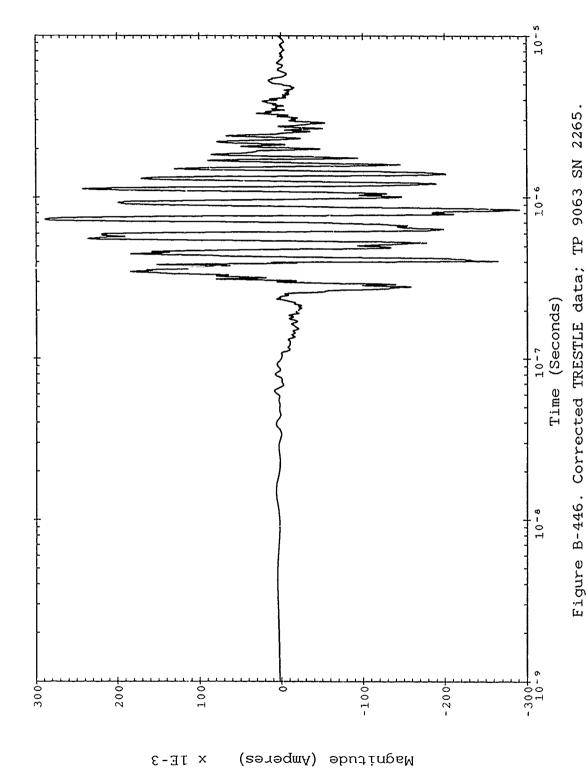
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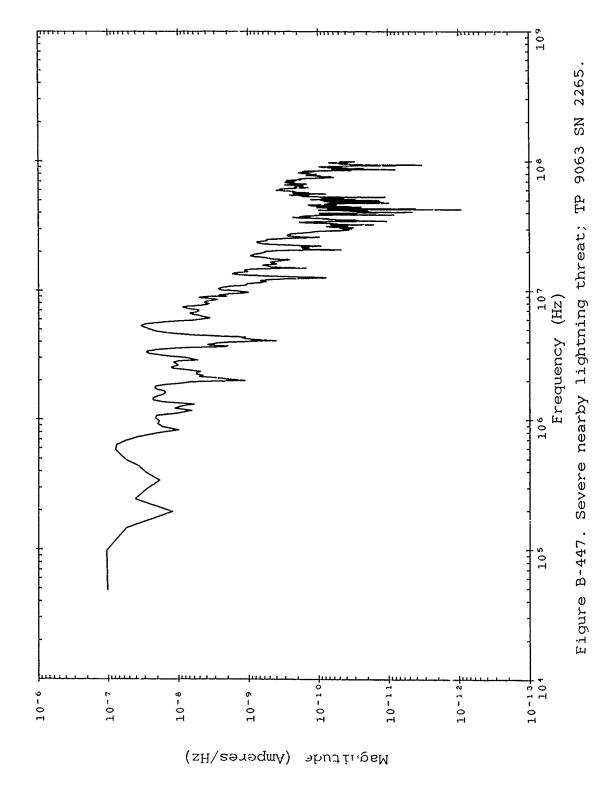
x JE-3





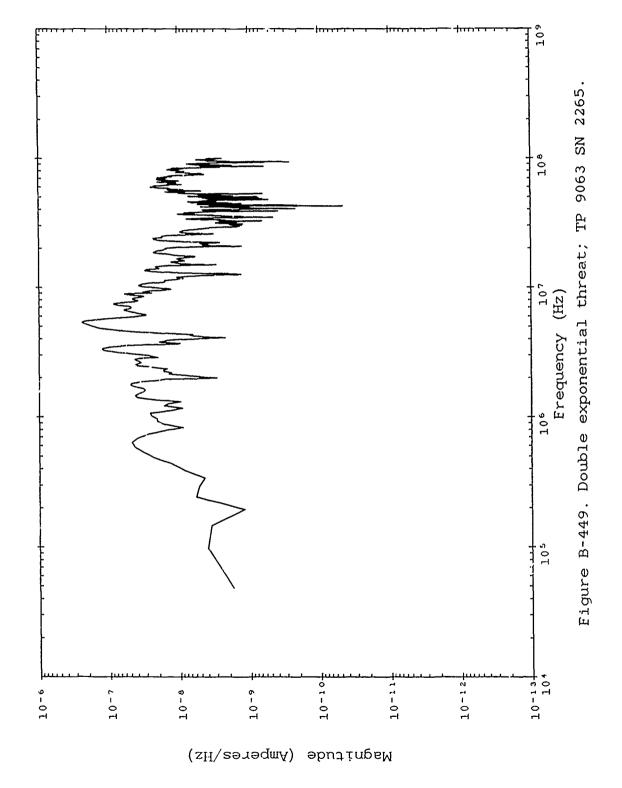


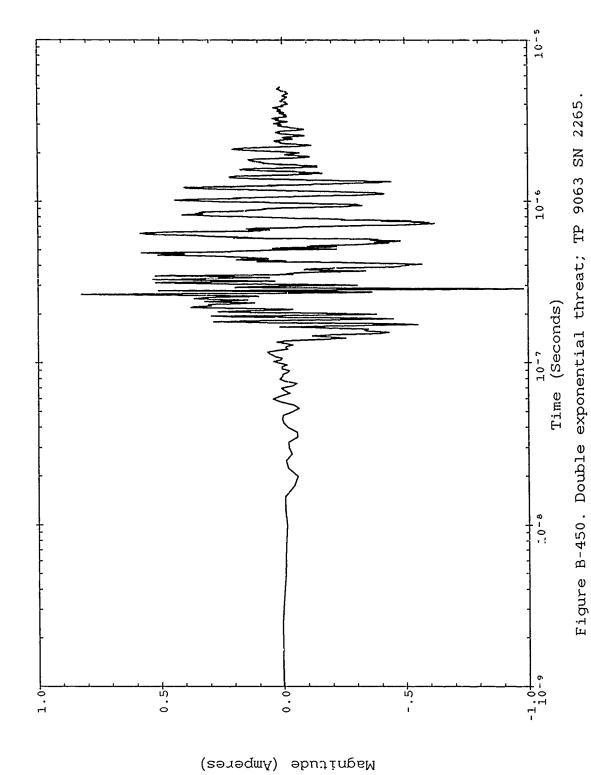


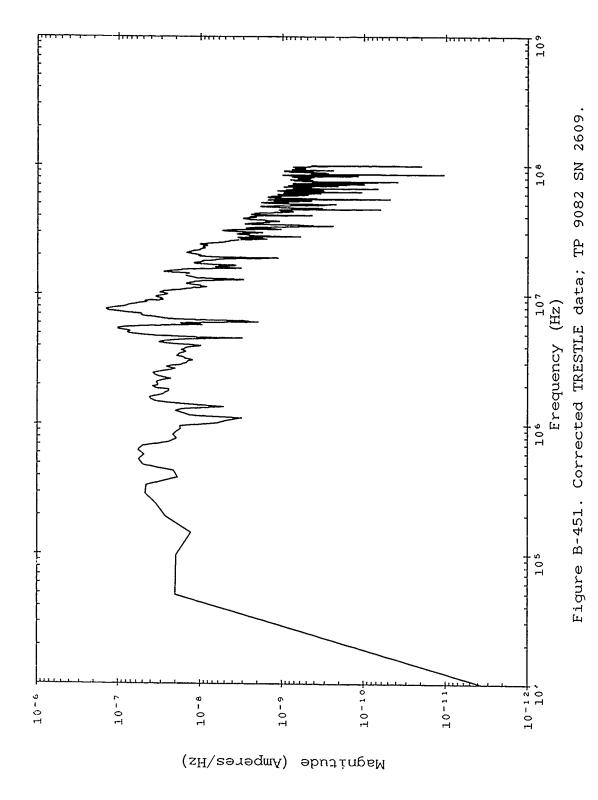


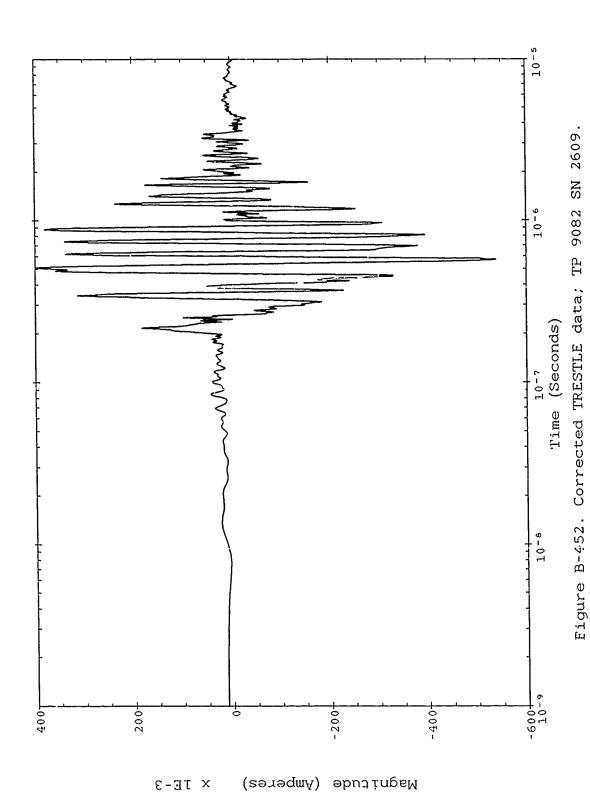
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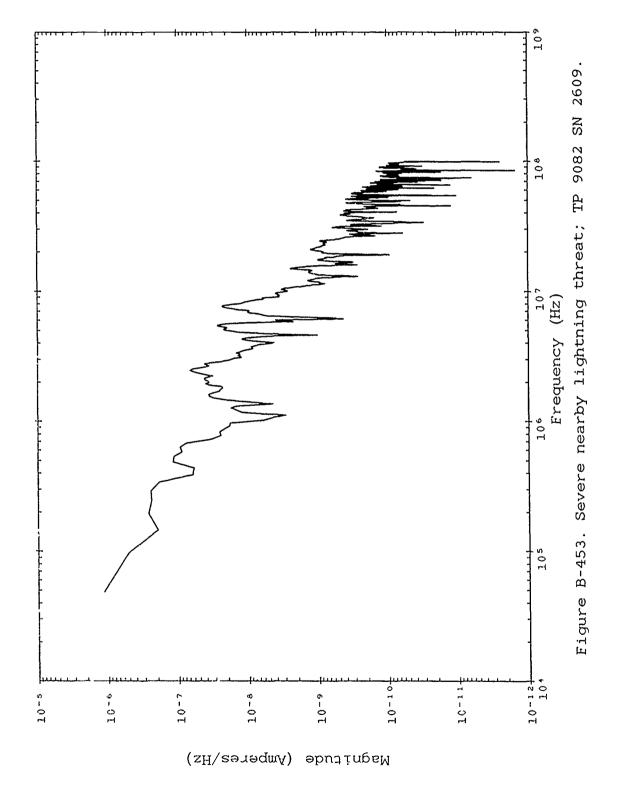
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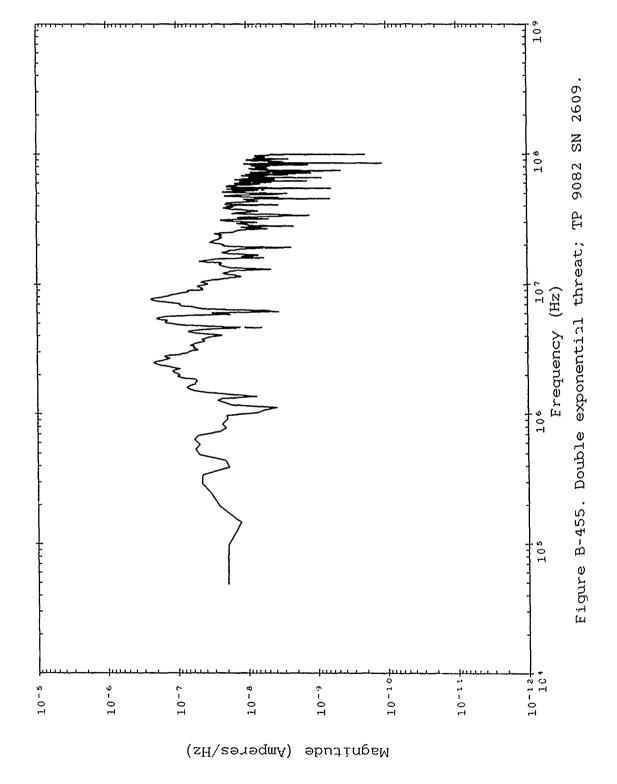


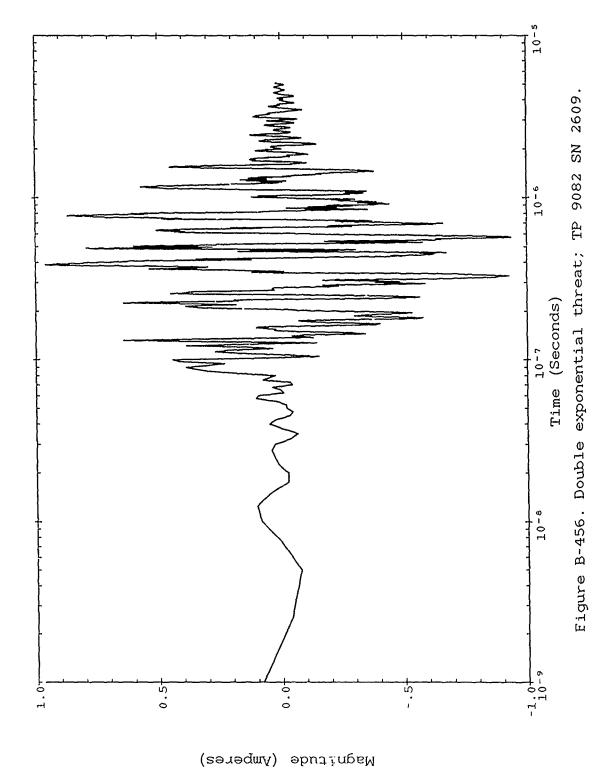
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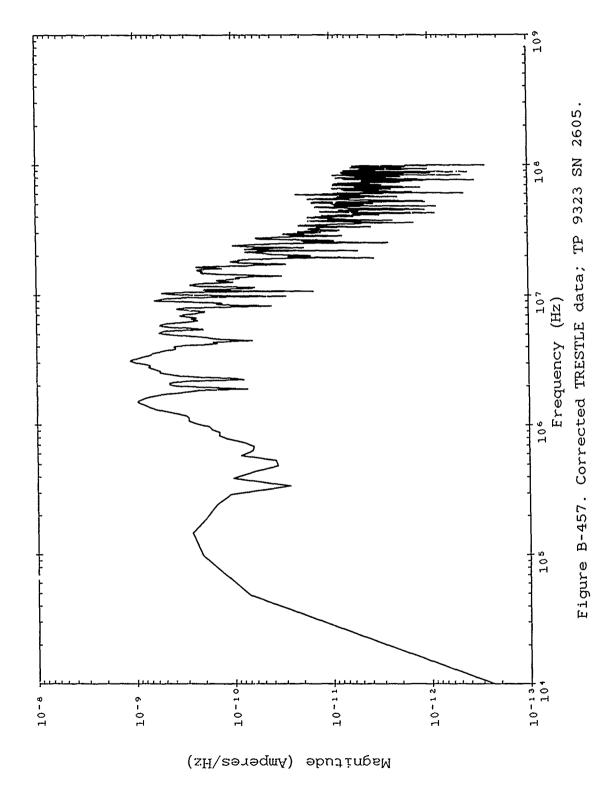
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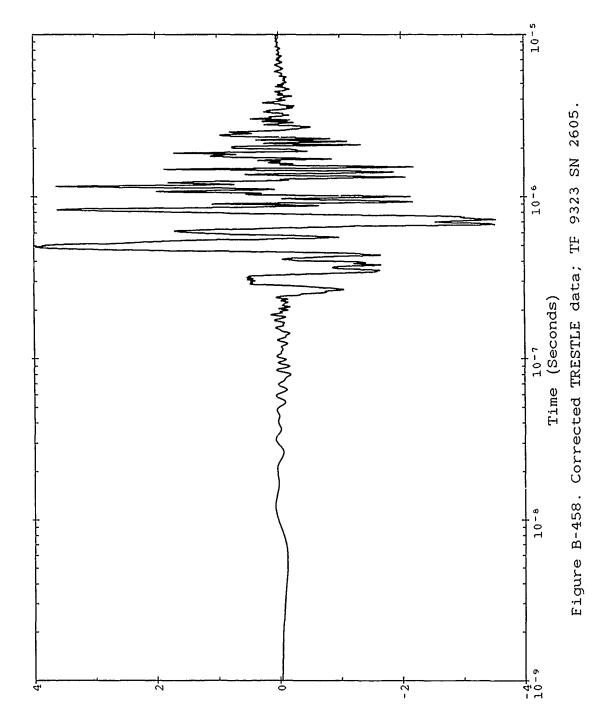
Magnitude (Amperes)





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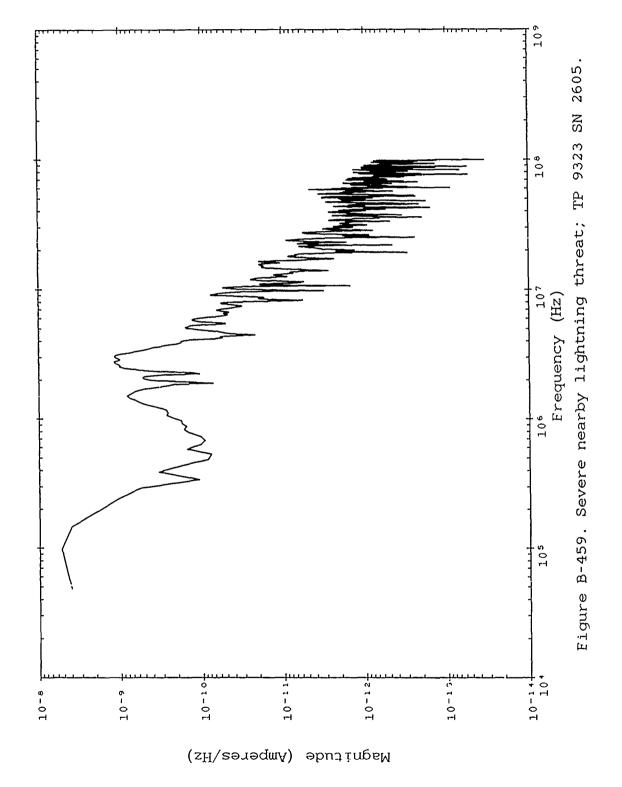


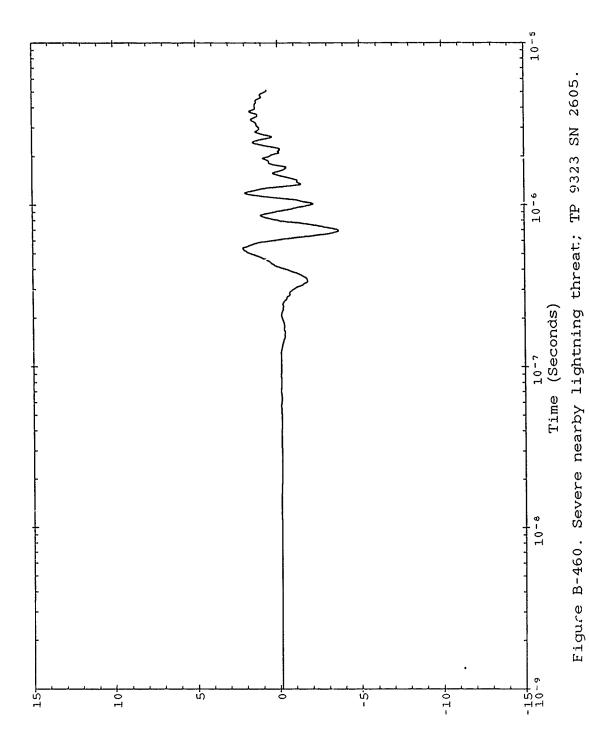


489

Magnitude (Amperes)

x 1E-3

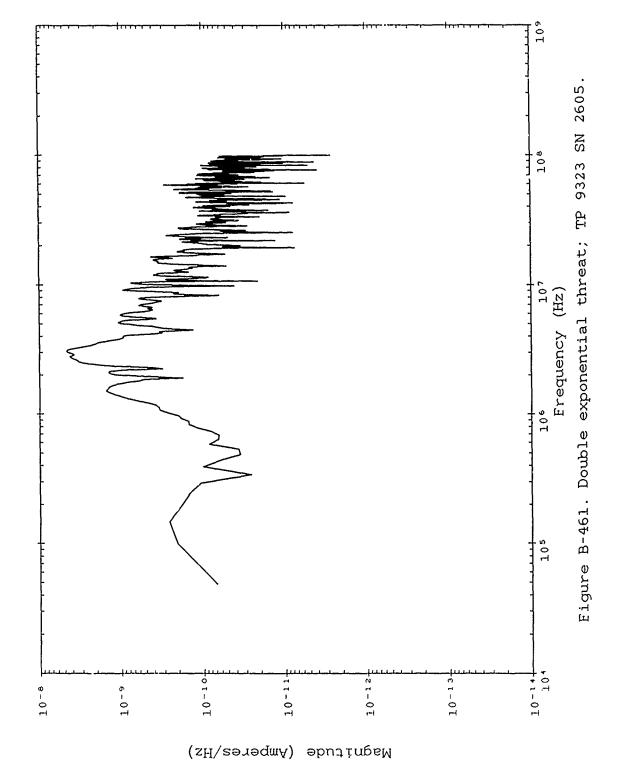


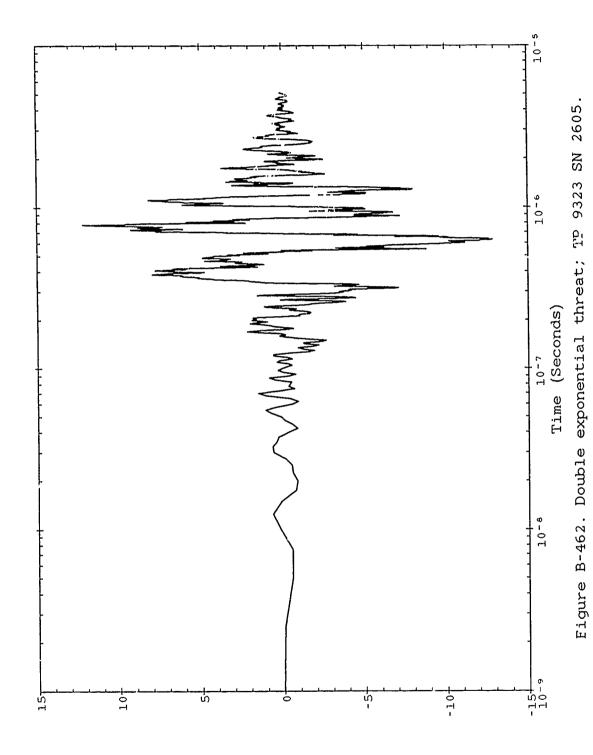


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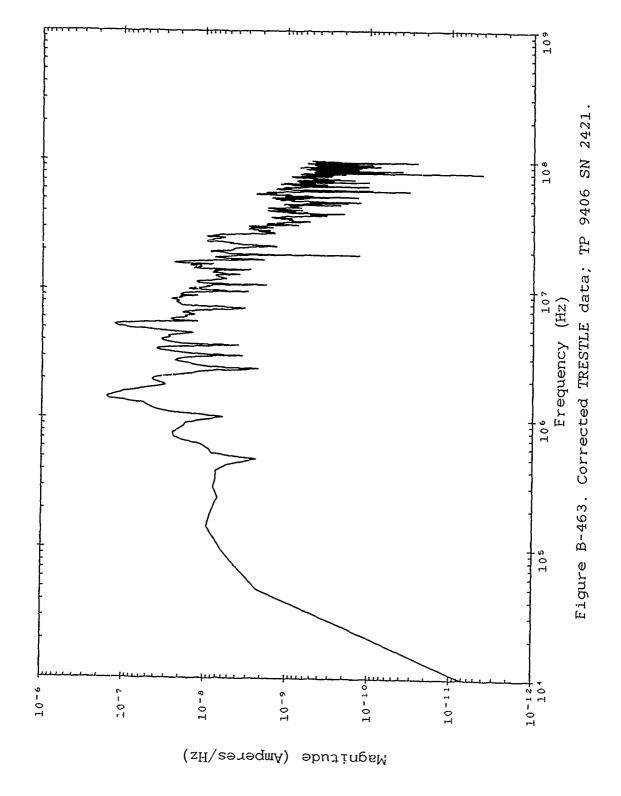
Magnitude (Amperes)

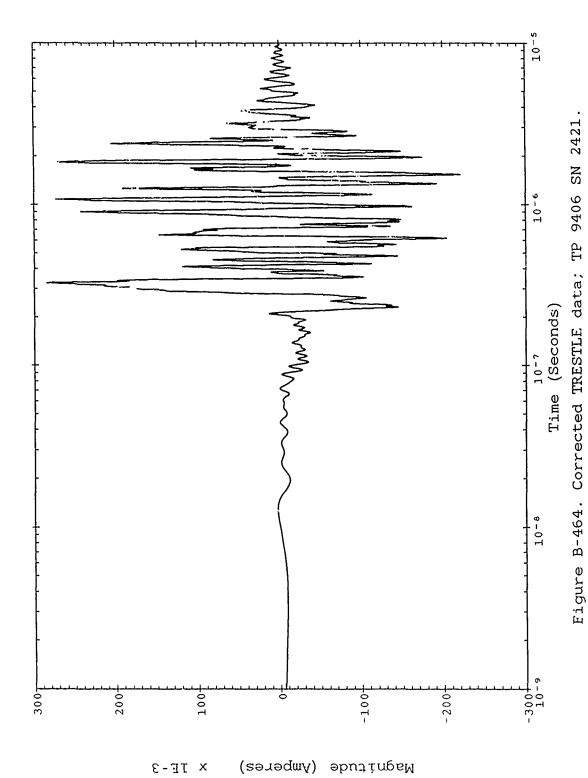
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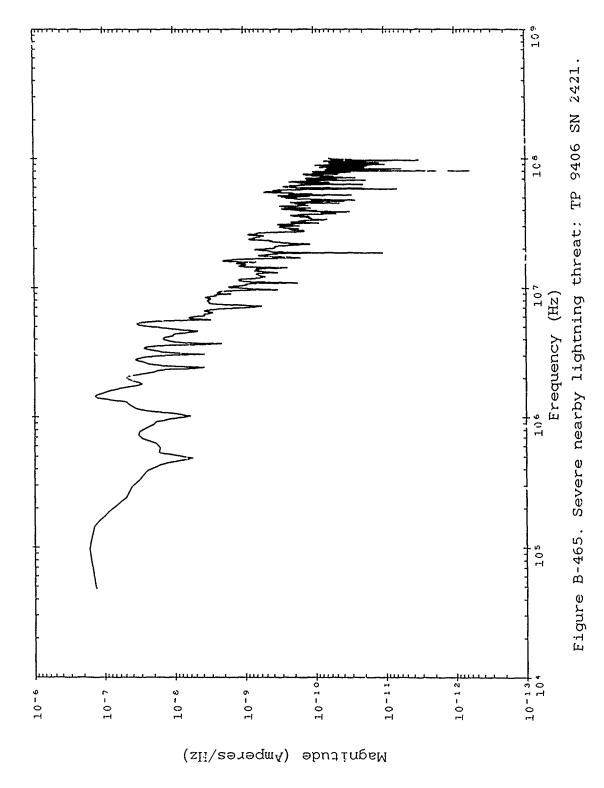


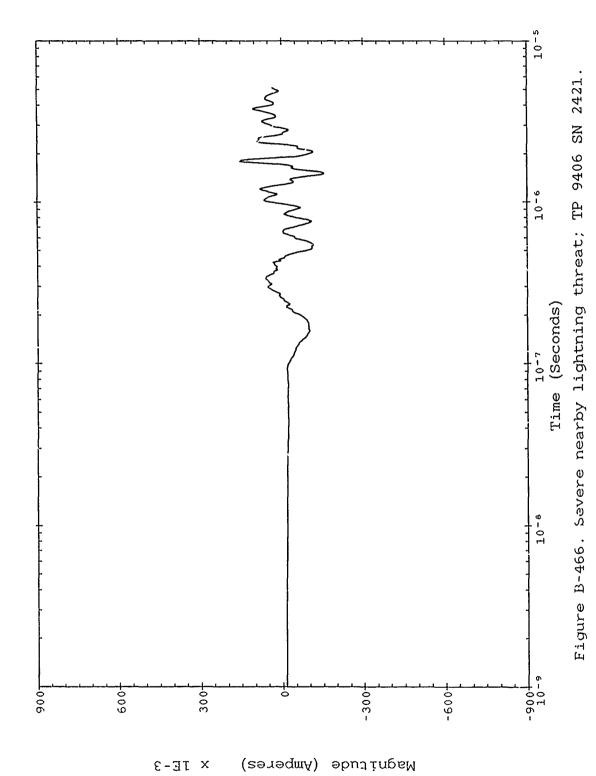
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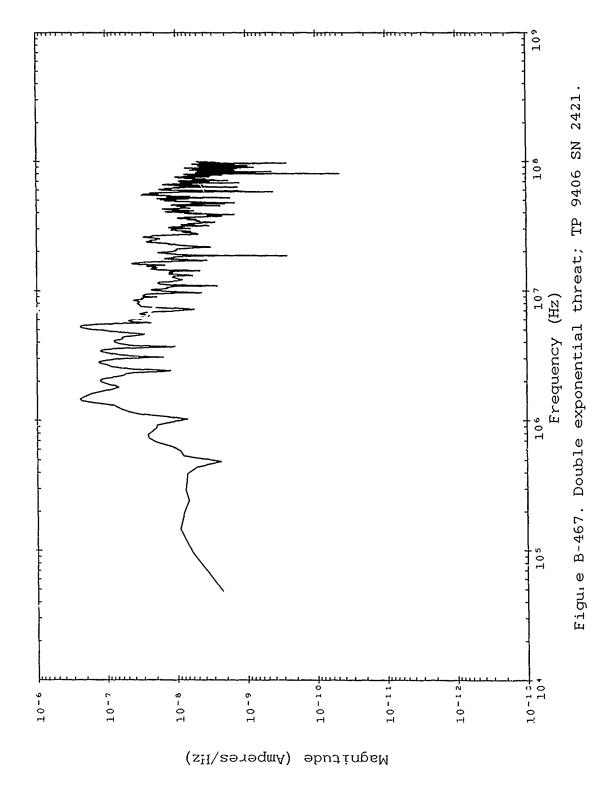


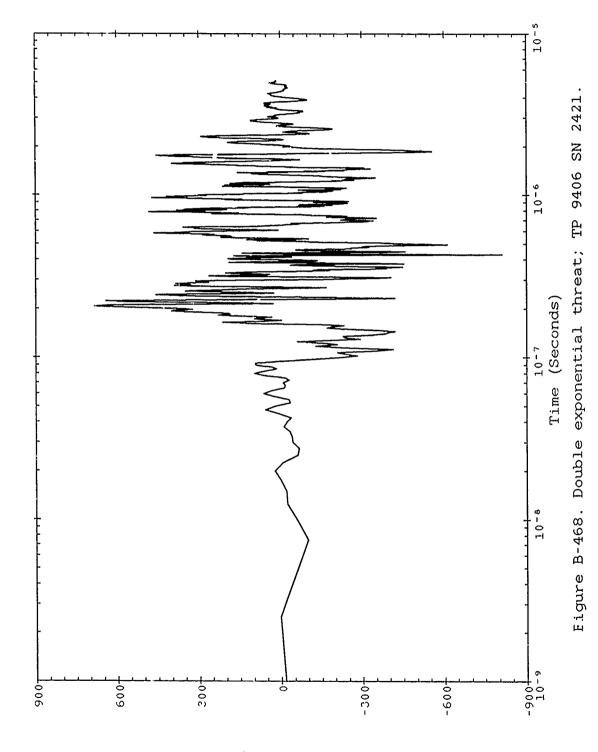


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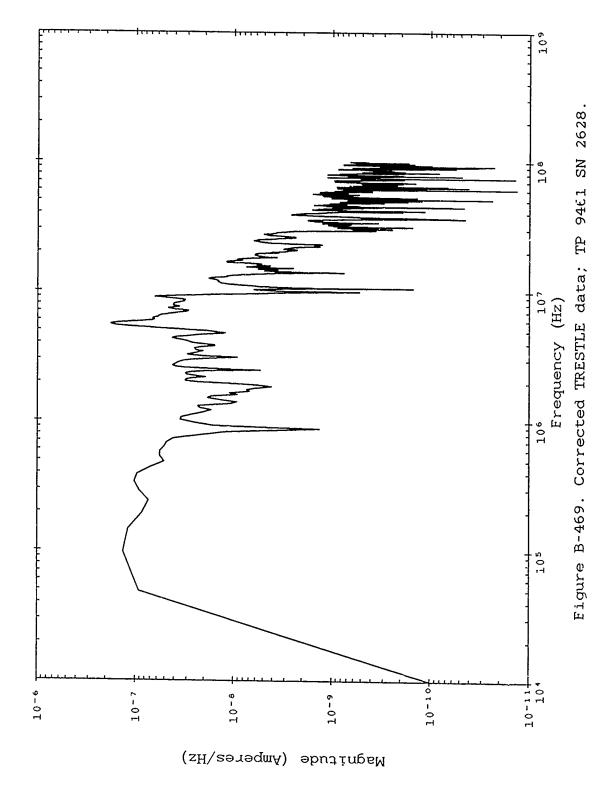


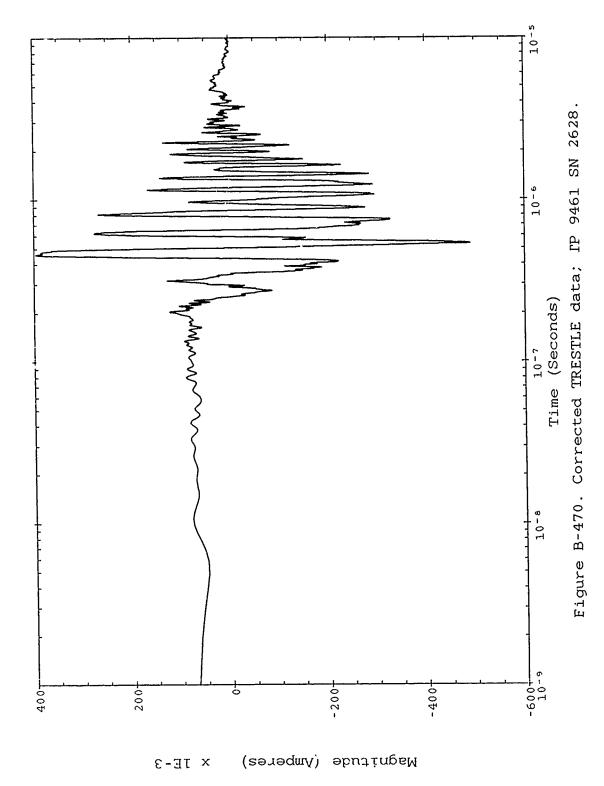


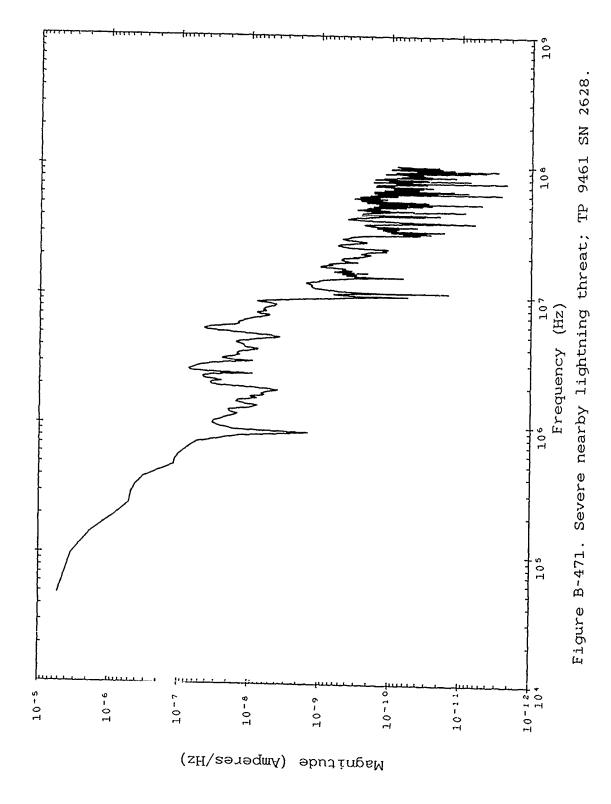


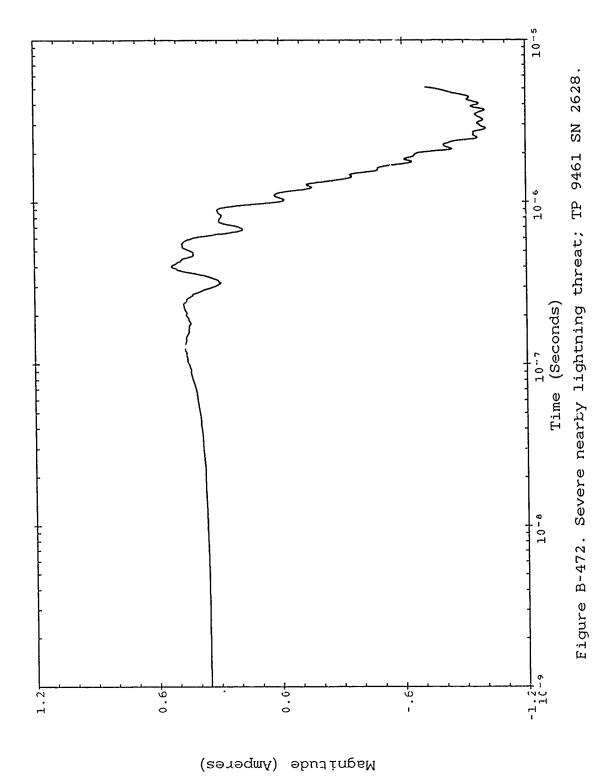


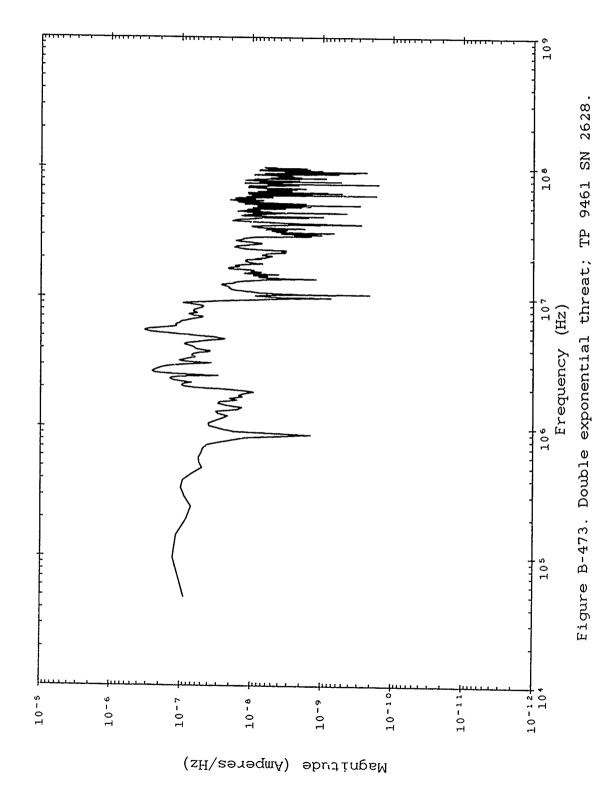
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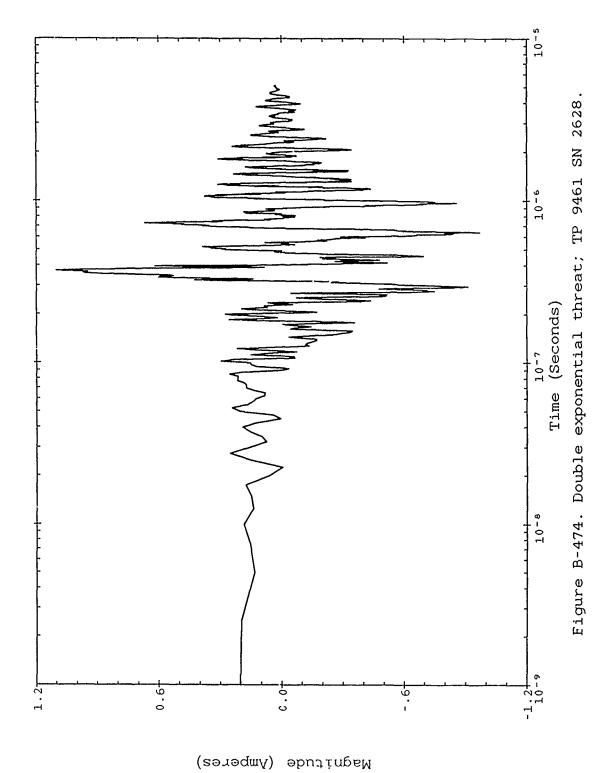


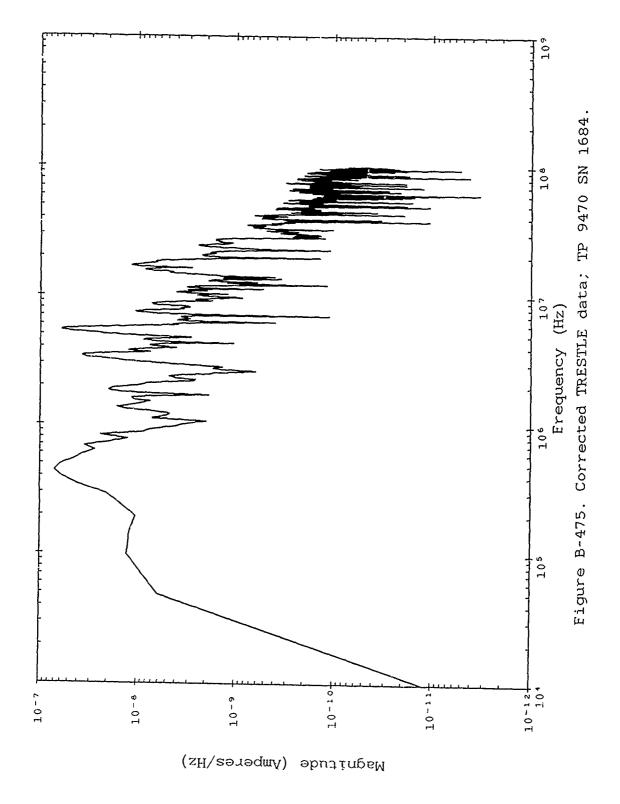


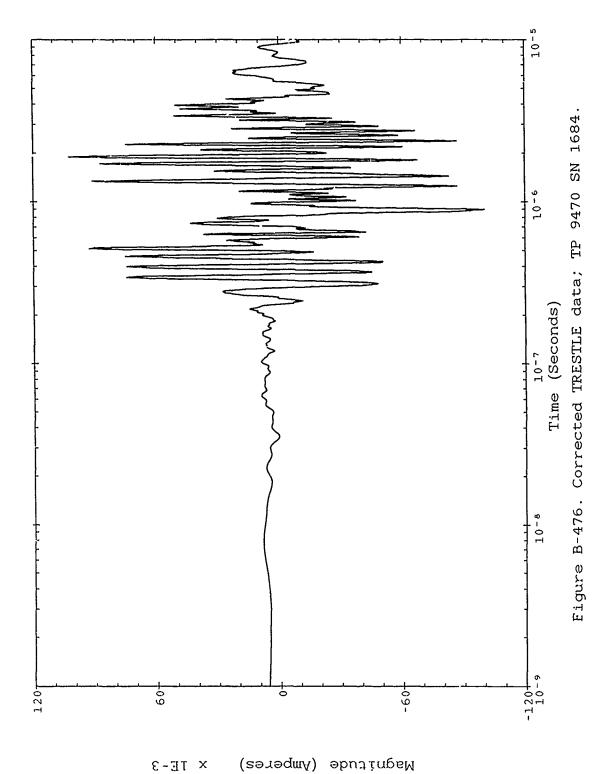




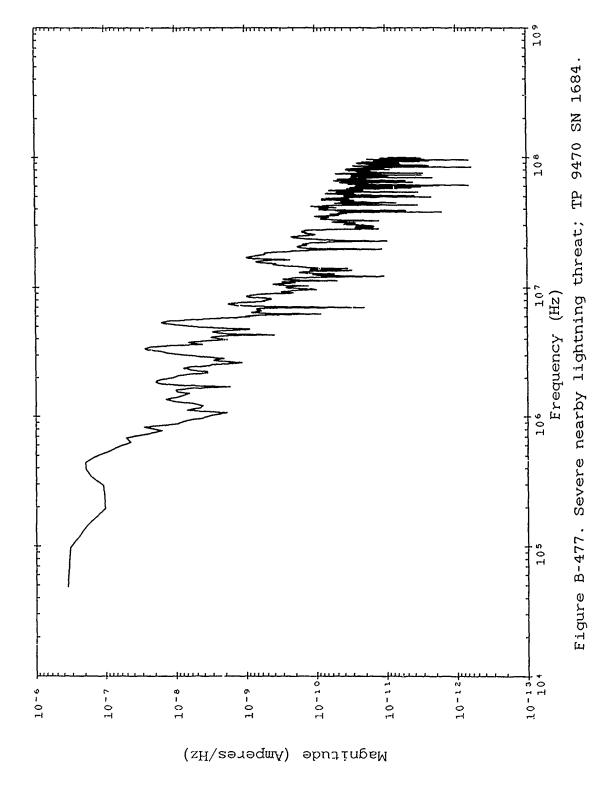


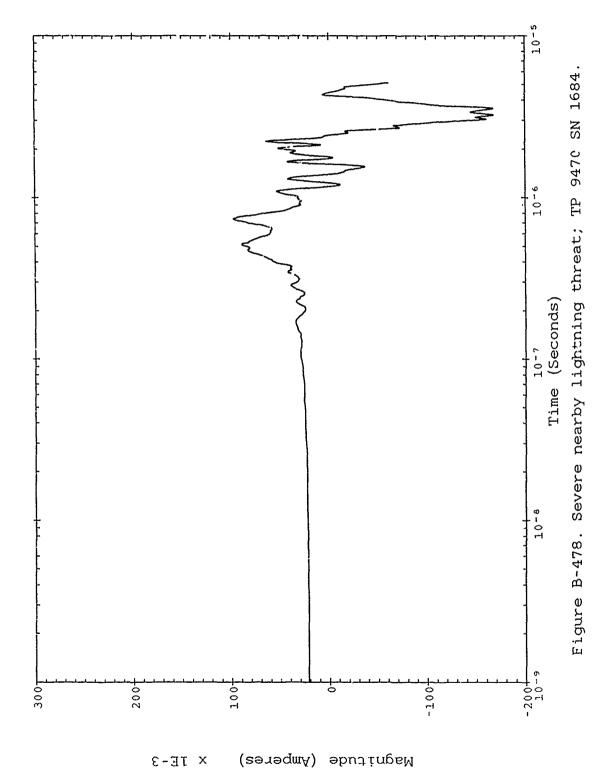


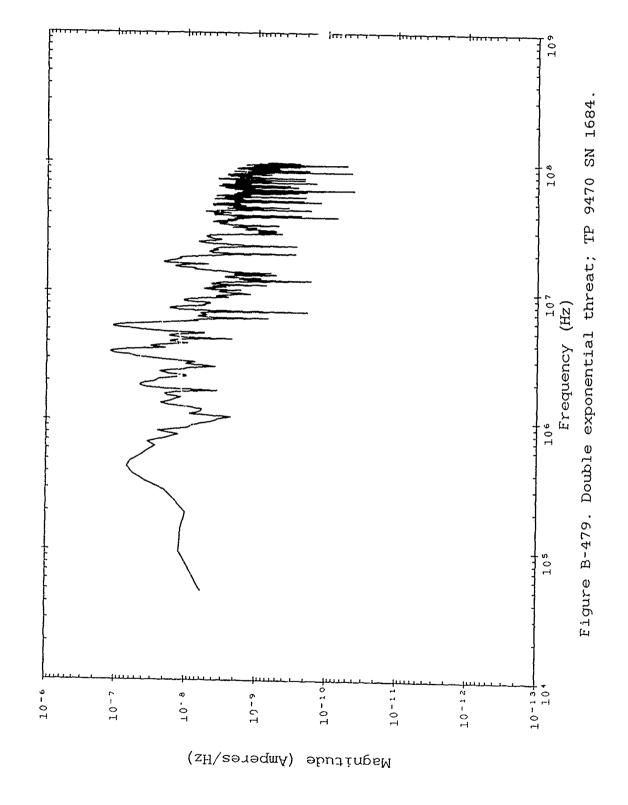


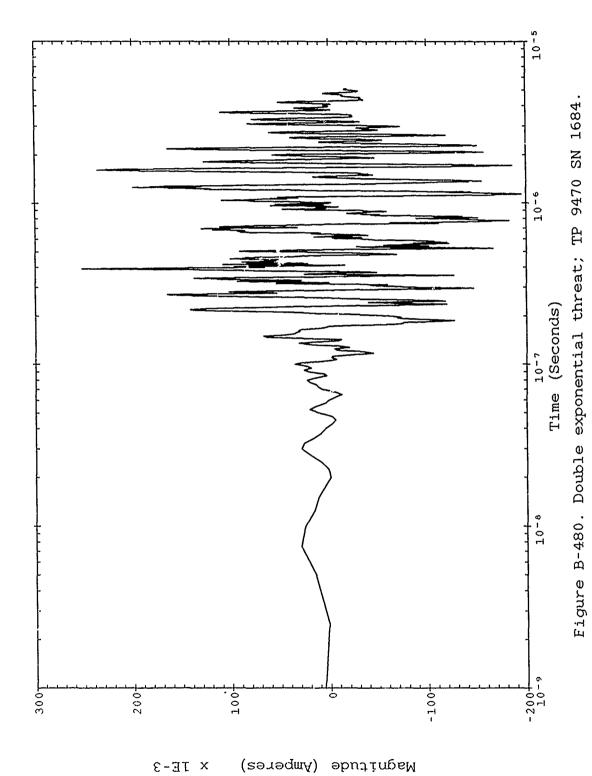


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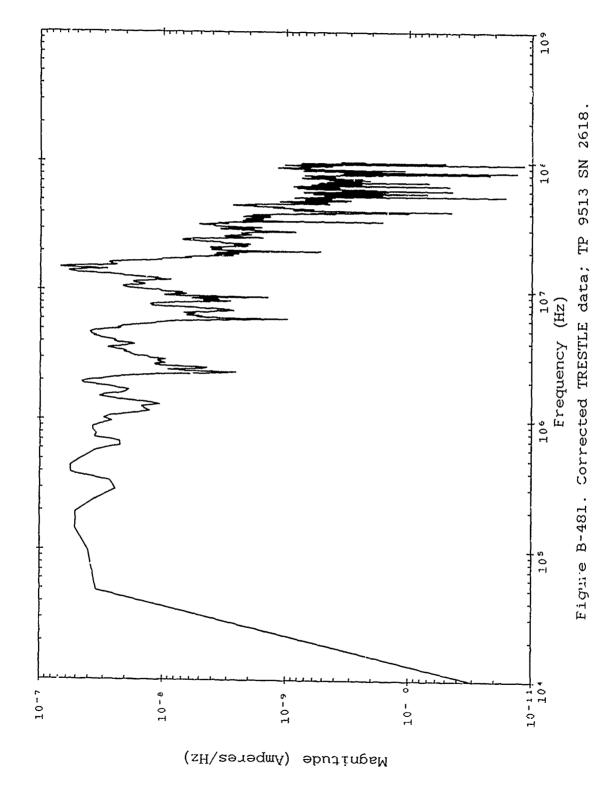


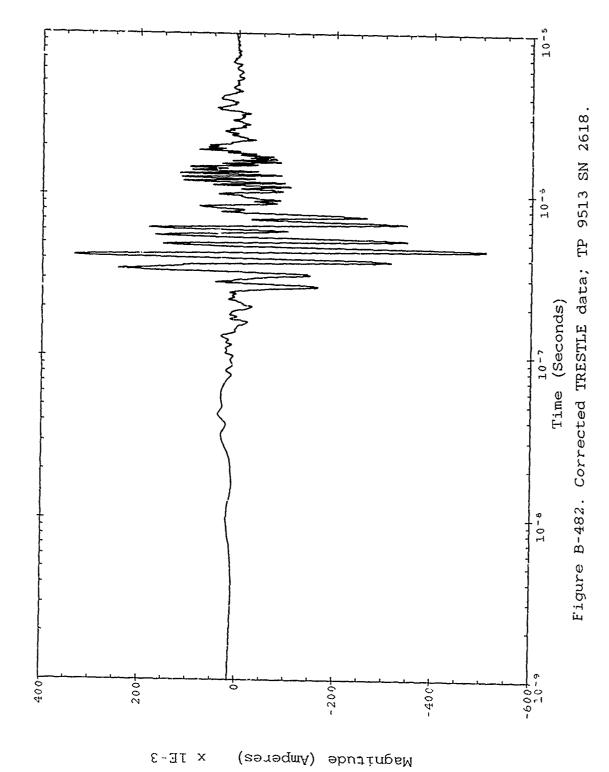


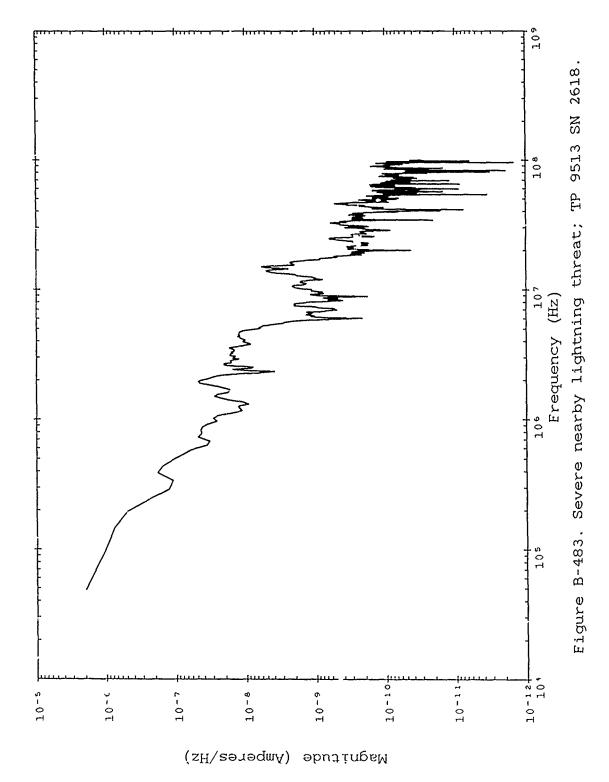


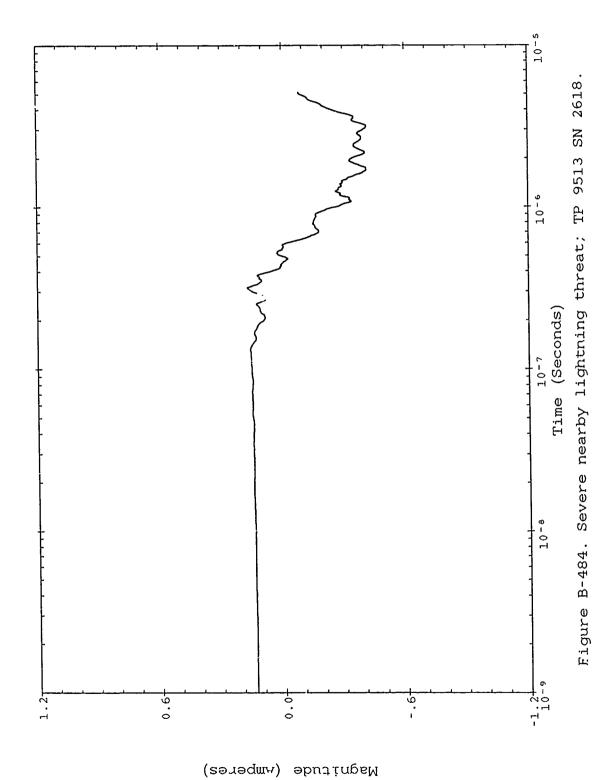
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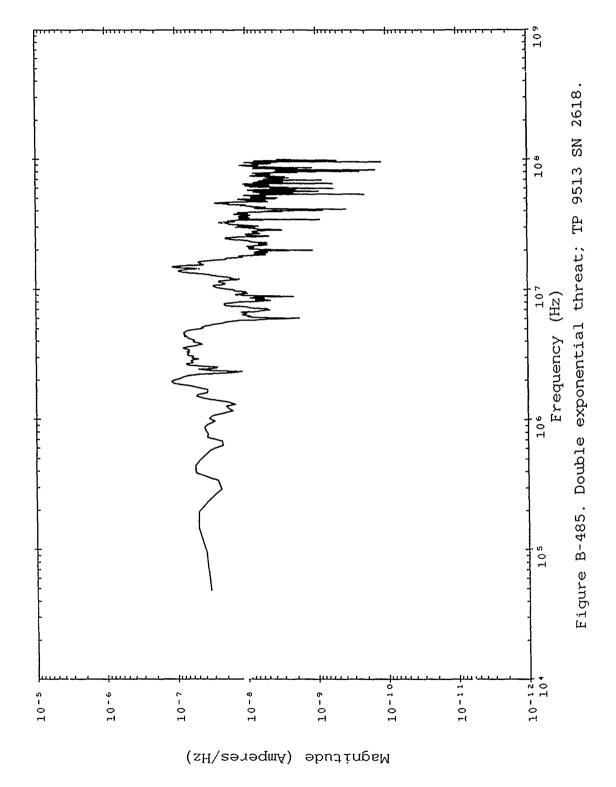
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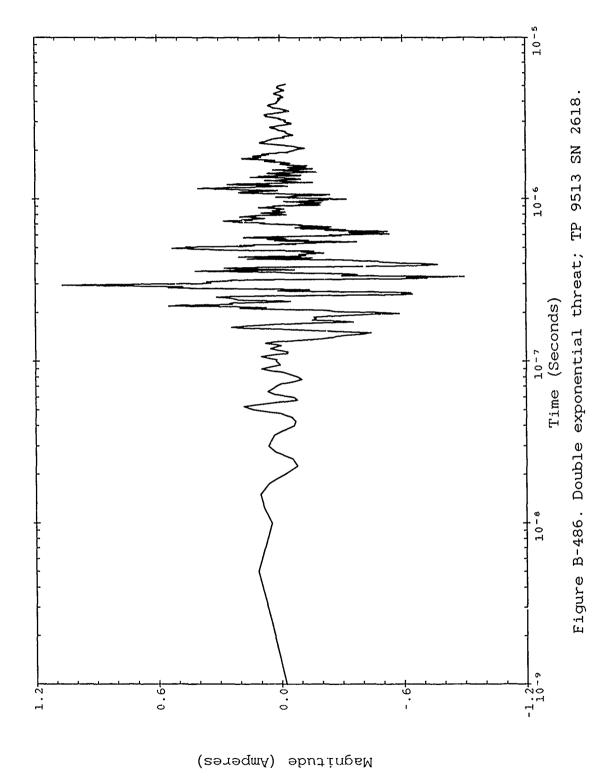






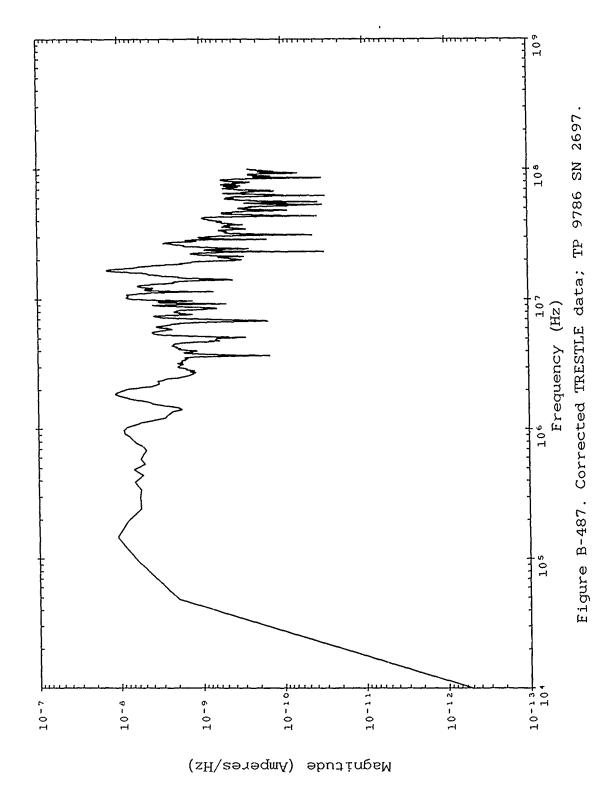


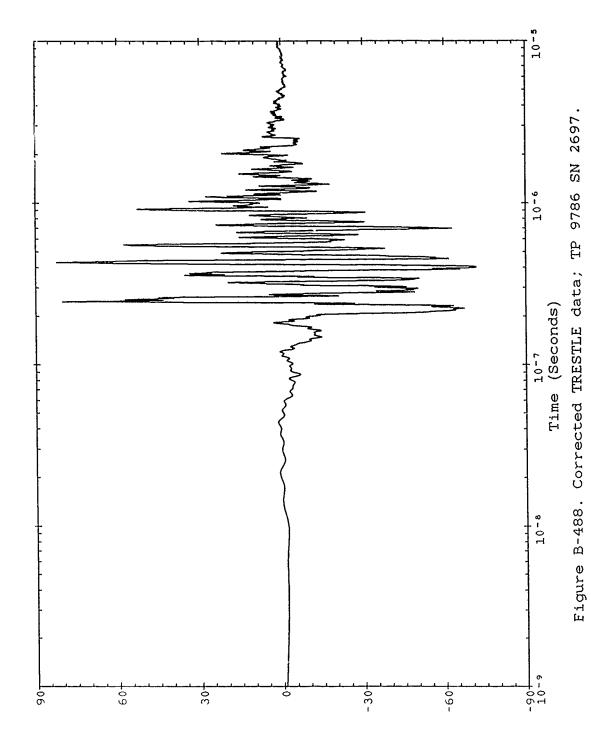




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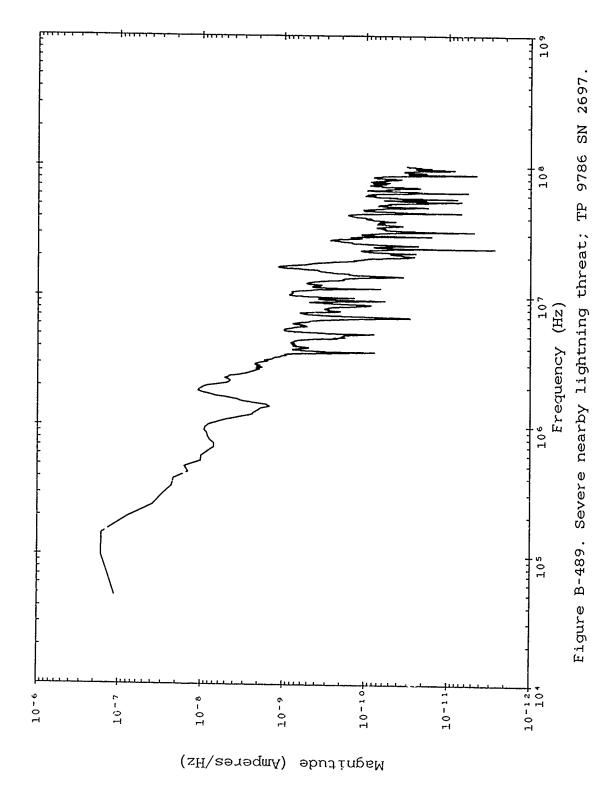
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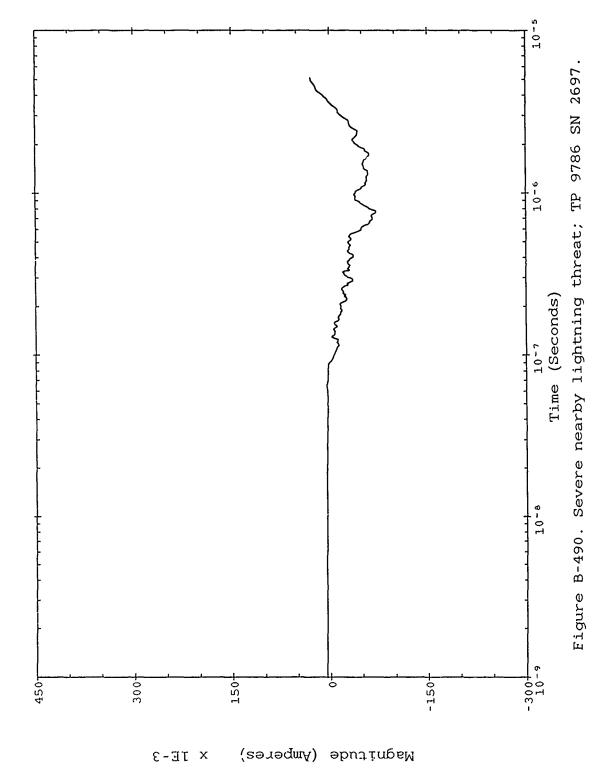


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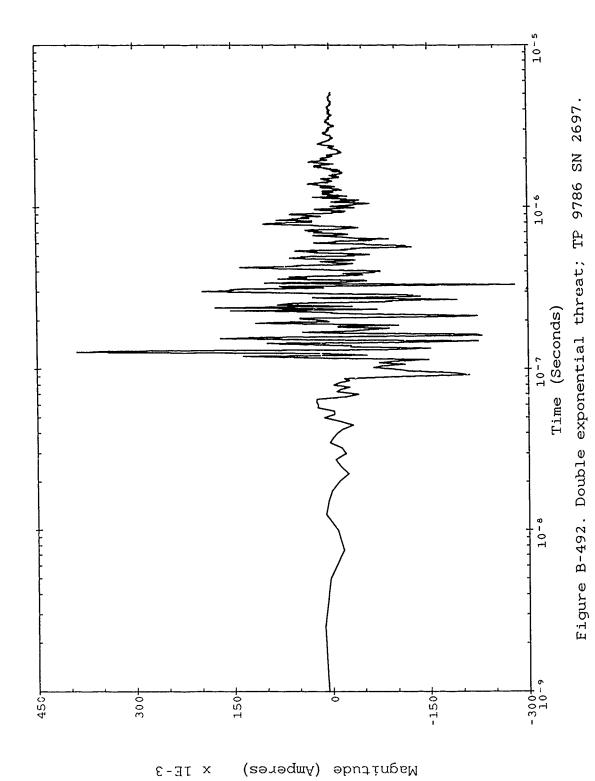
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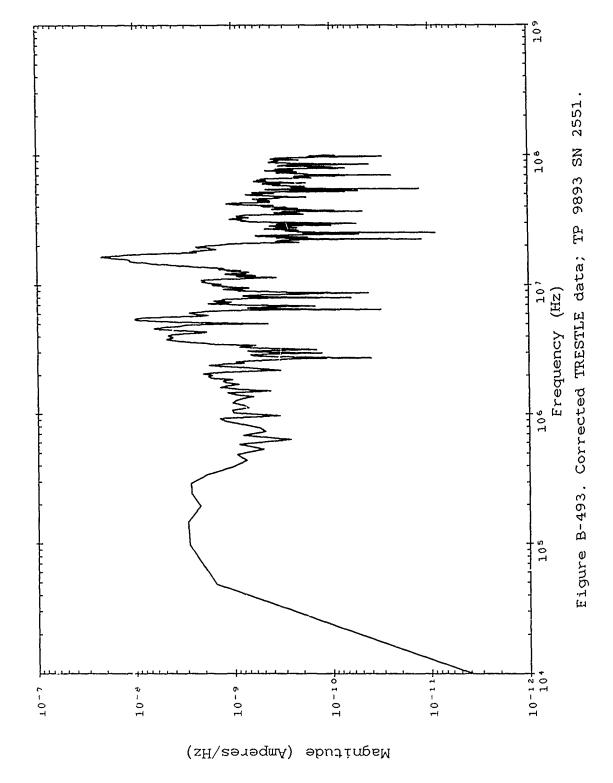
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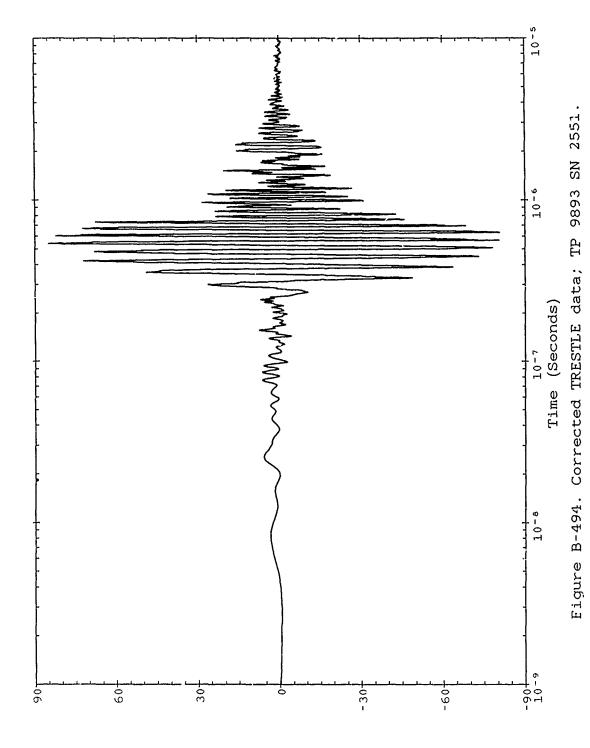




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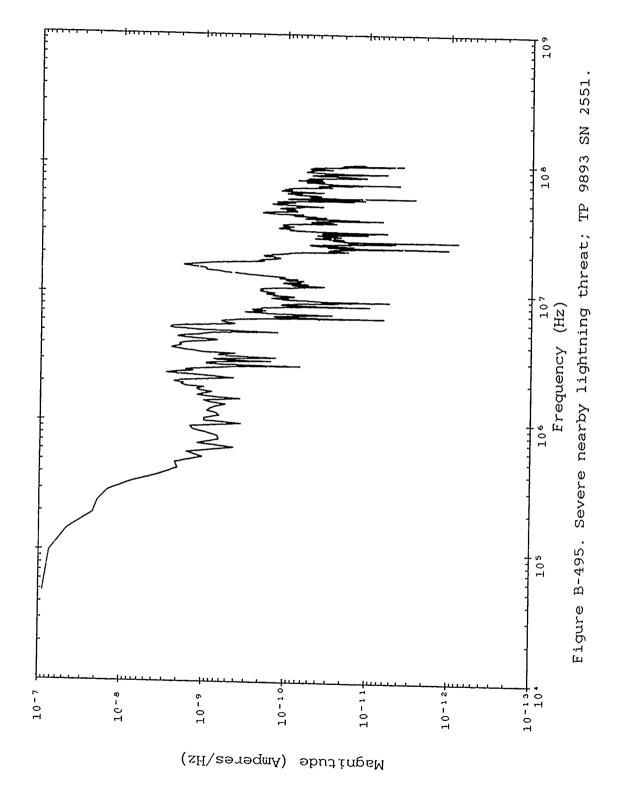


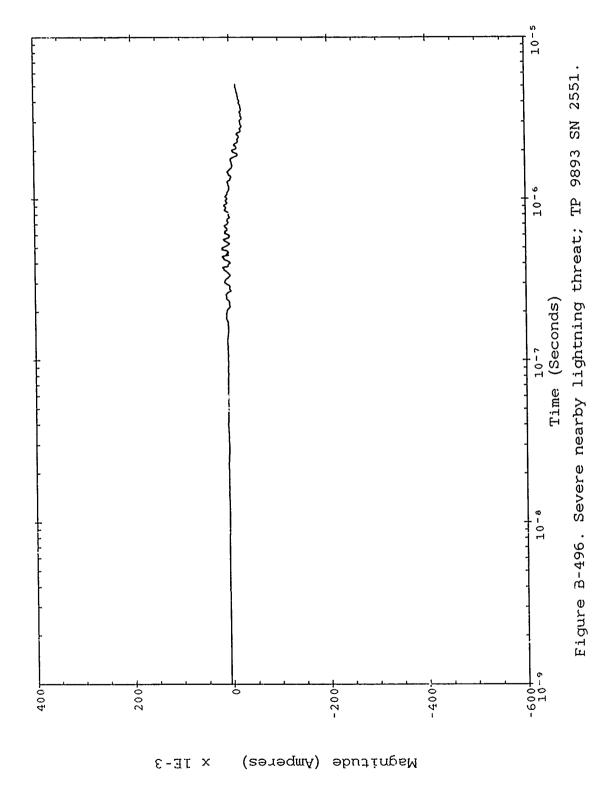


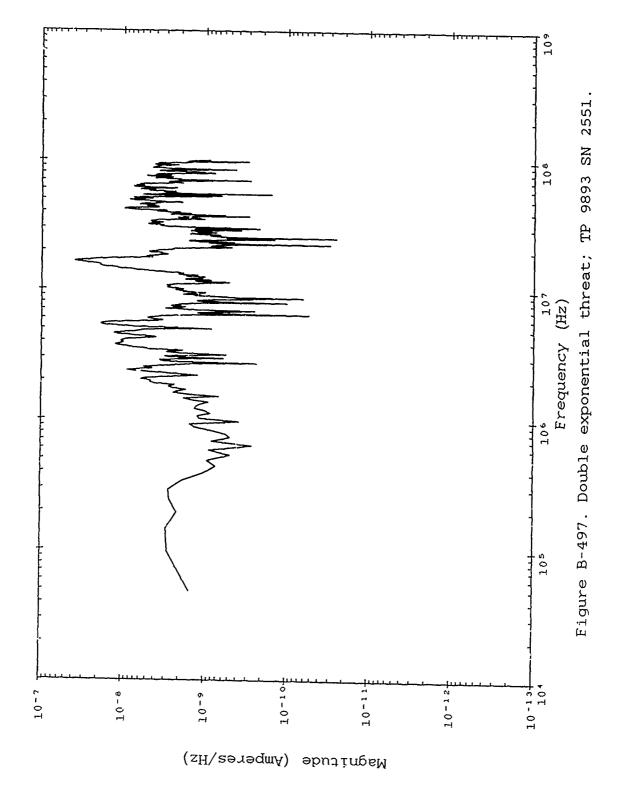
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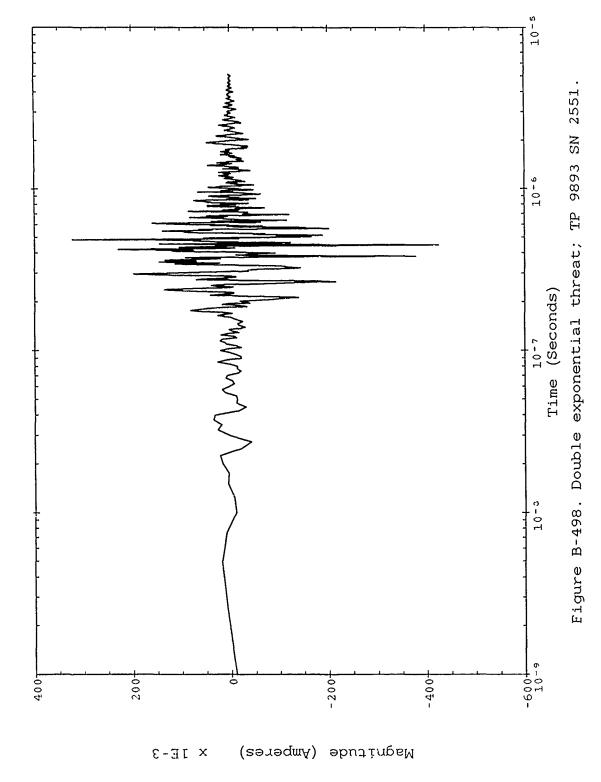
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